



Far-Field Propagation of Airburst Events Using a Cartesian Method



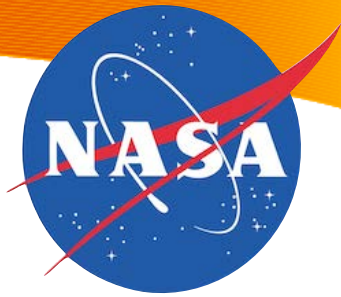
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NASA Advanced Supercomputing Division
NASA Ames Research Center

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Asteroids Characterization, Atmospheric Entry and
Risk Assessment





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- NASA Advanced Supercomputing Division – Task 3 & 4 teams

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- Entry Systems Division – Task 2 team

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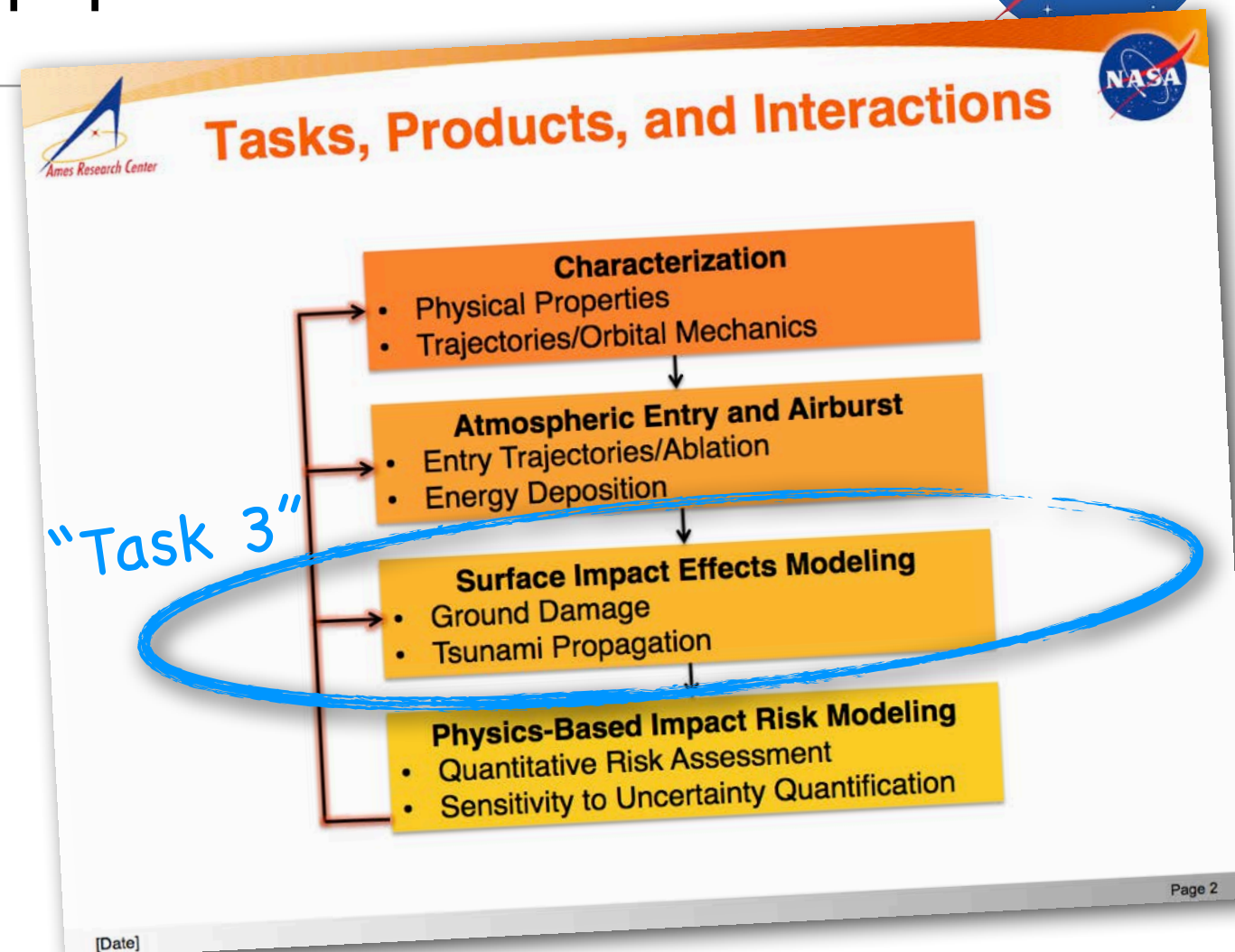
- New York University

Marsha Berger

ARC Planetary Defense IPT

Ground & Water Effects

- “Task 3” of the PD IPT
- Focus on ground effects modeling
 - Airburst & atmospheric propagation
 - Surface overpressure & wind prediction
 - Ground damage
 - Tsunami propagation
- Inputs come from entry and airburst modeling in Task 2
- Outputs of atmospheric propagation feed tsunami modeling
- Outputs of atmospheric & tsunami modeling feed physics-based risk models in Task 4

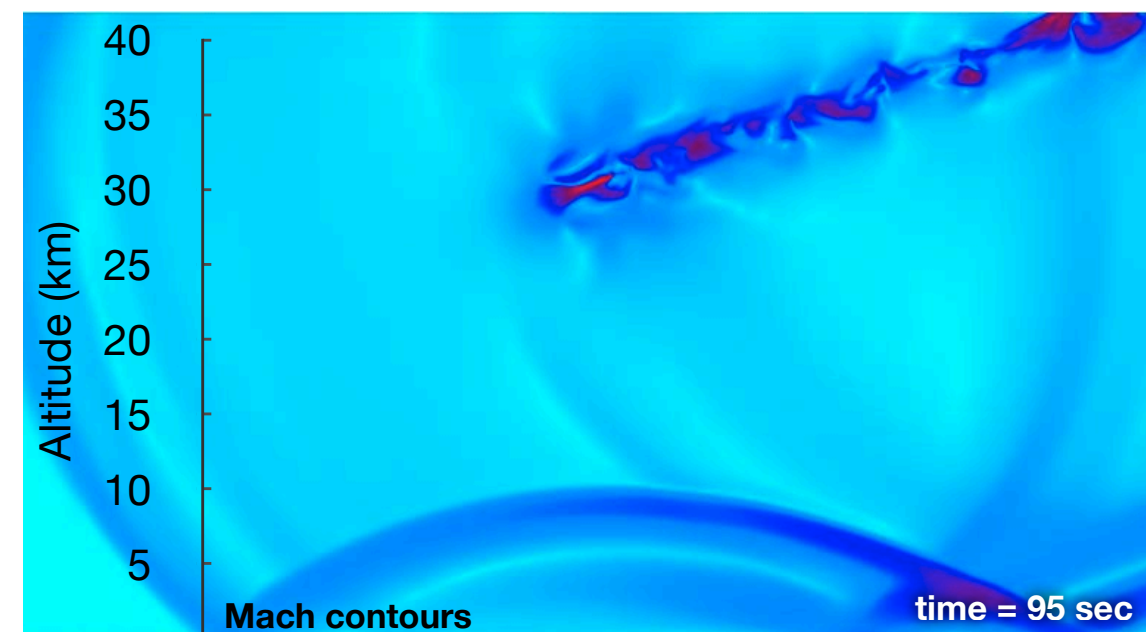
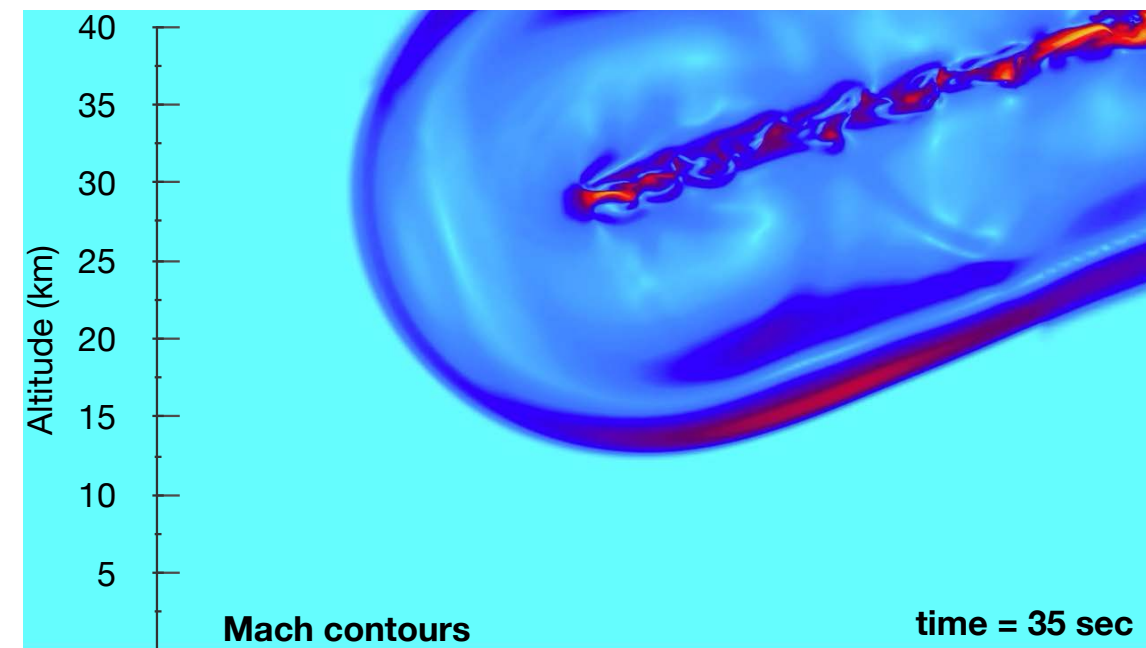
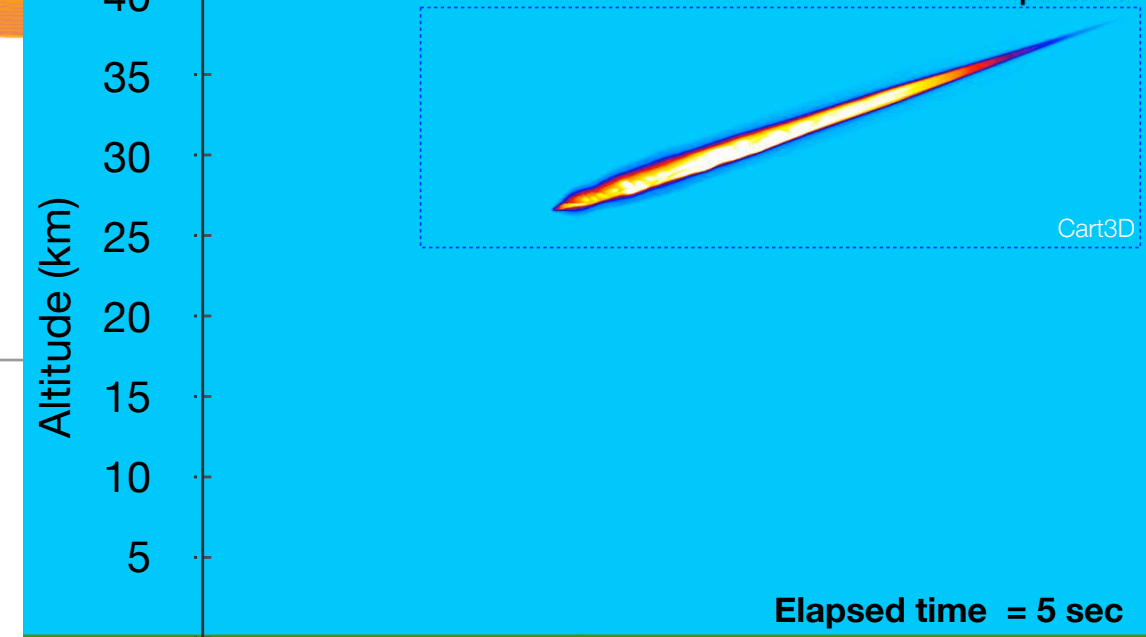


ARC Planetary Defense IPT

Goal of atmospheric propagation is prediction of surface footprint

- Far-field atmospheric propagation drives
 - Ground footprint and land damage prediction
 - Atmospheric forcing for tsunami modeling
- Focus
 - Perform detailed reconstruction of specific events
 - Perform parametric studies to develop surface footprint models for PRA
 - Goal is to do thousands of such simulations – need to control computational expense

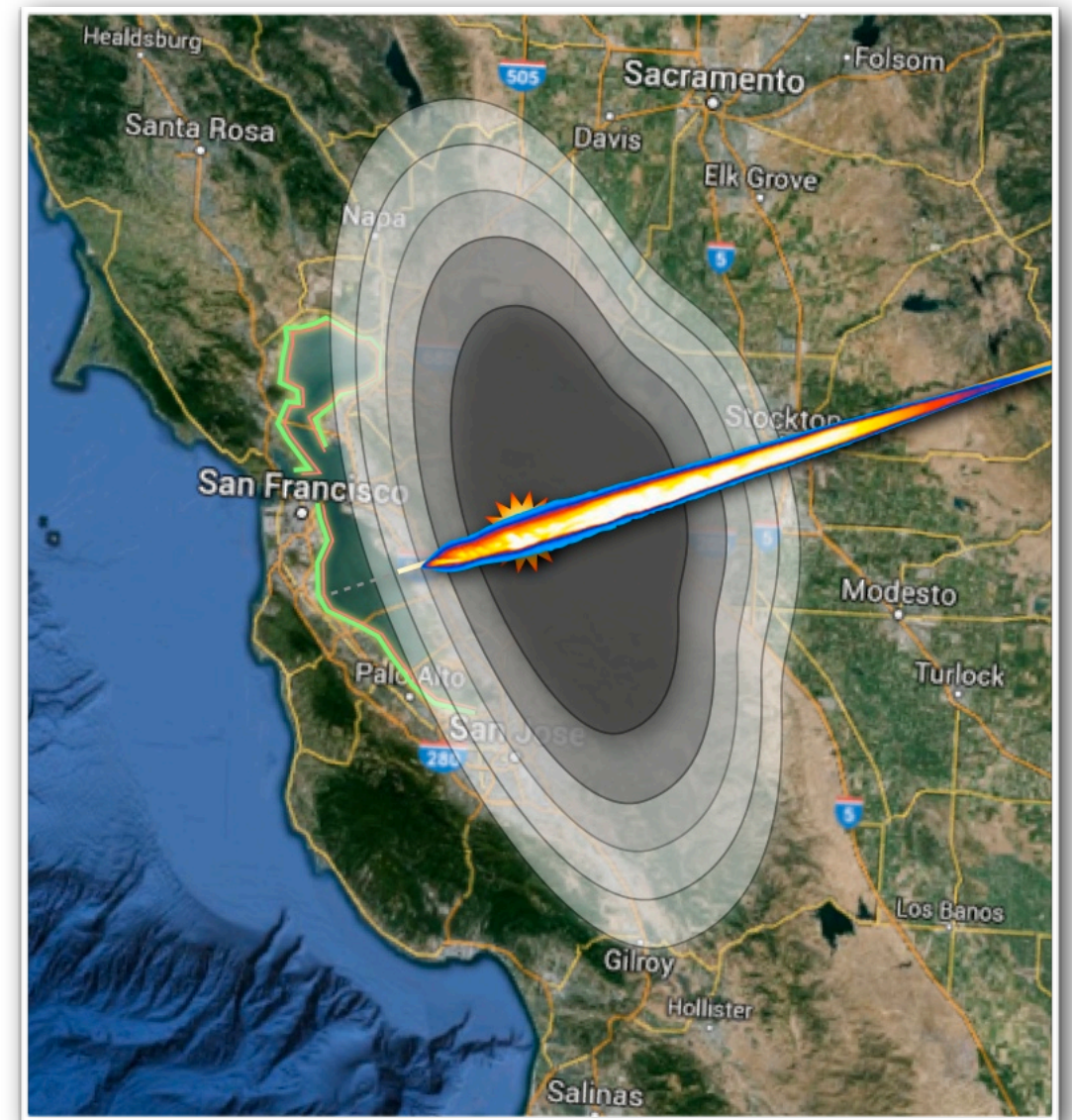
Current work focuses on airburst only, no ground impact



Overview

Report current status of effort and connection with PRA and tsunami

- Modeling tools & solver
- Verification & Validation
 - Basic
 - Chelyabinsk Case Study
- Investigations of ground-footprint sensitivity
 - Line-source vs time-dependent entry
 - Entry Angle
- Upcoming Efforts



Overview

Report current status of effort and connection with PRA and tsunami

- Modeling tools & solver

- Verification

- Physics

- Code

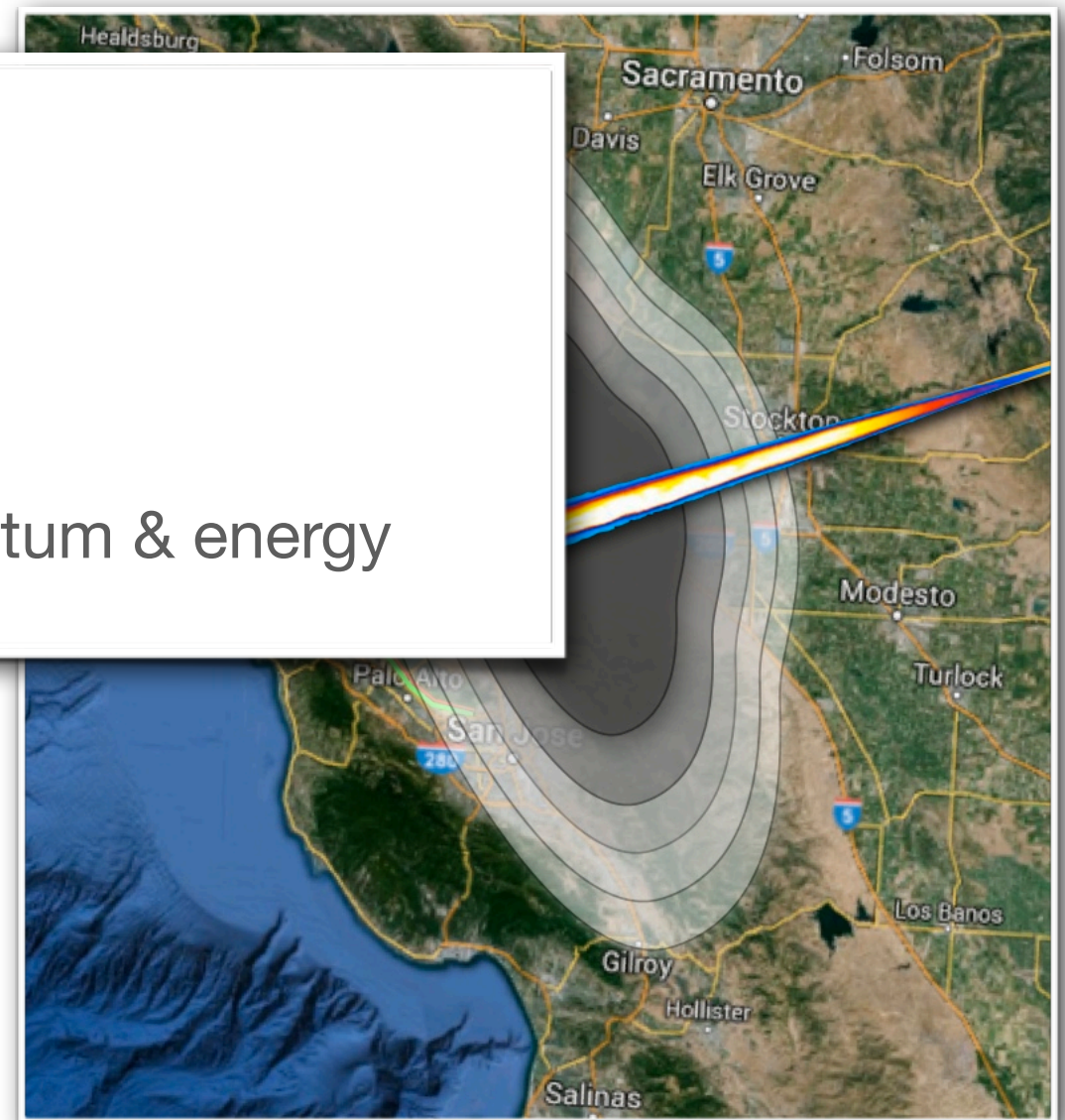
- Investigation

- Data

- Model

- Atmosphere model
- Governing equations
- Solver and simulation methodology
- Model for deposition of mass, momentum & energy

- Upcoming Efforts



Modeling

Inviscid scale-height atmosphere model

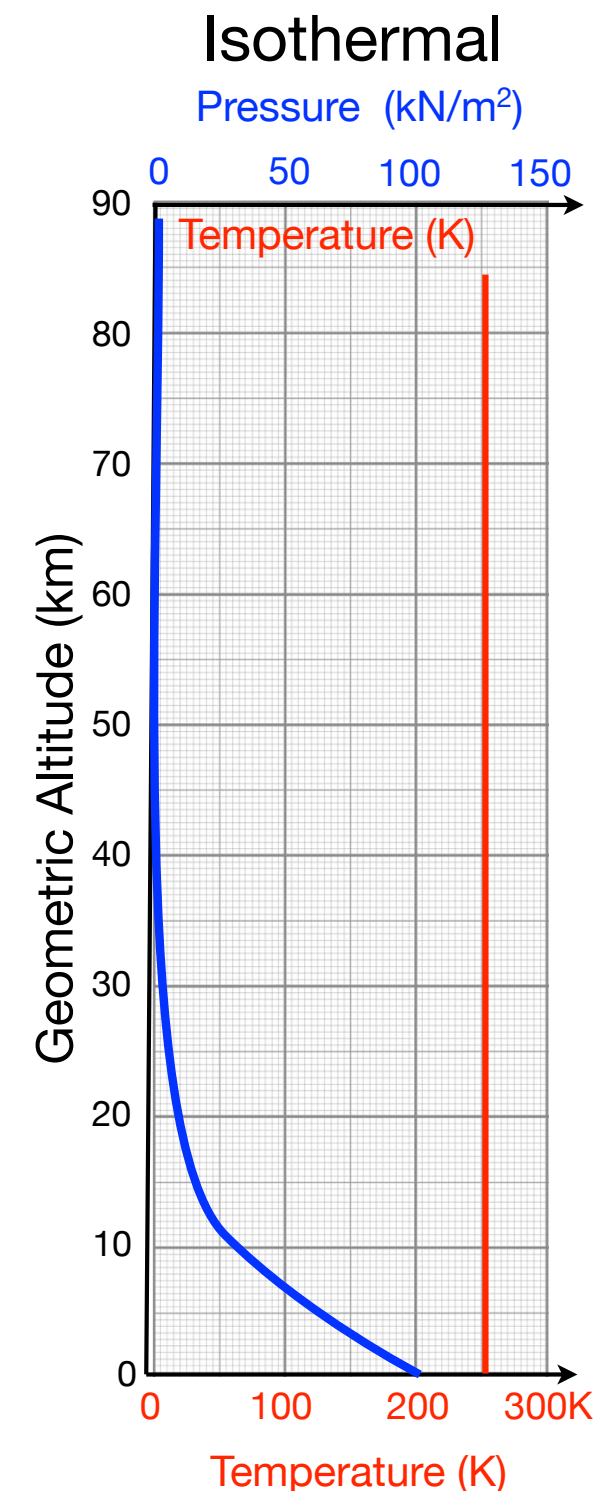
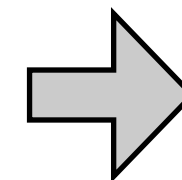
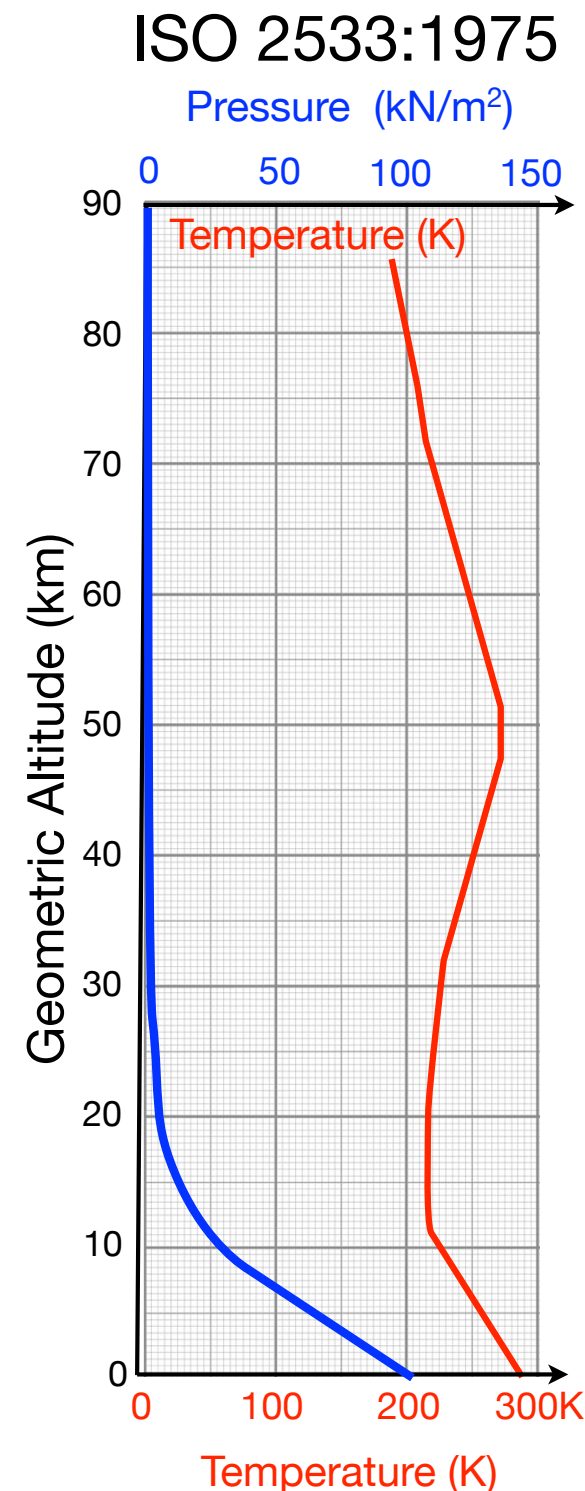
- Atmosphere model based on 1976 Standard Atmosphere (ISO 2533:1975)

- Isothermal approximation for scale-height description

$$P(z) = P_o e^{-z/H}$$

$$\rho(z) = \frac{P(z)}{RT}$$

- Use $H = 8$, and initialize simulations with atmosphere in hydrostatic equilibrium



Modeling

Inviscid scale-height atmosphere model

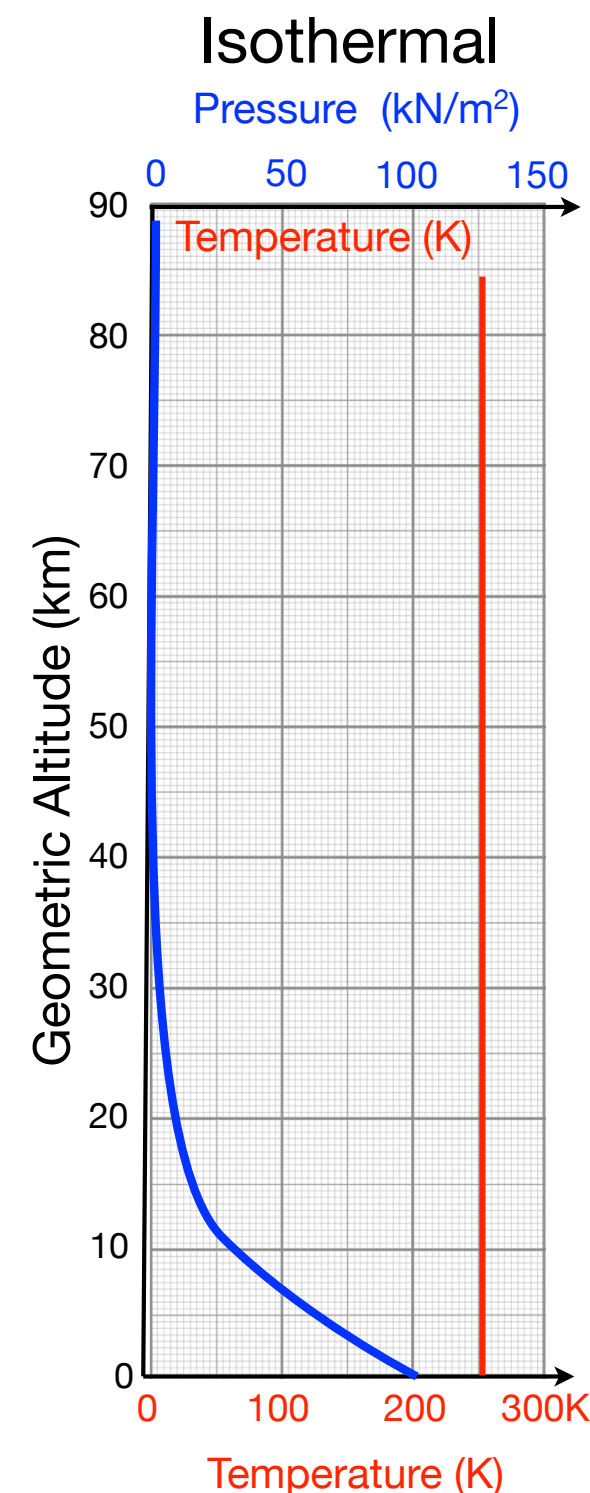
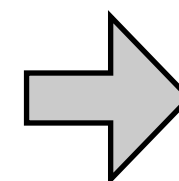
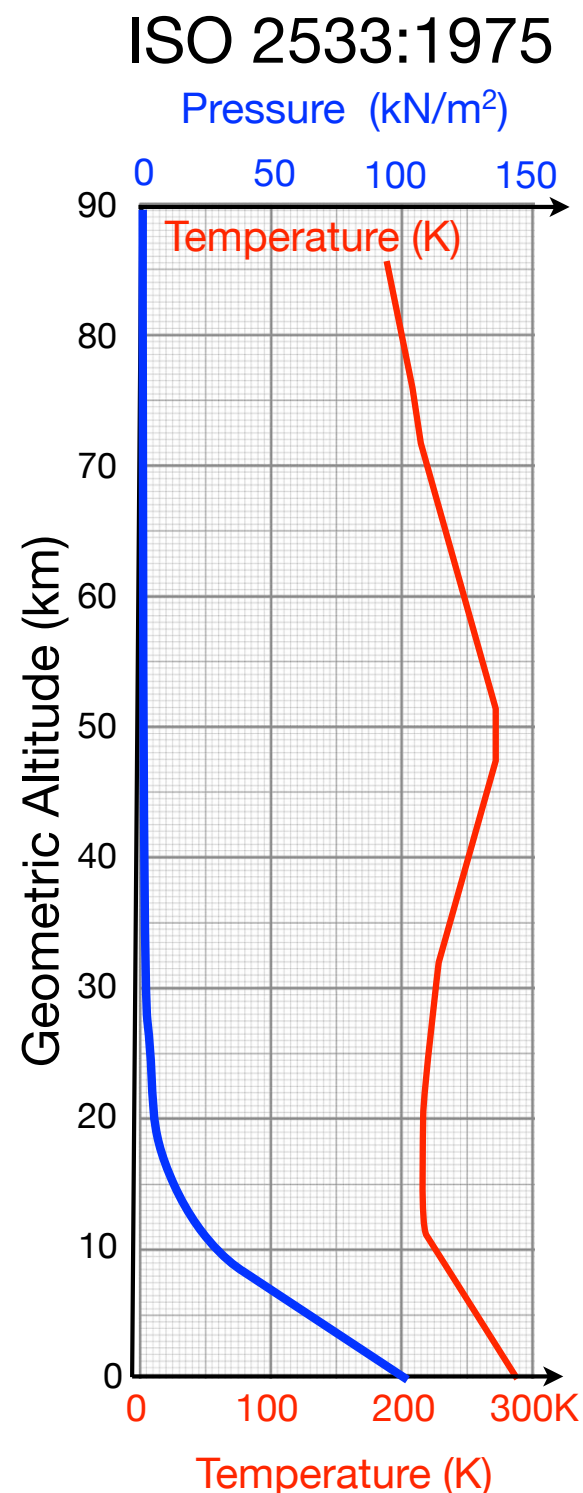
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Modeling

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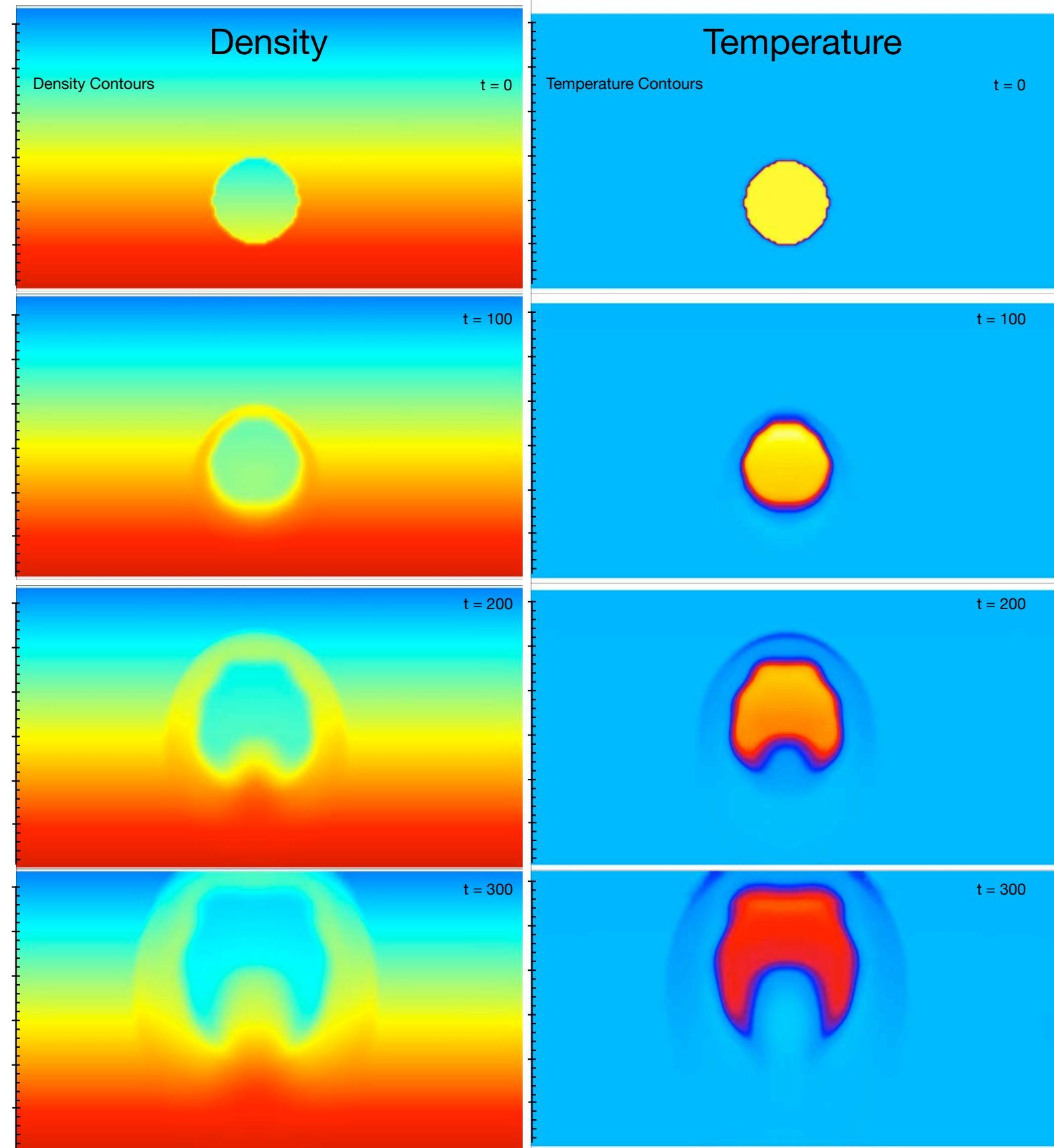
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Simple Buoyancy Test





Modeling

Inviscid scale-height atmosphere model in hydrostatic equilibrium

- Use 3D Euler eqs. in strong conservation law form, including body force due to gravity

$$\frac{d}{dt} \int_{\Omega} U dV + \oint_{\partial\Omega} (\mathbf{F} \cdot \hat{n}) dS = \int_{\Omega} S dV$$

- The state vector of conserved variables is

$$U = (\rho, \rho u, \rho v, \rho w, \rho E)^T$$

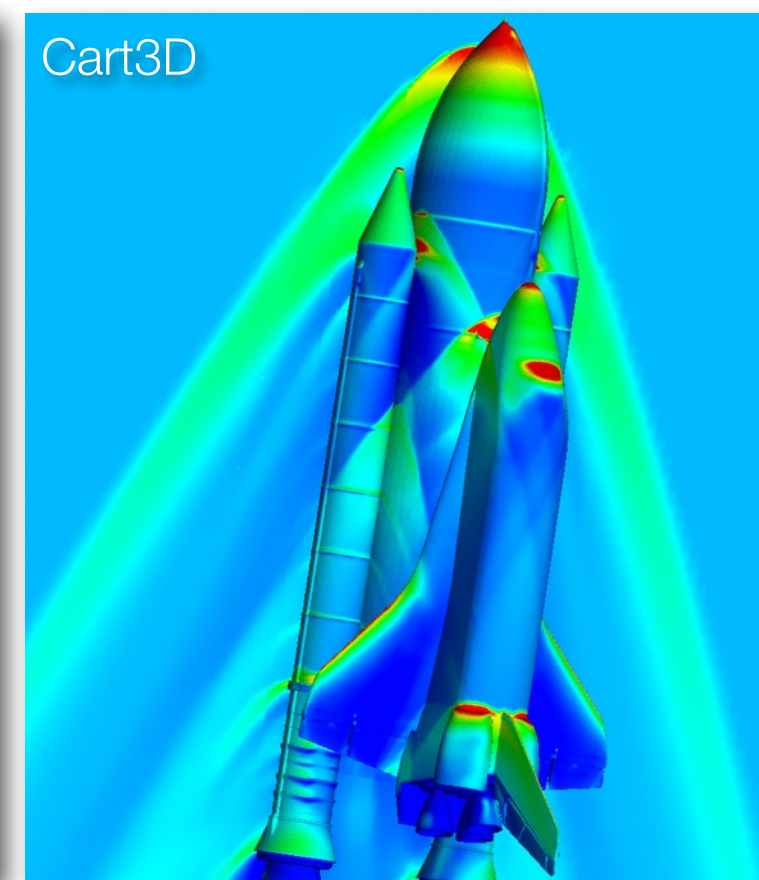
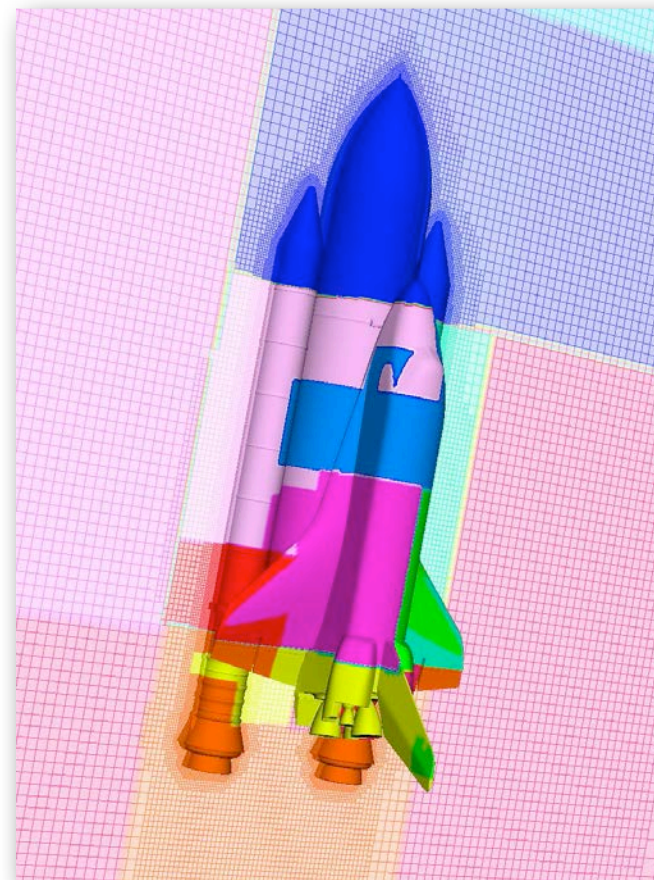
- Flux density tensor and gravitational body force term are

$$\mathbf{F} = \begin{pmatrix} \rho u & \rho v & \rho w \\ \rho u^2 + p & \rho uv & \rho uw \\ \rho uv & \rho v^2 + p & \rho vw \\ \rho uw & \rho vw & \rho w^2 + p \\ u(\rho E + p) & v(\rho E + p) & w(\rho E + p) \end{pmatrix} \quad S = \begin{pmatrix} 0 \\ 0 \\ 0 \\ -\rho g \\ -\rho w g \end{pmatrix}$$

Solver: Cart3D Overview

Production solver based on cut-cell Cartesian mesh method

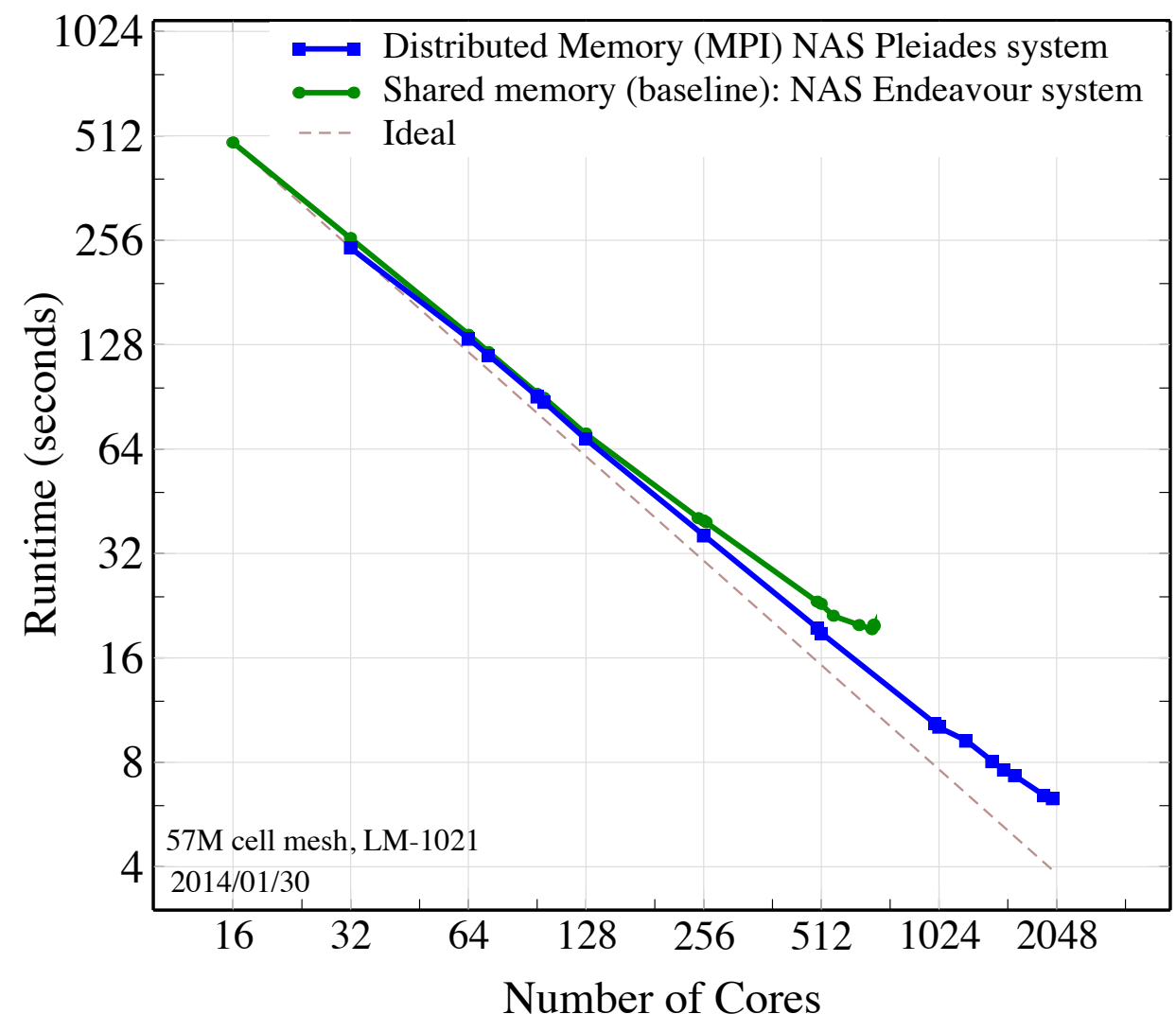
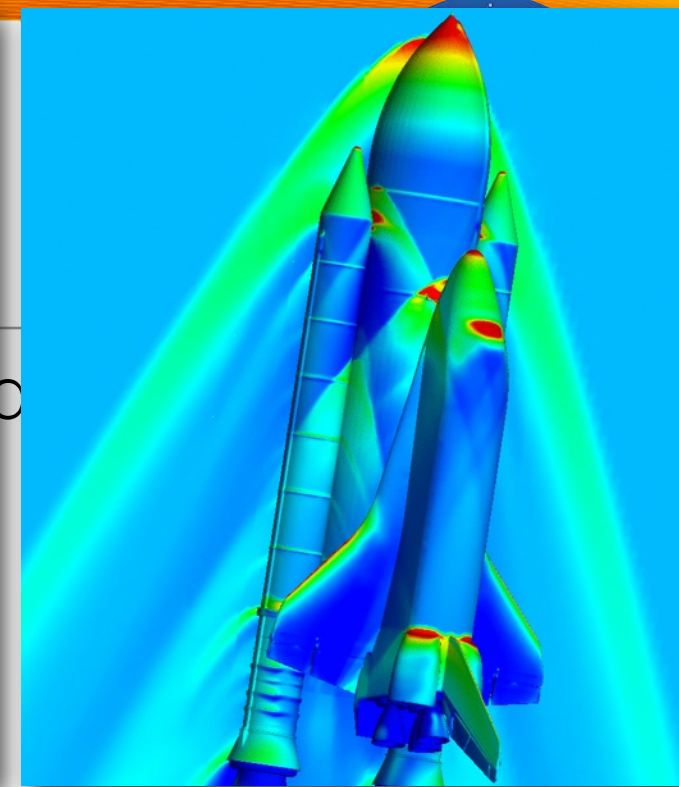
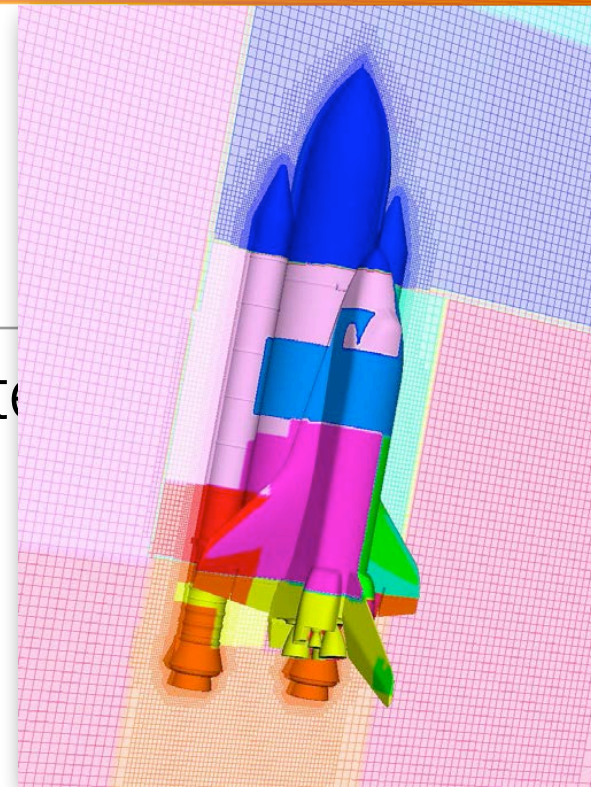
- Original development 1998-2002
- Fully-automated mesh generation for complex geometry
- Unstructured Cartesian cells
- Fully-conservative finite-volume method
- Multigrid accelerated 2nd-order upwind scheme
- Excellent scalability through domain decomposition
- Broad use throughout NASA, US Government and industry
 - Over 500 users in aerospace community
 - One of NASAs most heavily used production solvers, large validation database



Solver: Cart3D Overview

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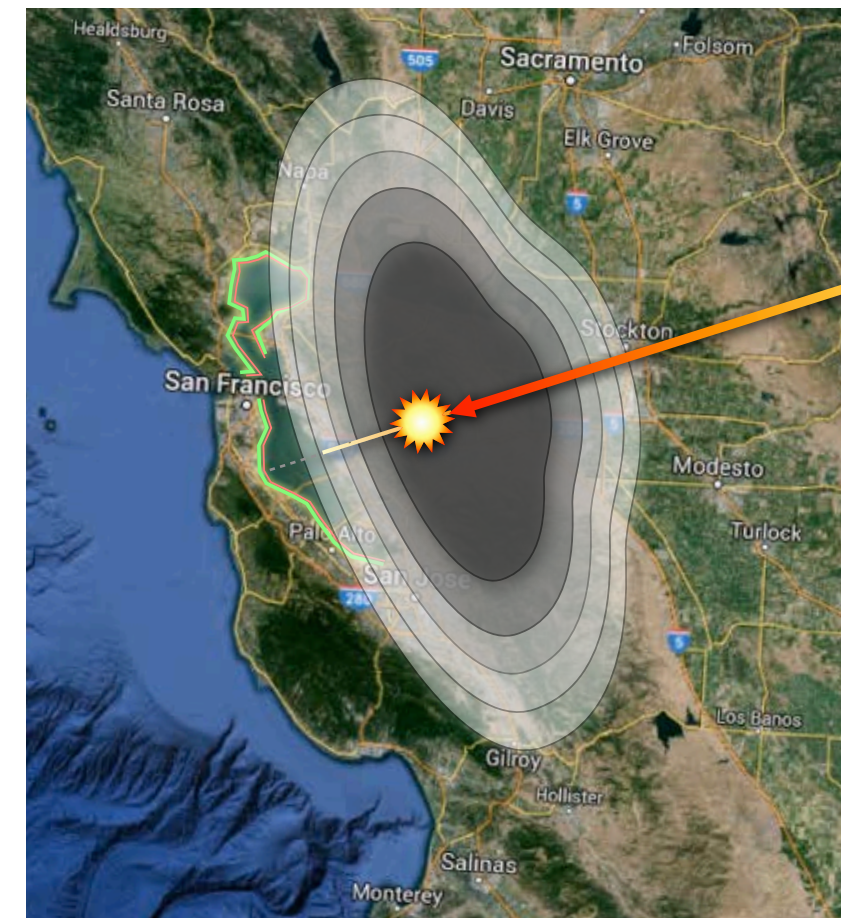
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Deposition of Mass, Momentum & Energy

Goal is accurate prediction of surface effects from energy deposition inputs

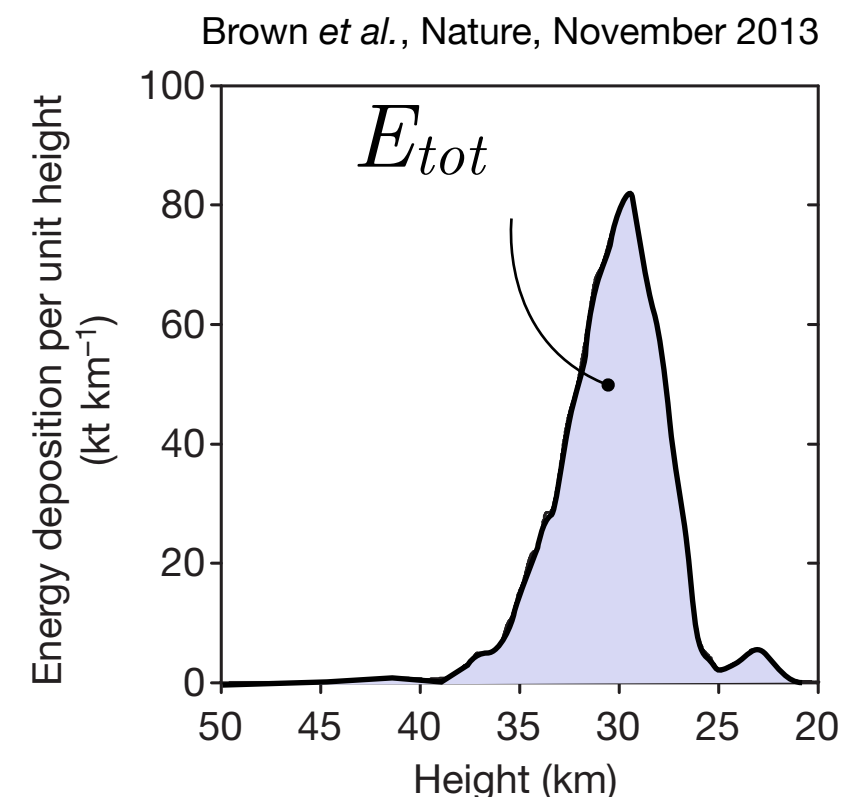
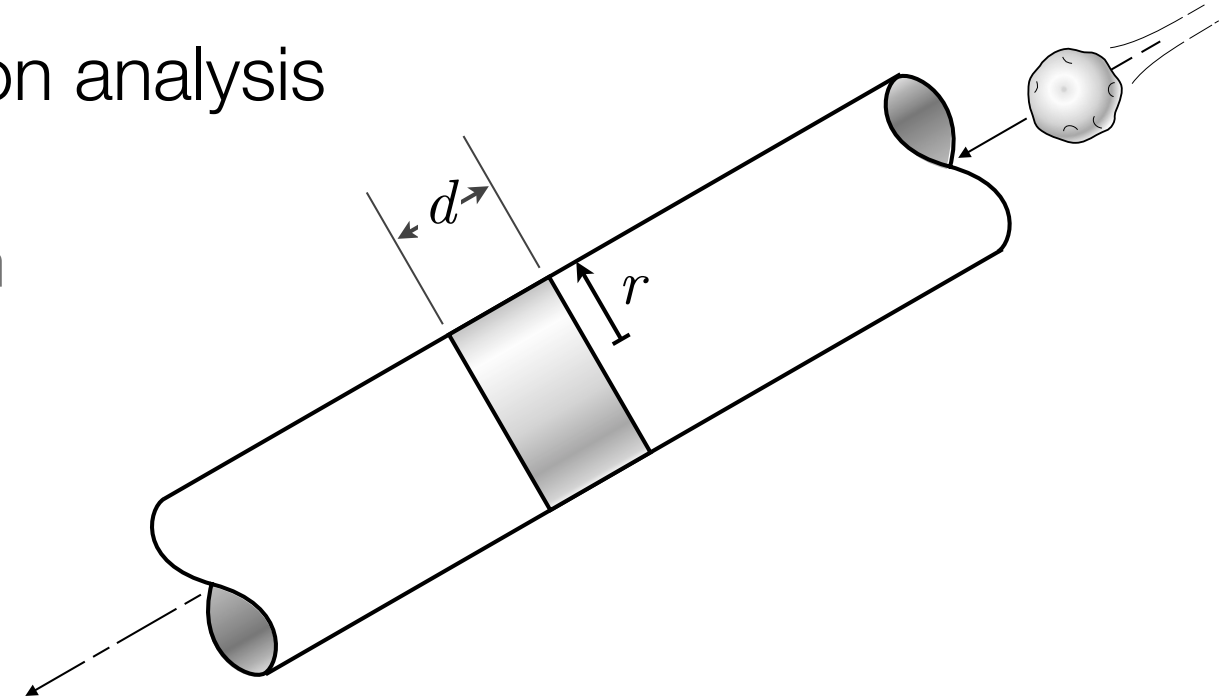
- Focus on ground footprint, not near-field physics
- Abstract entry physics as simply sources of mass, momentum & energy
- Drive simulations via deposition profile taken from:
 - Models (e.g. ReVelle, Cepulecha, H&G, Shuvalov)
 - Simulations (Task 2, CTH, ALE3D, Shuvalov, Boslough)
 - Light-curve derived profiles (Jenniskins, Popova)
 - Infrasound based energy deposition (Brown, ReVelle)
- Need to derive source terms from deposition profiles



Deposition of Mass, Momentum & Energy

Derive source terms through conservation analysis

- Release energy, mass and momentum into a corridor of known radius, r
- Over each time step, Δt , the meteor travels a distance d
- Given: energy deposition profile as a function of altitude
 - From modeling
 - From simulation
 - From observational data

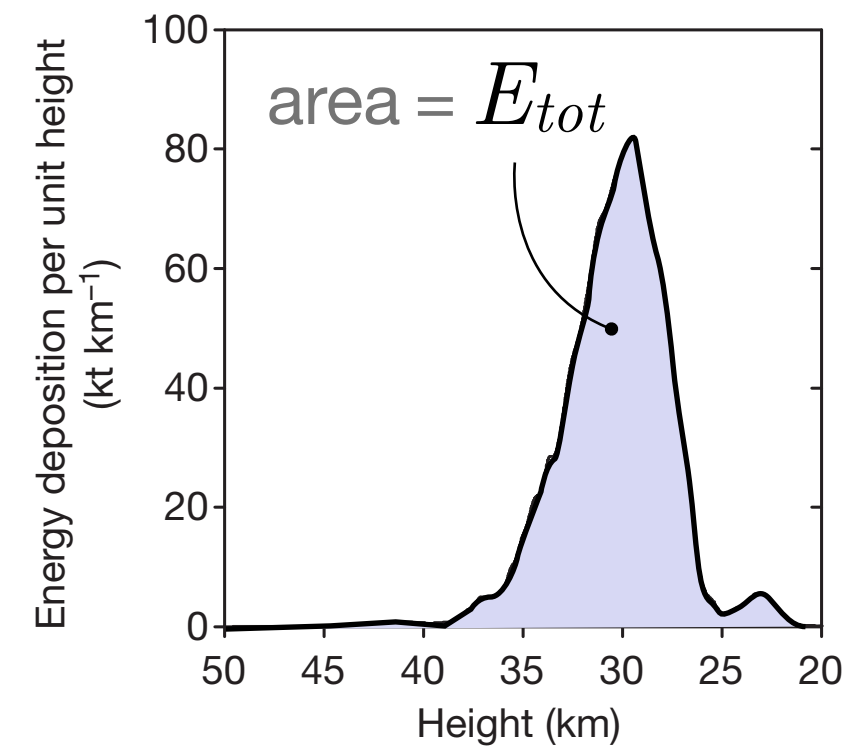


Deposition of Mass, Momentum & Energy

Conservation of energy

- Given energy deposition we know the total energy released is area under profile

$$E_{tot} = \int \frac{dE}{dh} dh \quad (+ \text{ radiation })$$



Deposition of Mass, Momentum & Energy

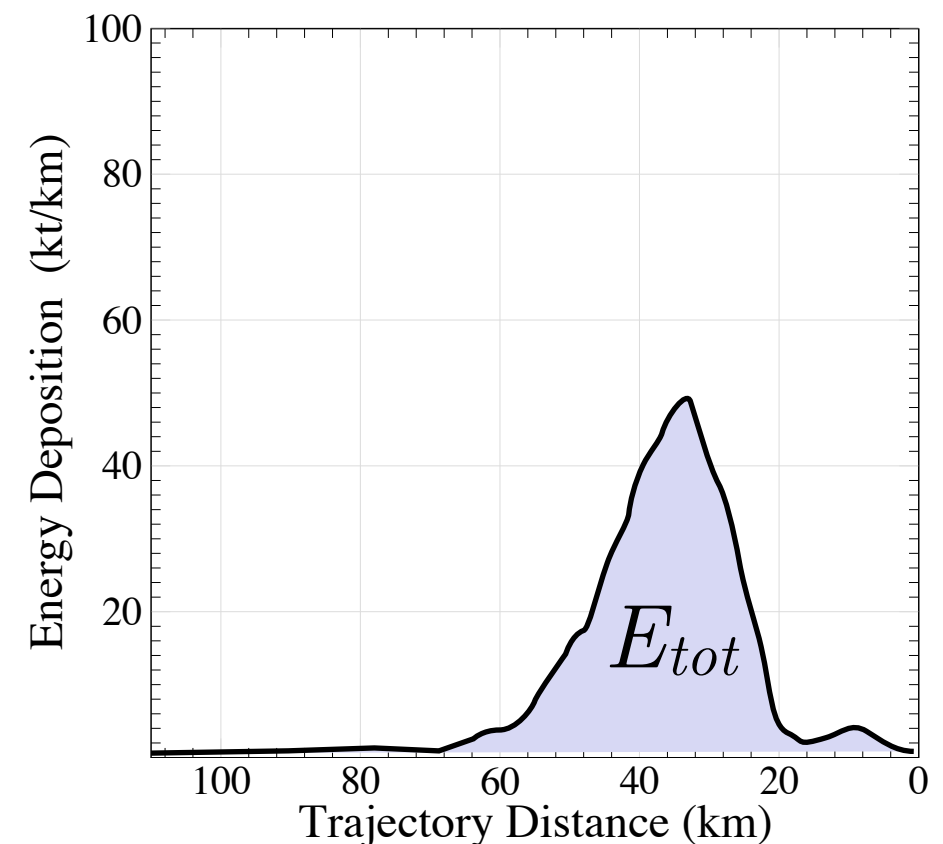
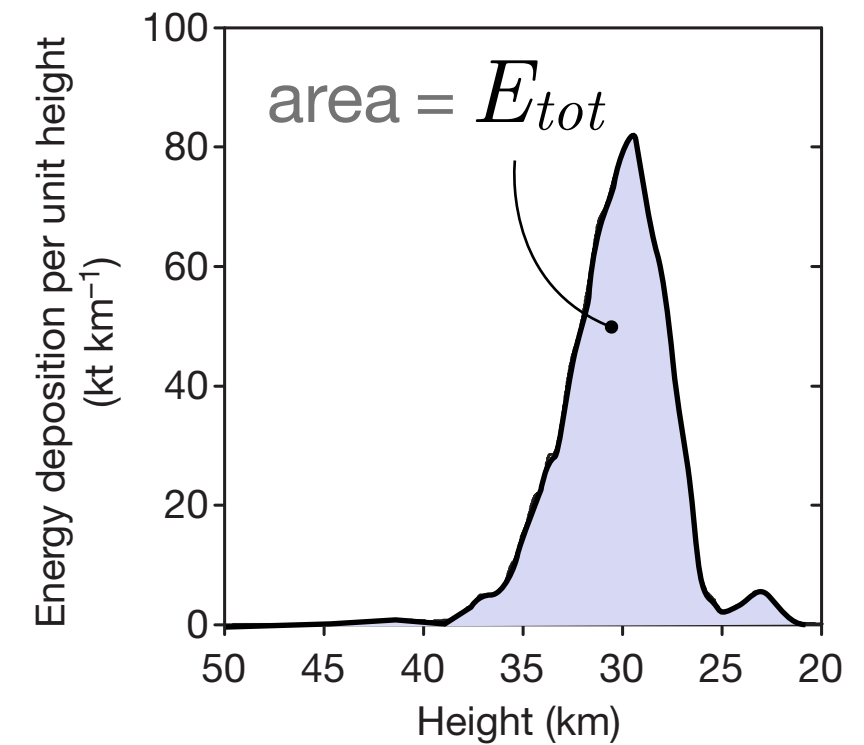
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Deposition of Mass, Momentum & Energy

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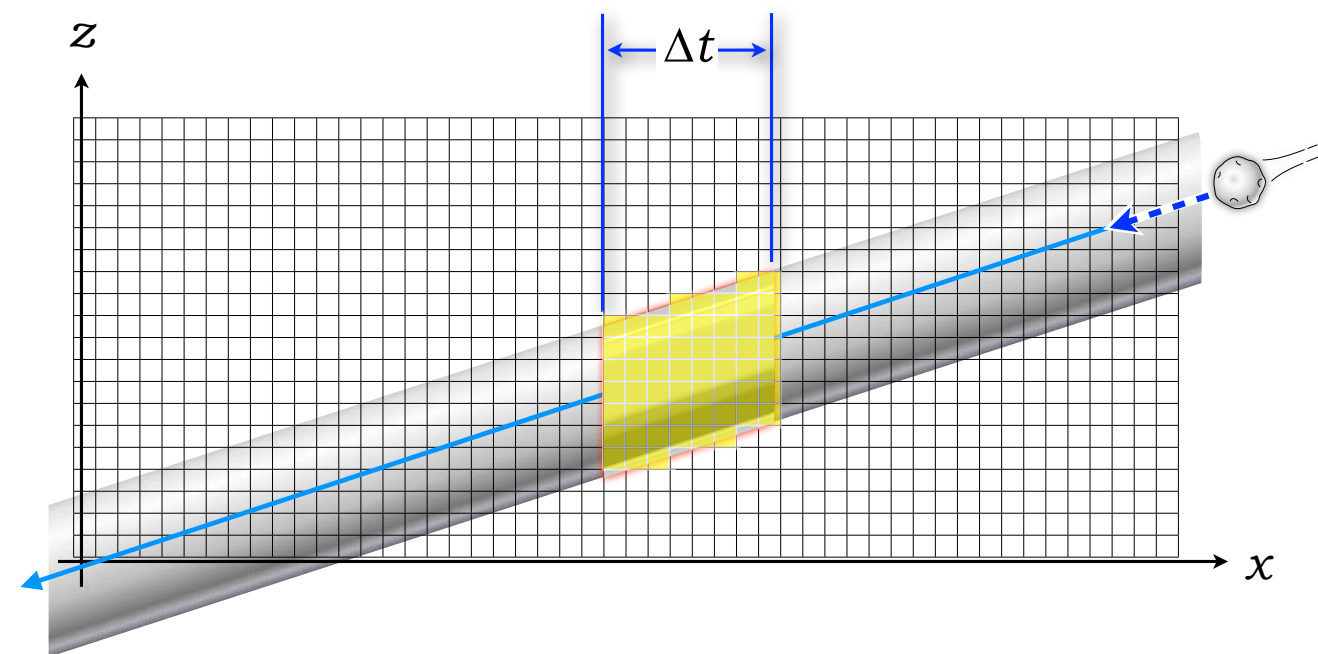
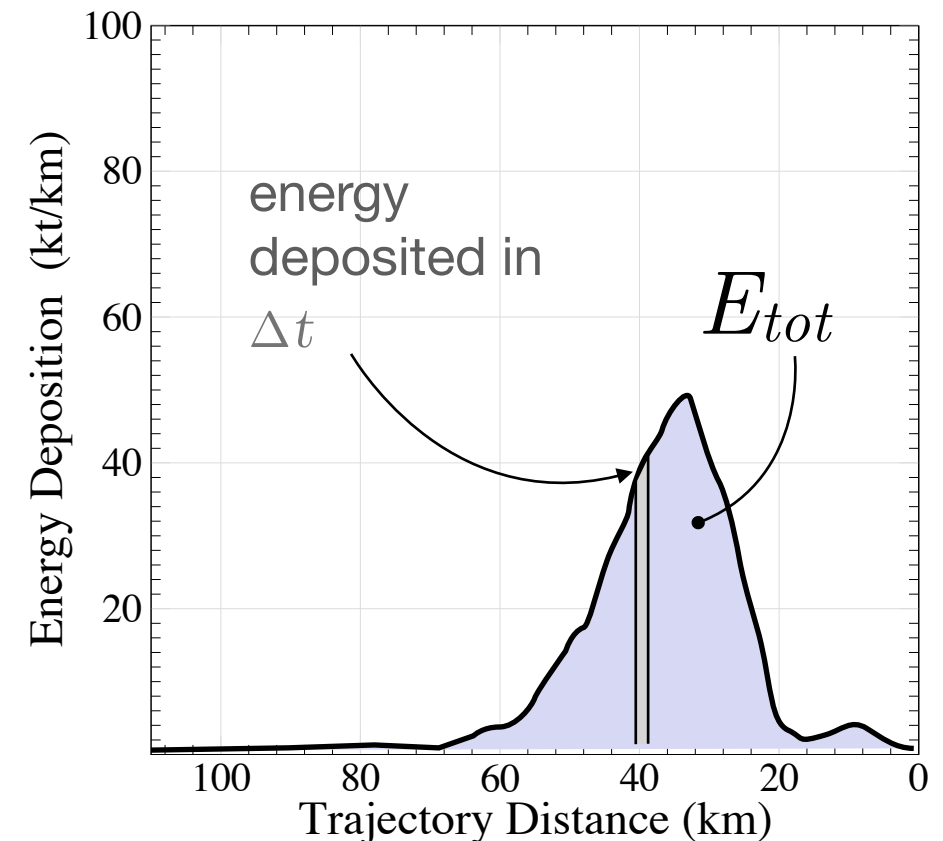
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- This energy gets released into the mesh cells which intersect the tube surrounding the meteor at each time step, Δt



Deposition of Mass, Momentum & Energy

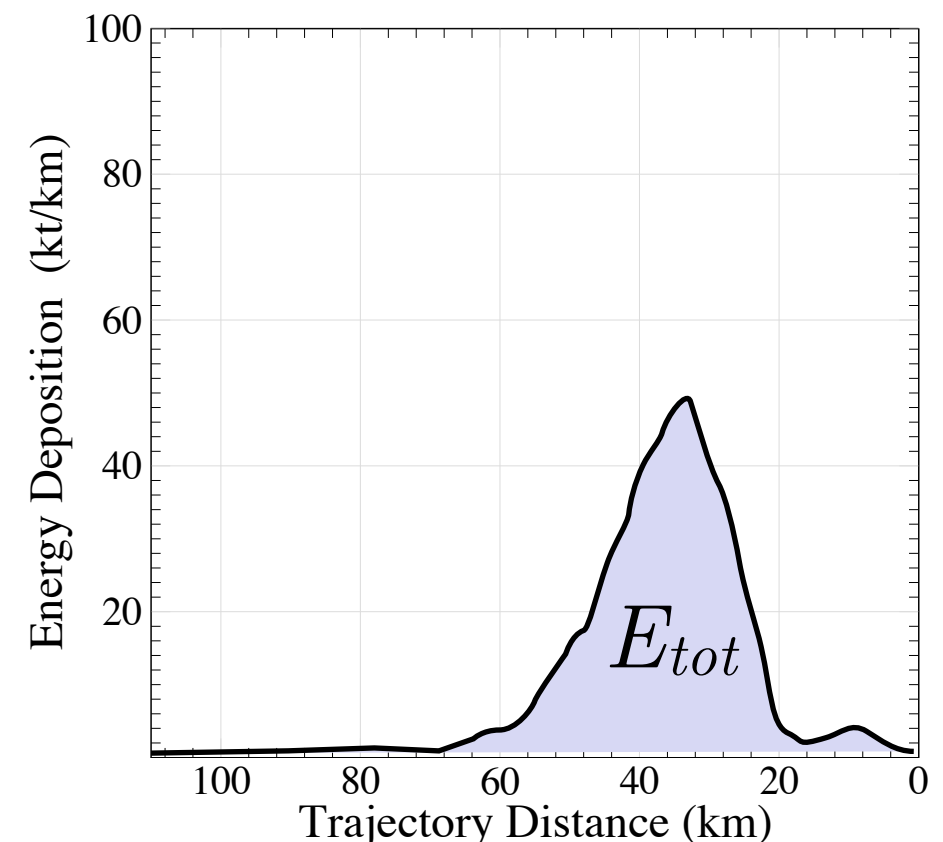
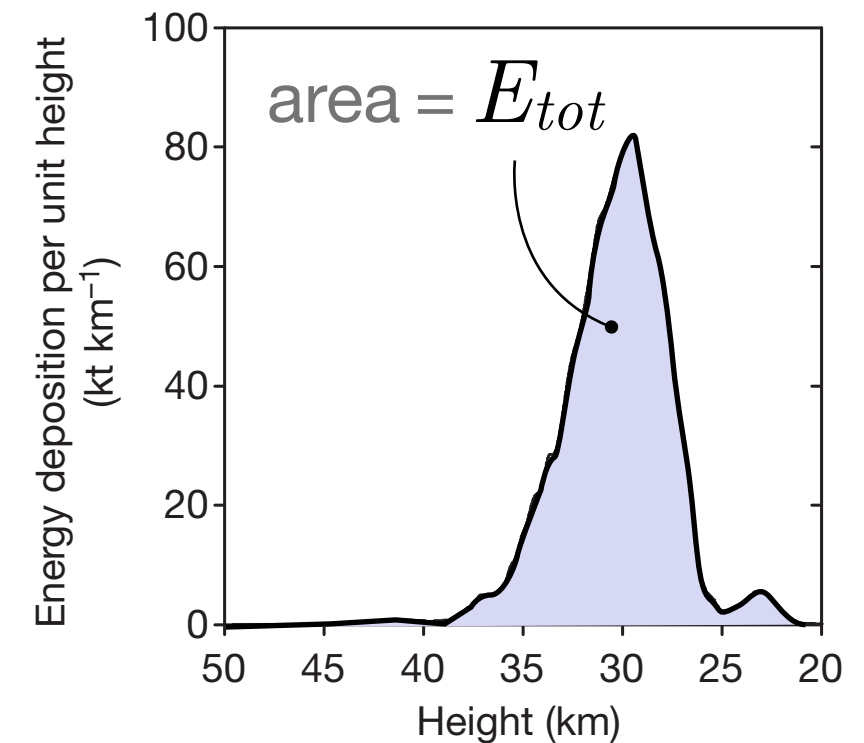
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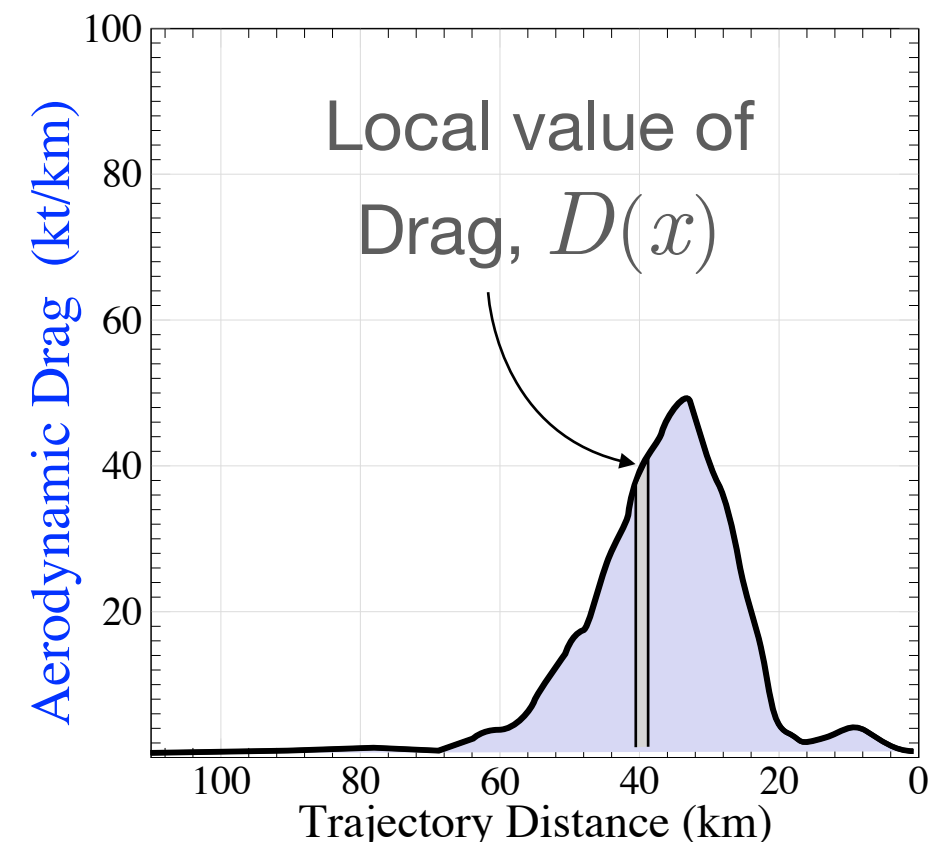
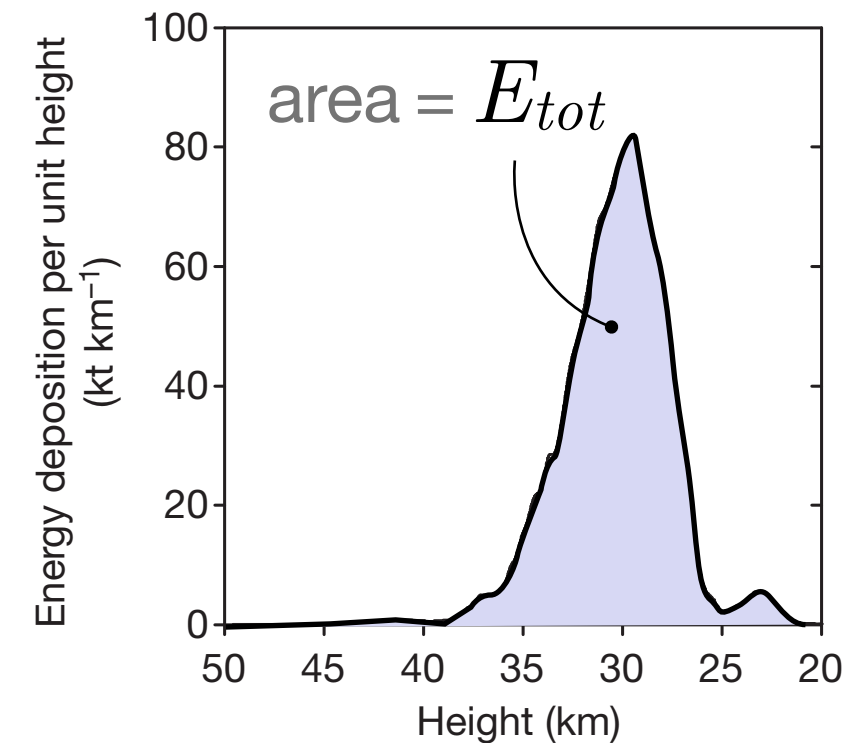
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- For known entry angle, can rescale profile to be energy released along trajectory, x

$$E_{tot} = \int \frac{dE}{dx} dx$$

- Since work = (force x distance), and aerodynamic drag is doing all the work, this profile is identically drag along the trajectory

$$E_{tot} = \int \frac{dE}{dx} dx = \int D(x) dx$$



Deposition of Mass, Momentum & Energy

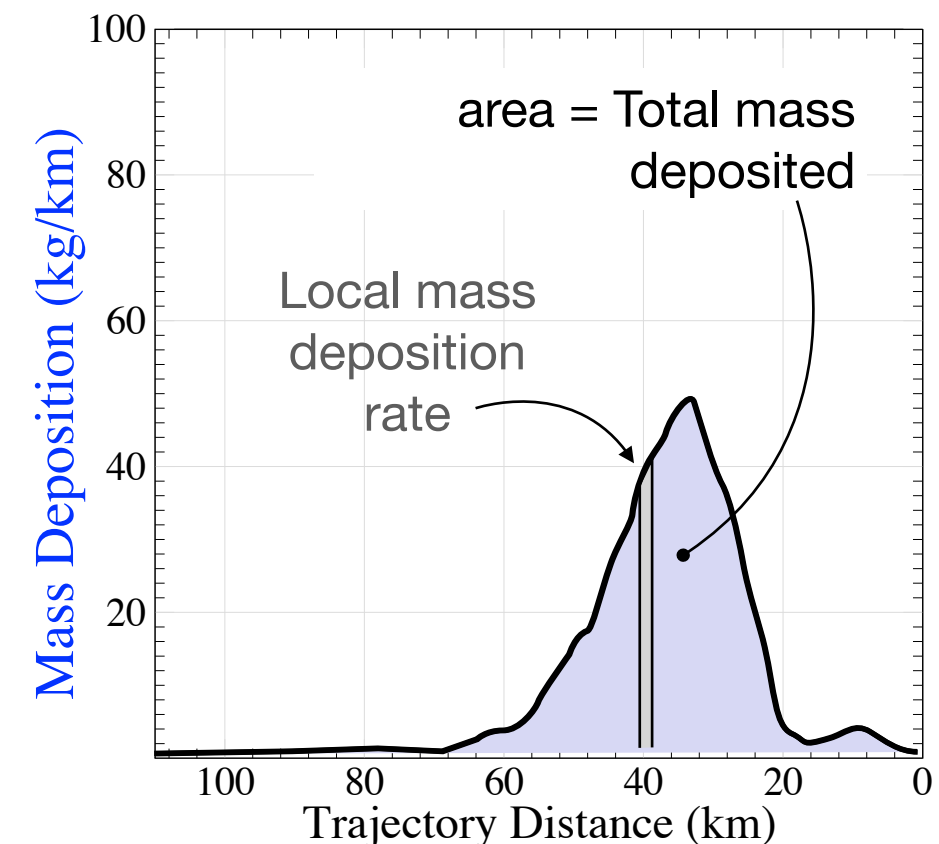
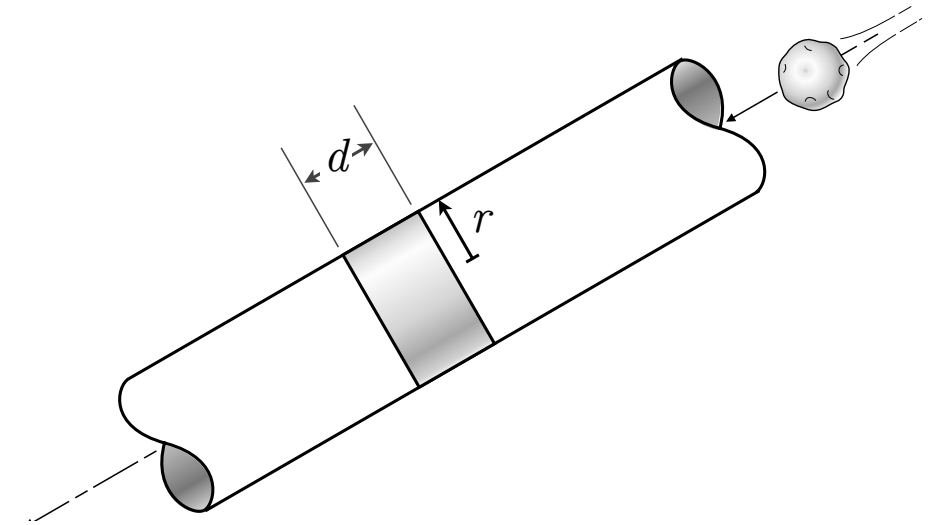
Conservation of mass & momentum

- Mass loss equation $\frac{dM}{dt} = -\sigma C_D S_m \frac{1}{2} \rho_{\text{air}} U_m^3$

- Recall that aerodynamic drag is

$$D = C_D S_m q_\infty \quad \text{with} \quad q_\infty = \frac{1}{2} \rho_{\text{air}} U_m^2$$

- So mass loss is simply $\frac{dM}{dt} = -\sigma D U_m$



Deposition of Mass, Momentum & Energy

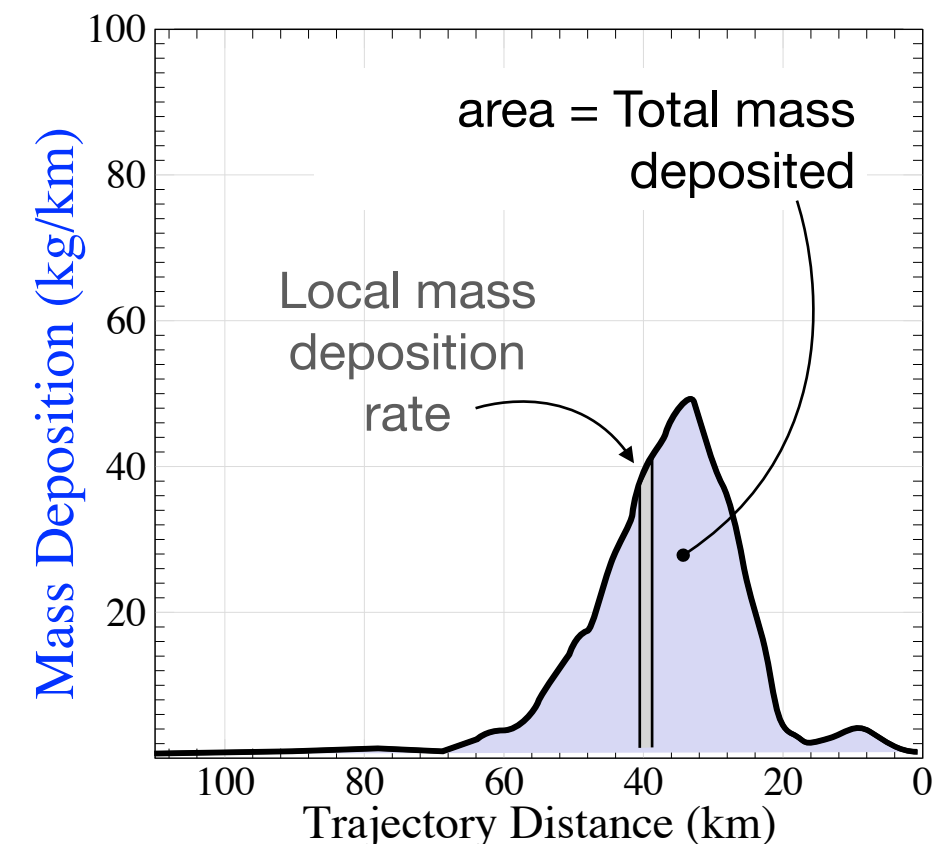
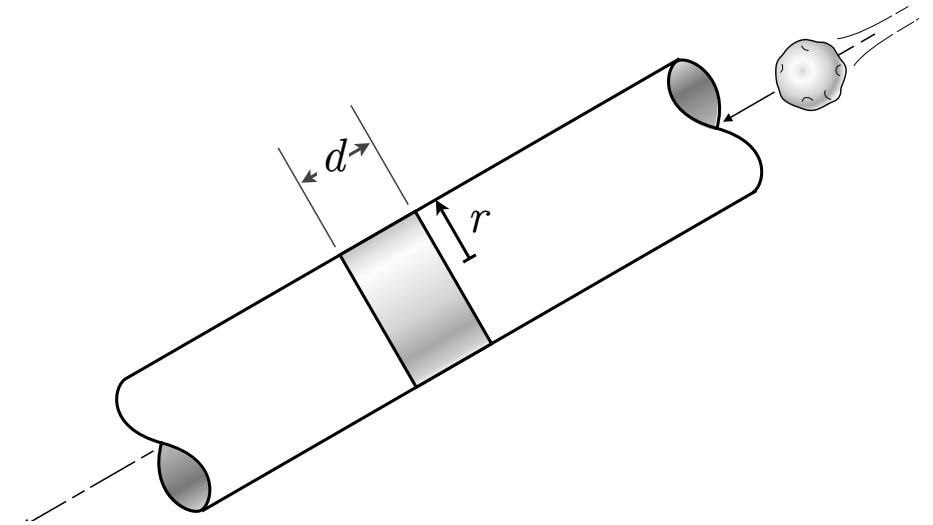
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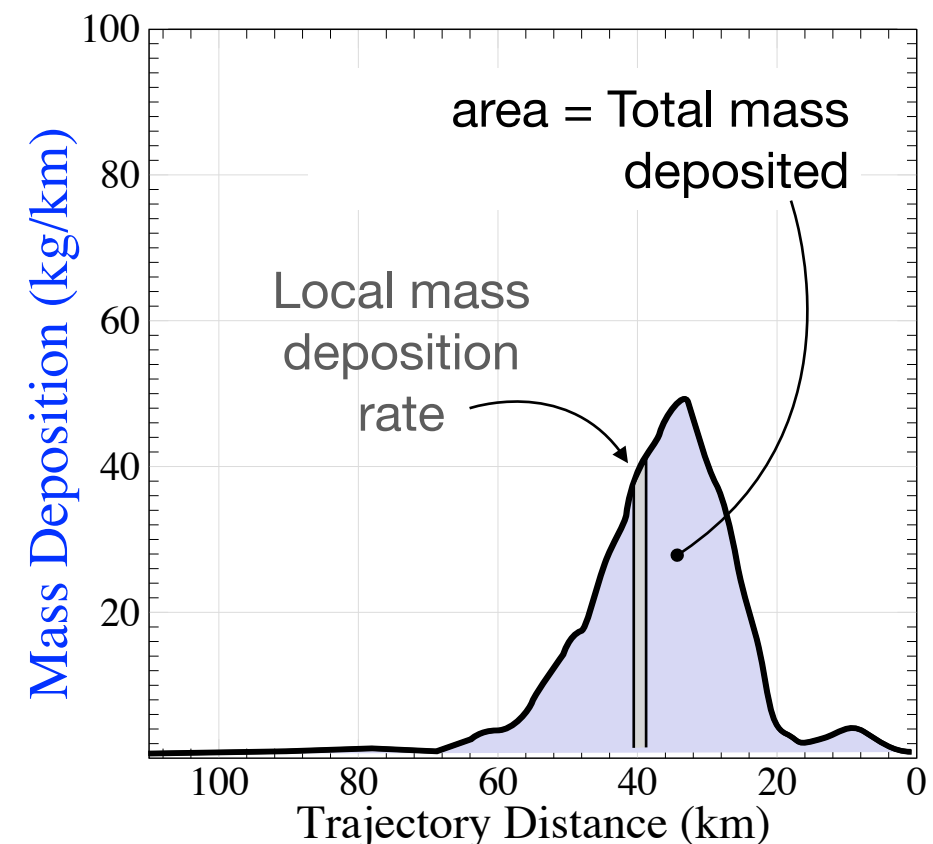
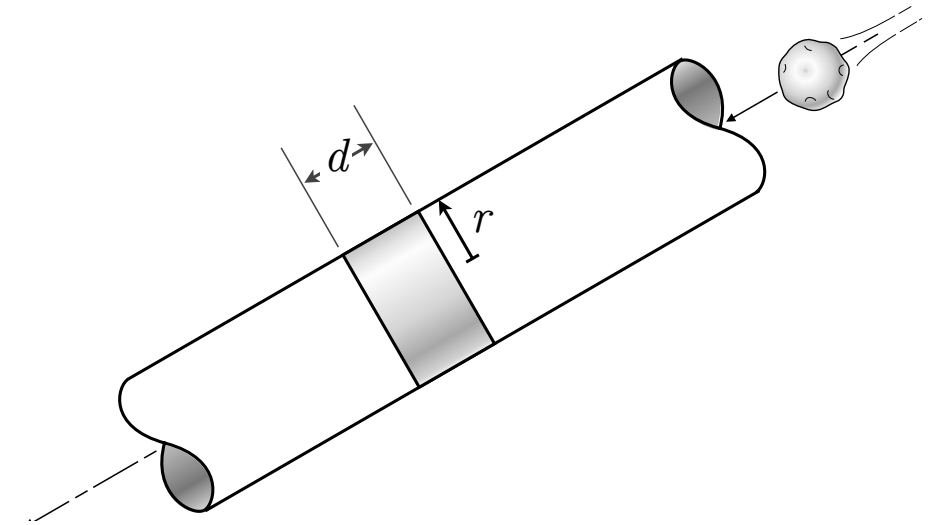
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- Assuming constant U_m and σ , local deposition of mass scales directly with Drag



Deposition of Mass, Momentum & Energy

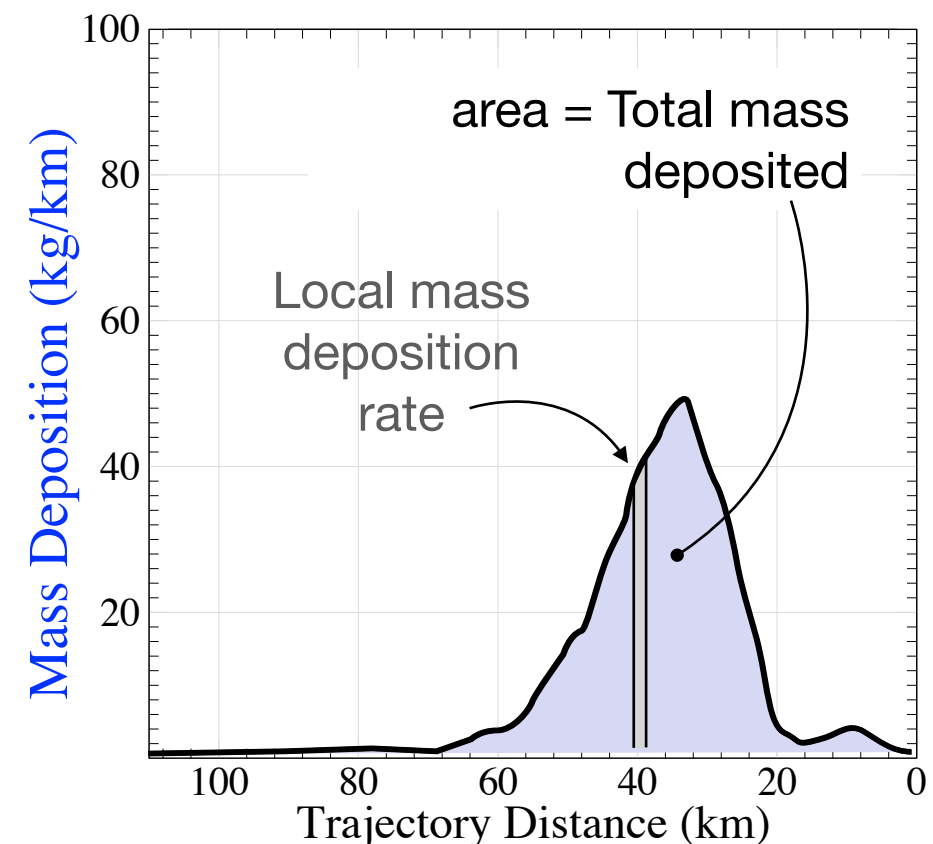
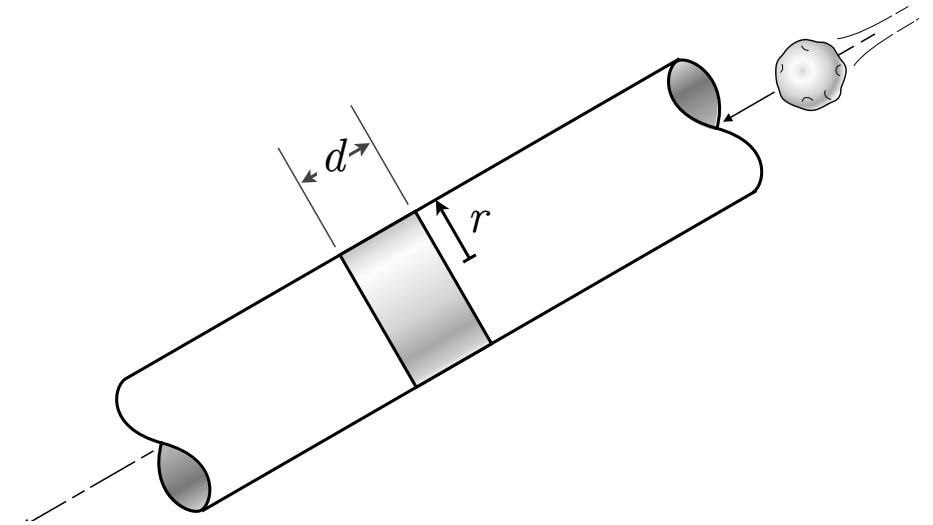
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- So mass loss is simply $\frac{dM}{dt} = -\sigma D U_m$
- Assuming constant U_m and σ , local deposition of mass scales directly with Drag
- Area under profile is total mass deposited ($M_{\text{entry}} - M_{\text{GroundFragments}}$)
- From mass deposition and velocity, we also know momentum deposition





Overview

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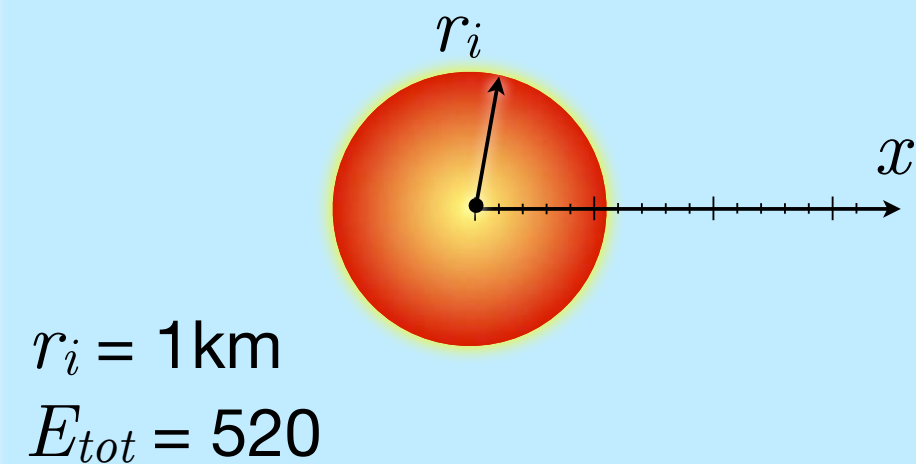
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 - Basic – Spherical charge examples
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Basic Verification & Validation

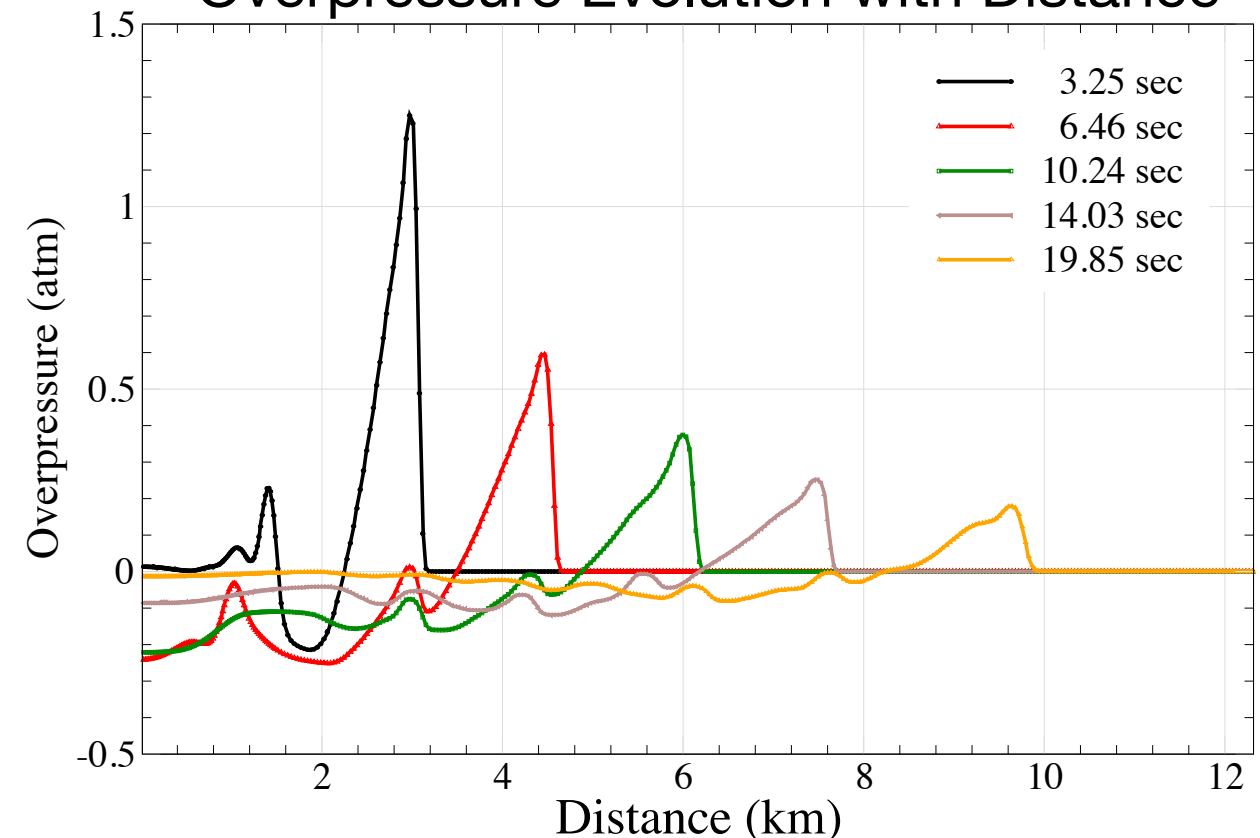
Blast from a spherical charge

- Static spherical charge with
 - No buoyancy
 - $E_{tot} = 520$ kt,
 - Initial radius, $r_i = 1$ km
- Classical refs.
 - Brode, H. L., Blast wave from a spherical charge, J. Phys. Fluids. (1959)
 - D. L. Jones. Intermediate strength blast wave. Physics of Fluids (1968)

Setup



Overpressure Evolution with Distance

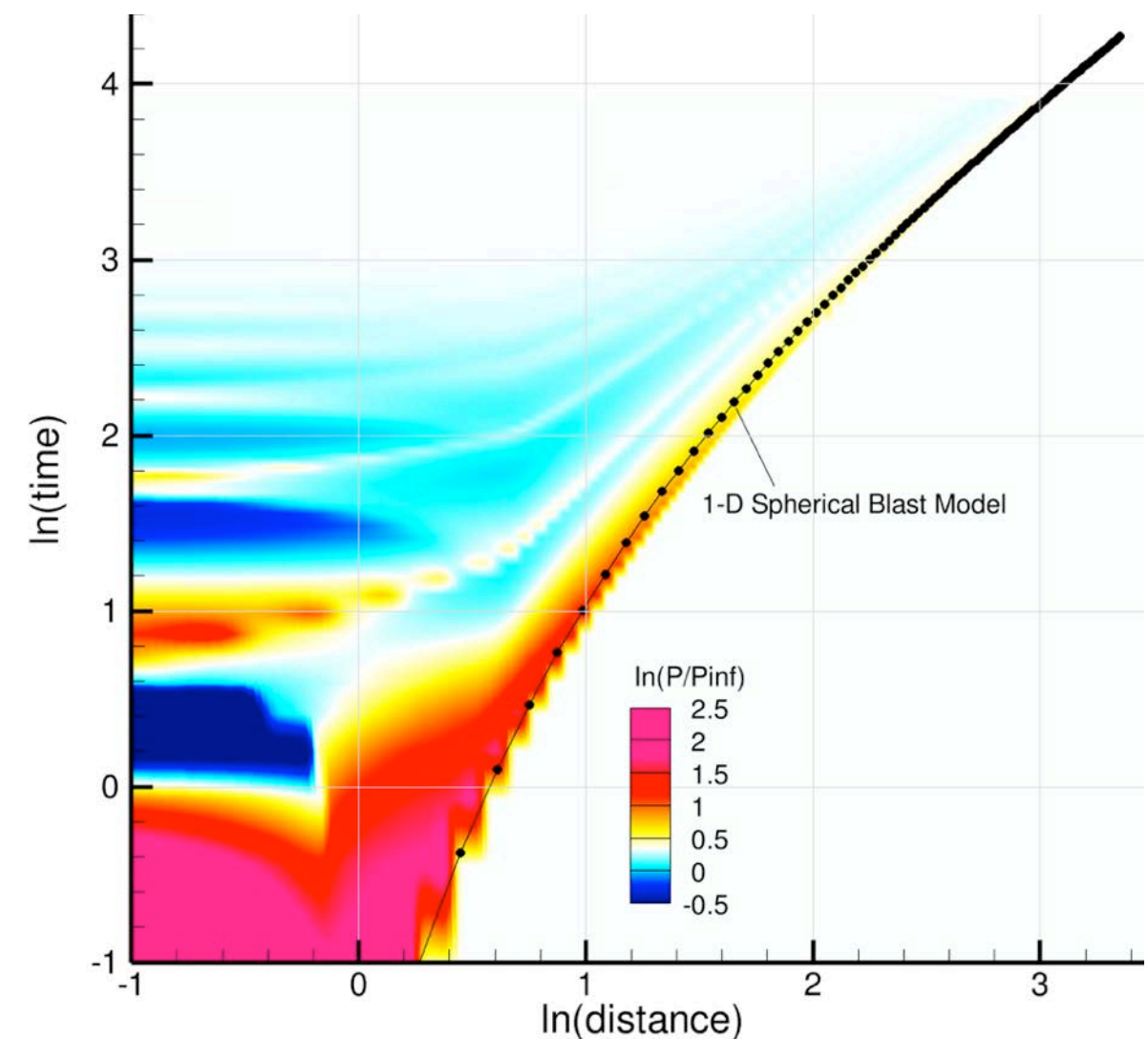
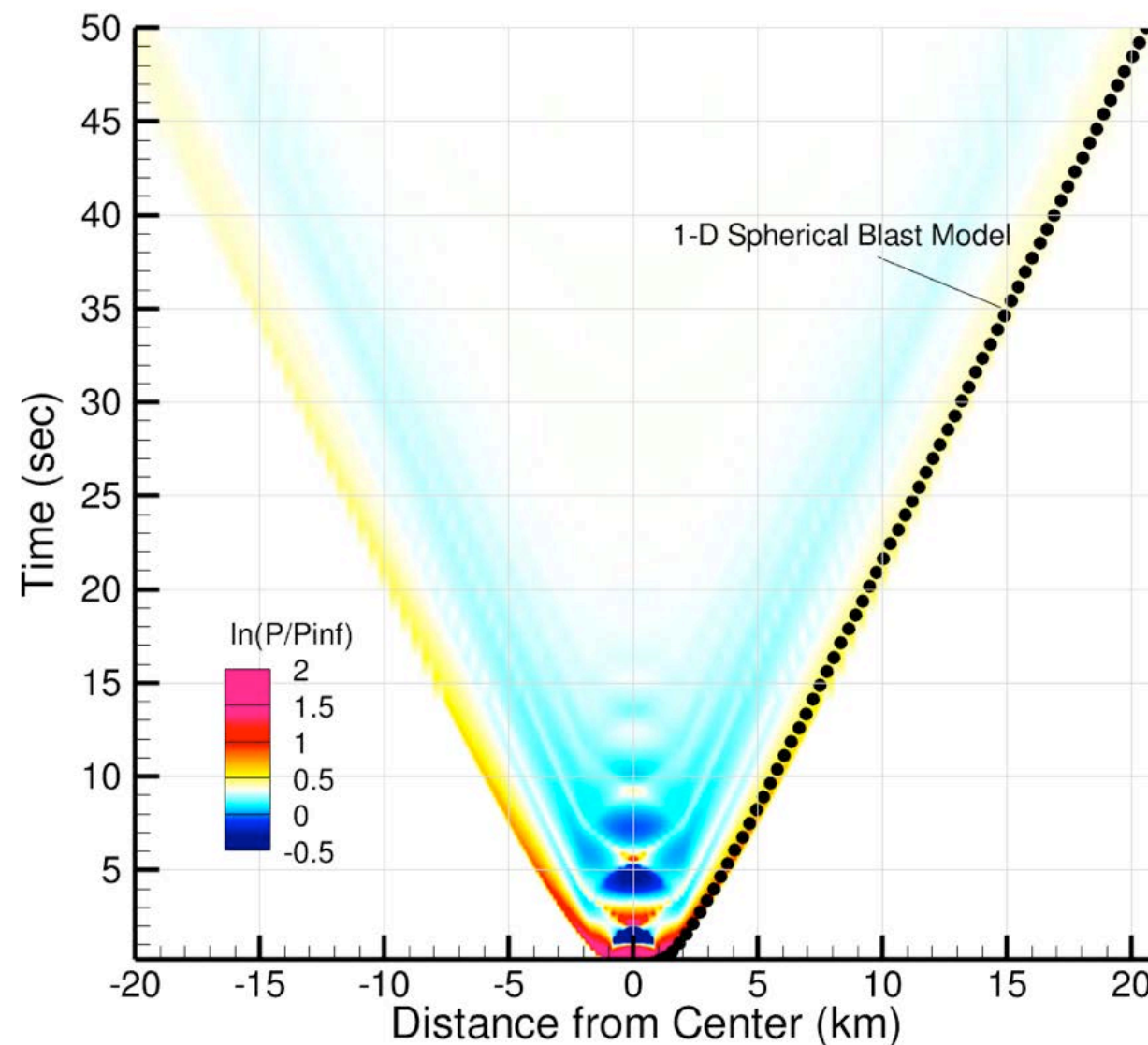


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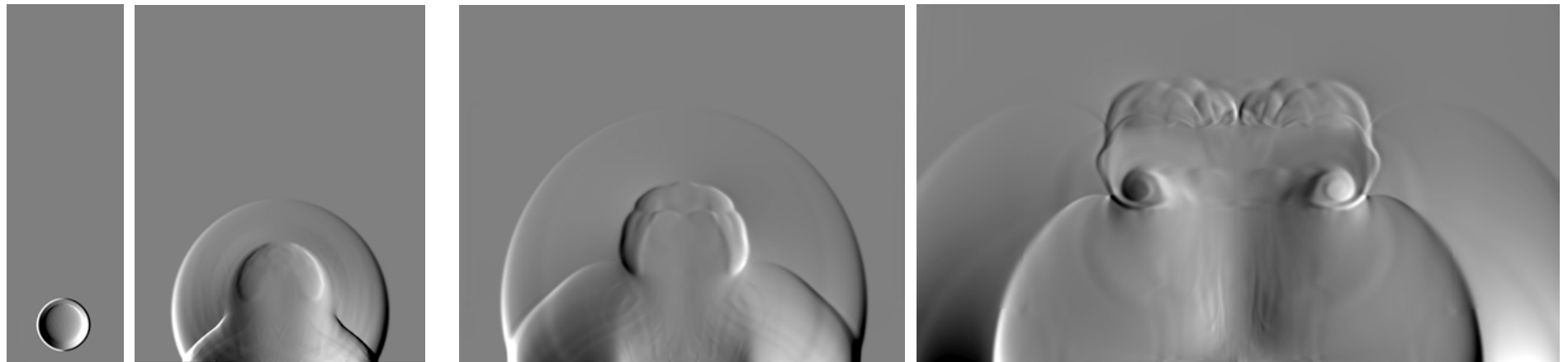
Space-time overpressure evolution



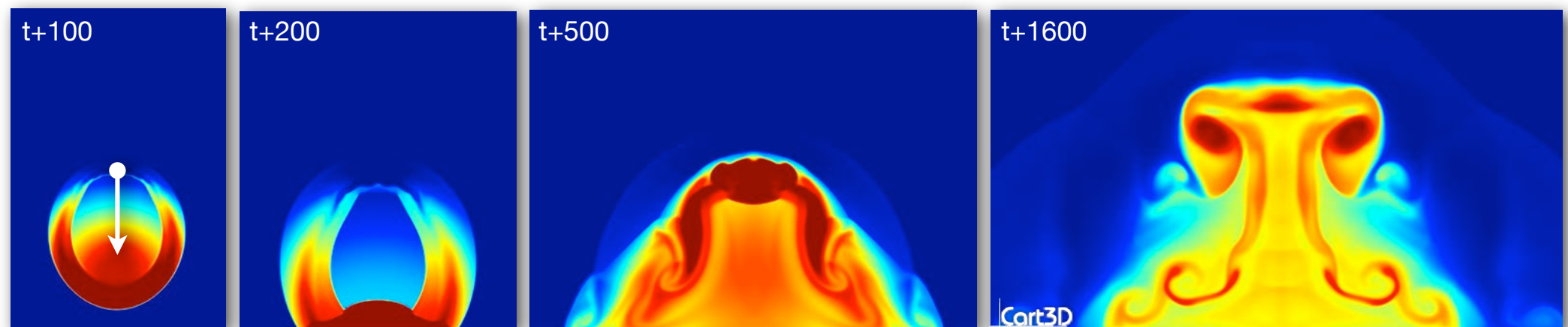
Basic Verification & Validation

Blasts over ground plane

- Numerous examples static and moving blasts over ground plane with buoyancy
 - Static airburst with buoyancy



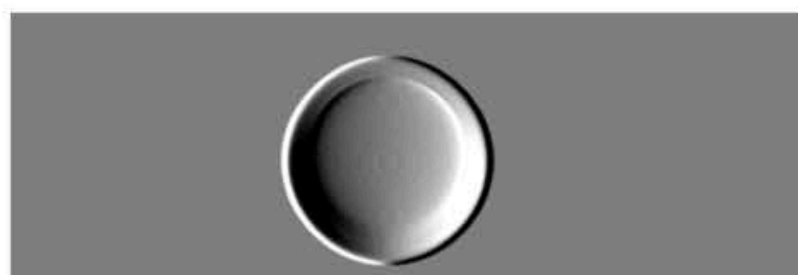
- Moving airburst



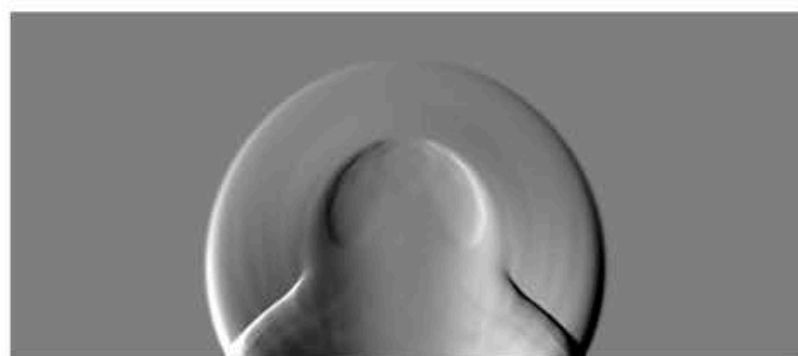
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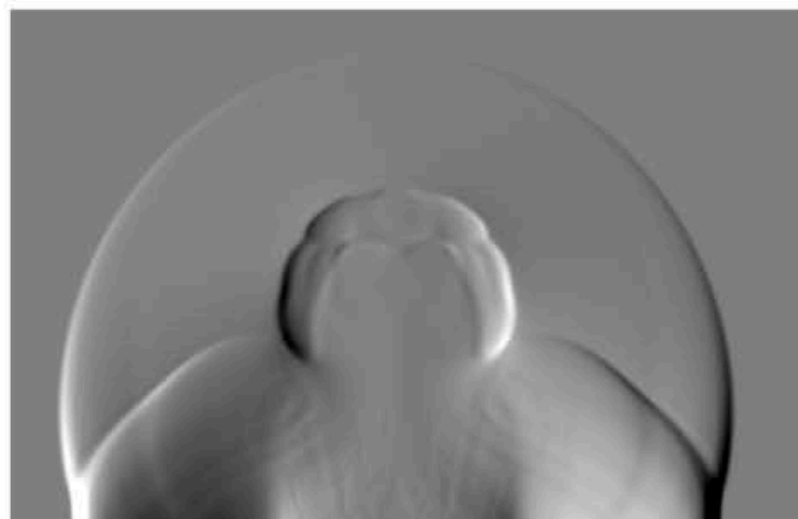
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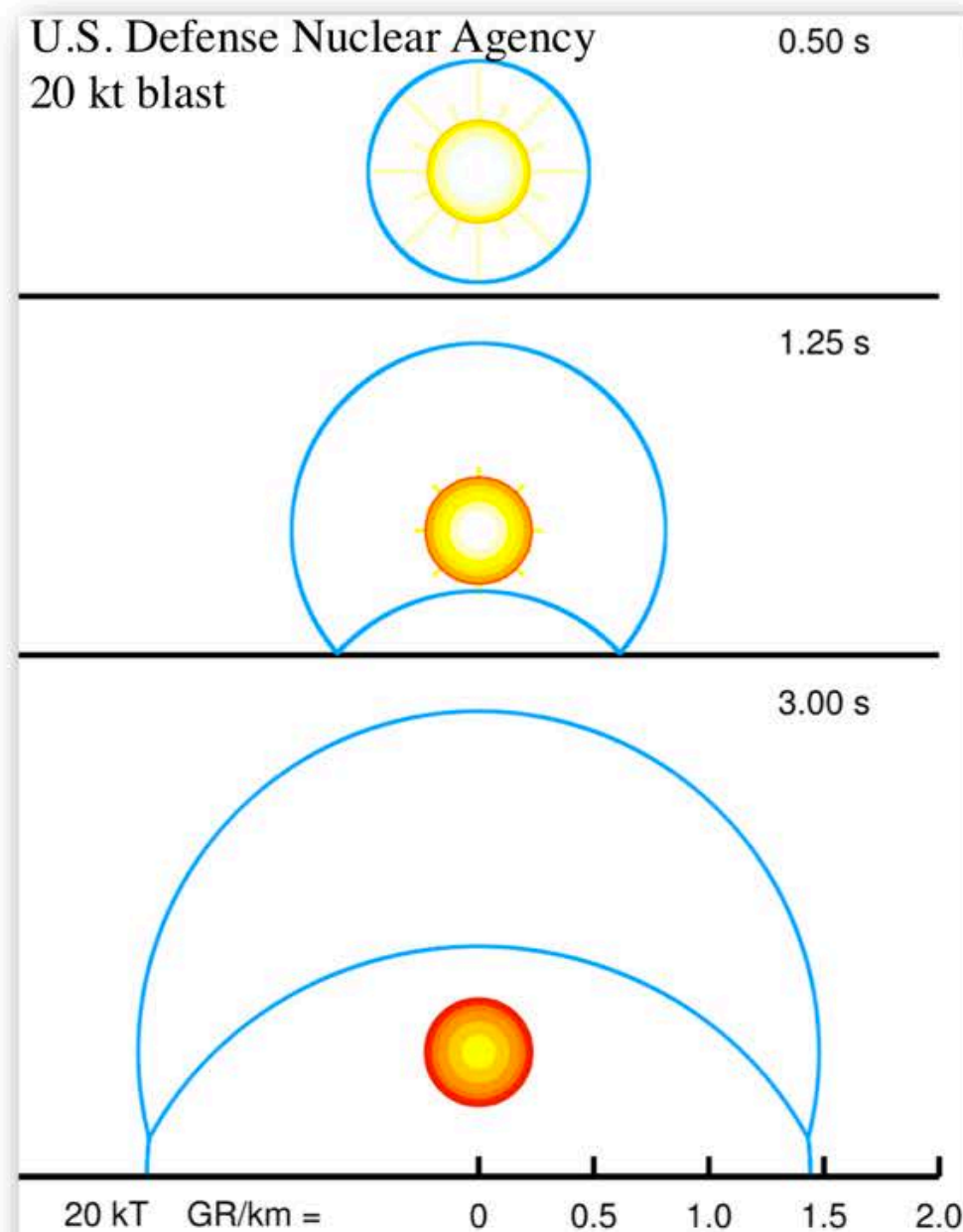
Spherical
airburst



Simple shock
reflection



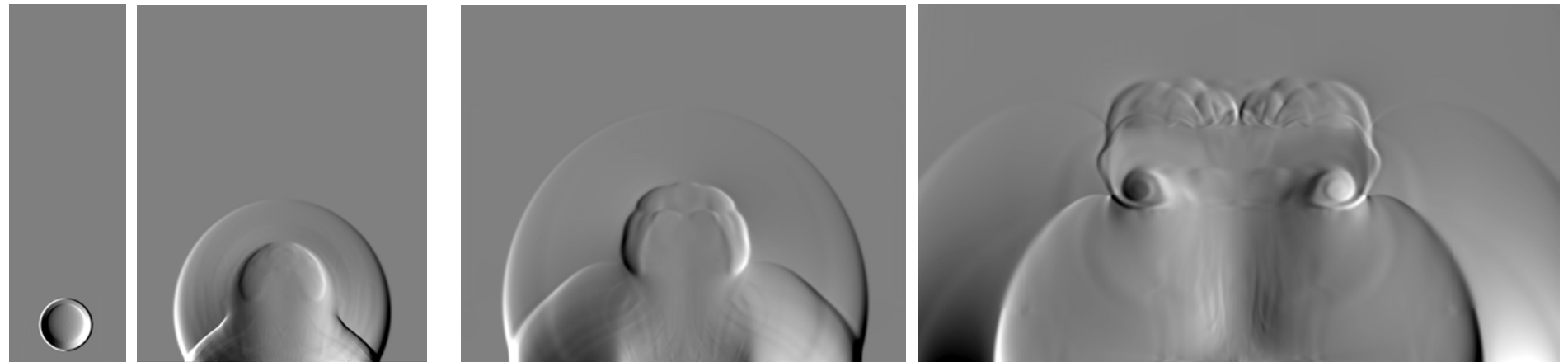
Mach stem
formation



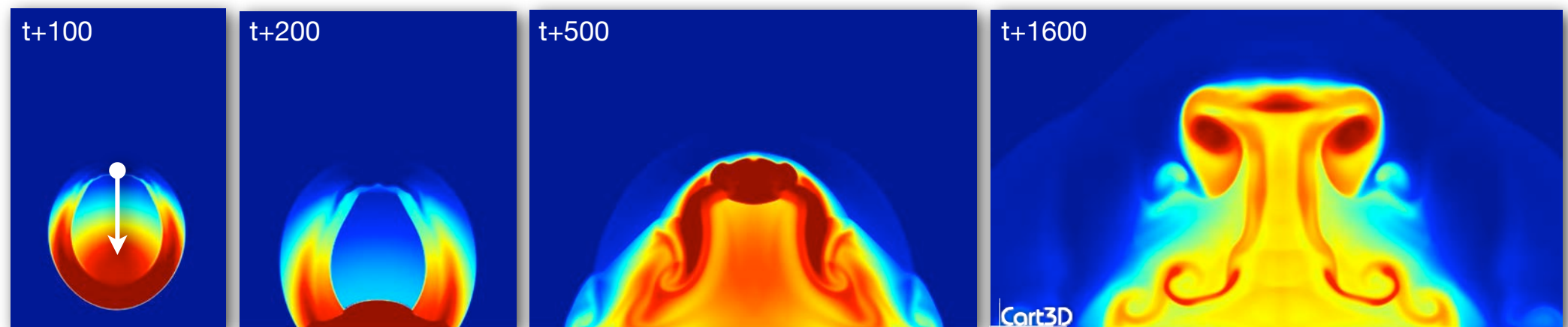
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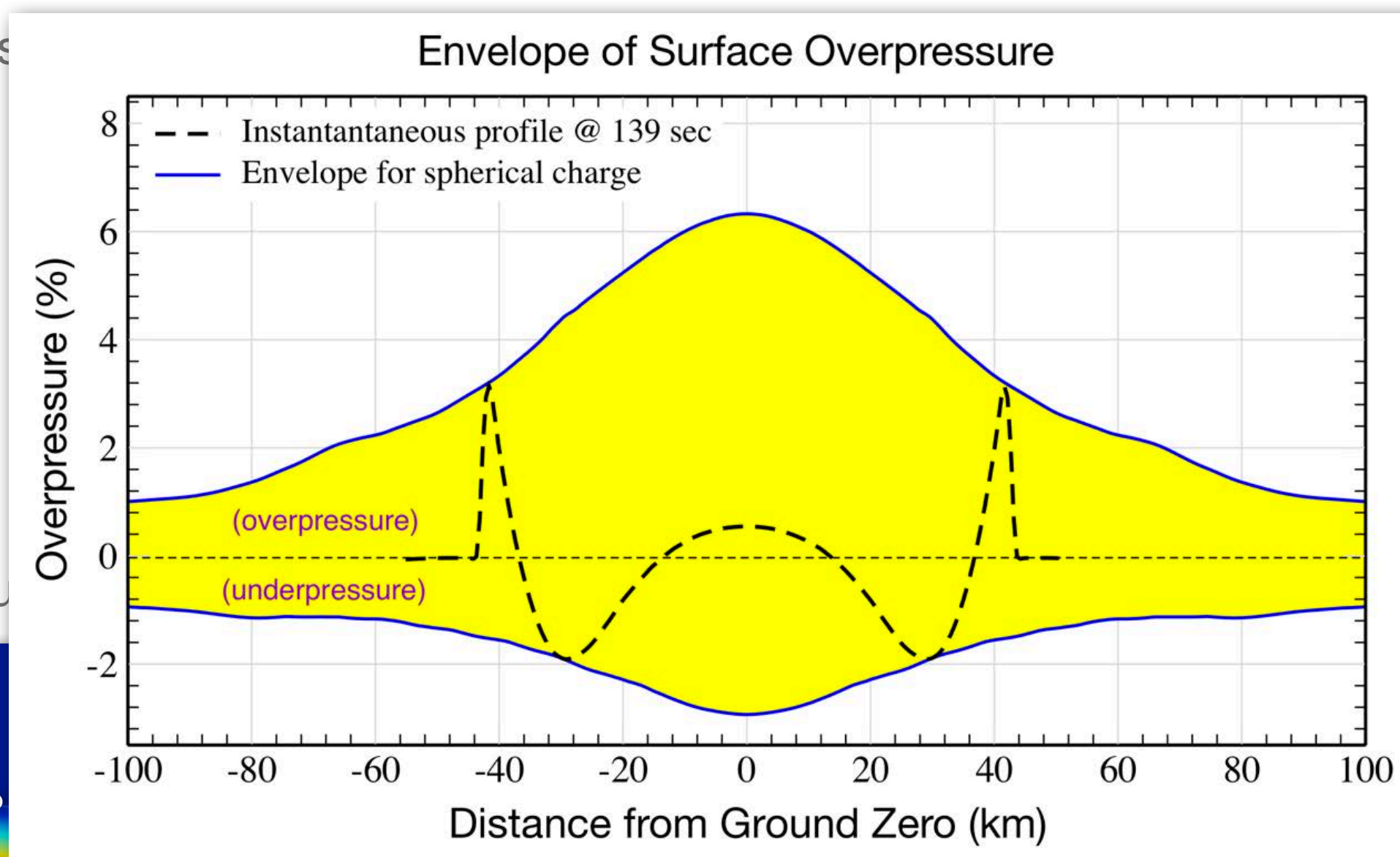


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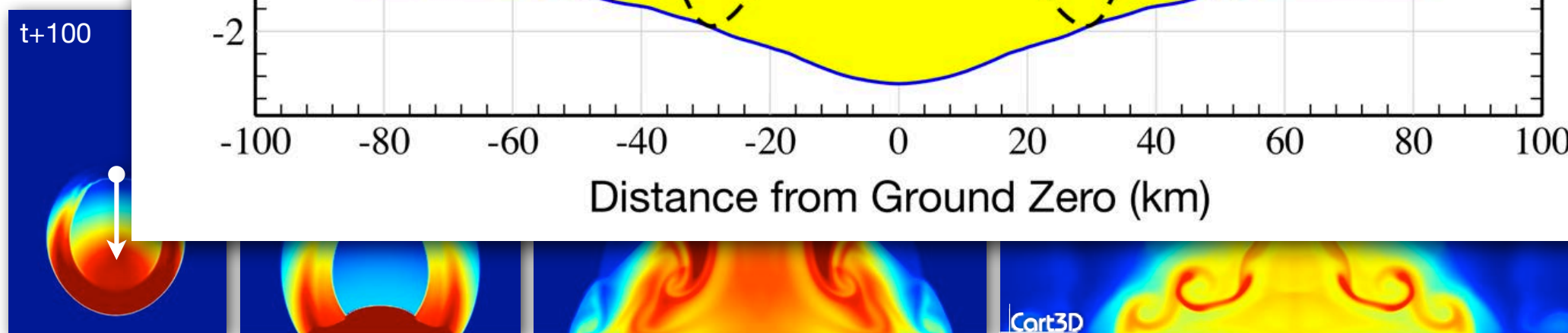
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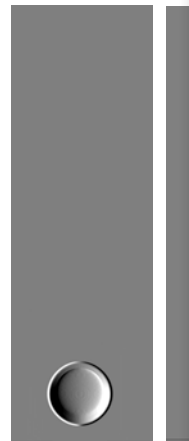


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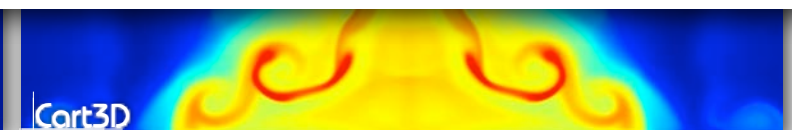
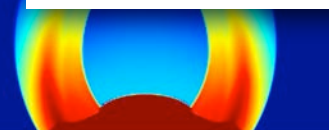
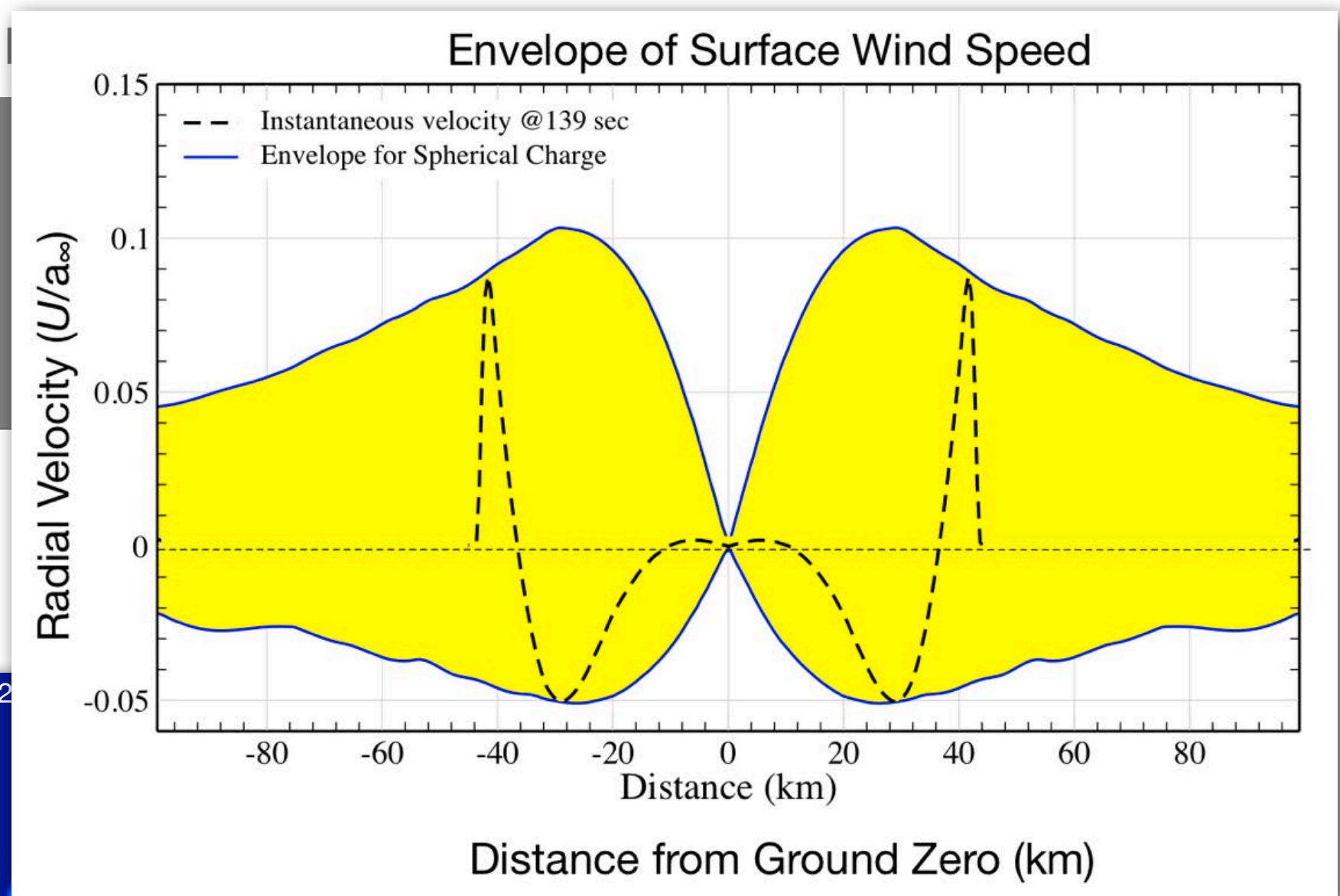
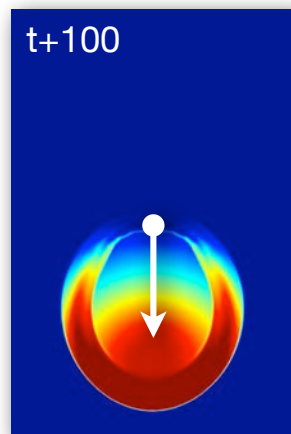
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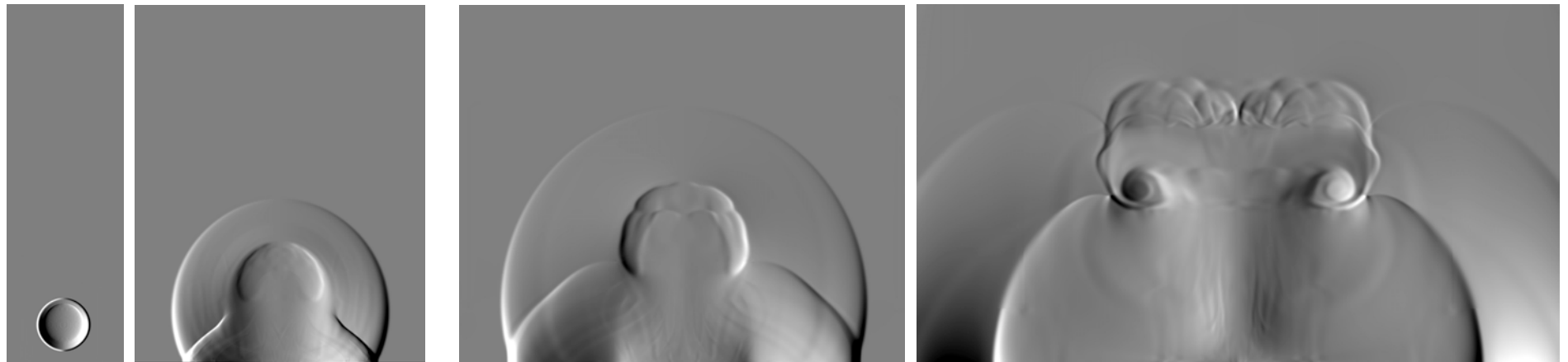


Cort3D

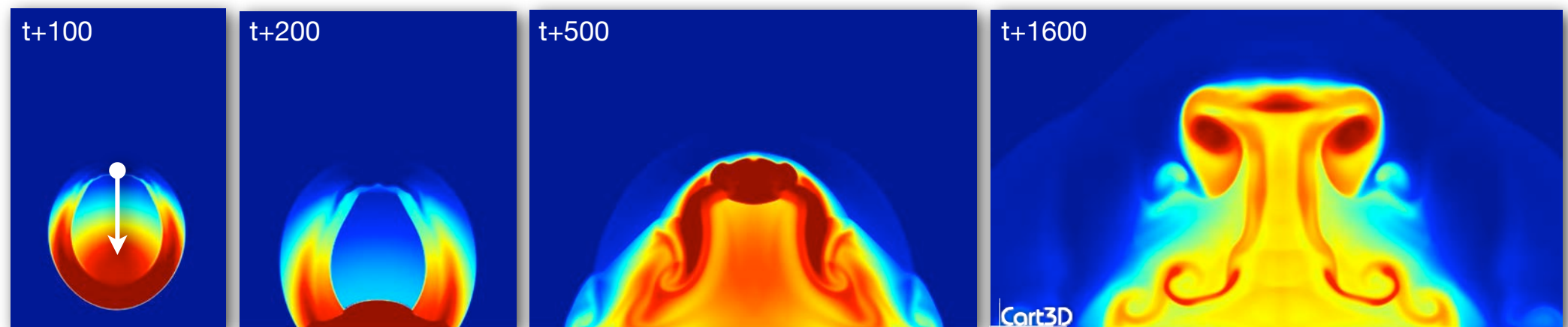
Basic Verification & Validation

Blasts over ground plane

- Numerous examples static and moving blasts over ground plane with buoyancy
 - Static airburst with buoyancy



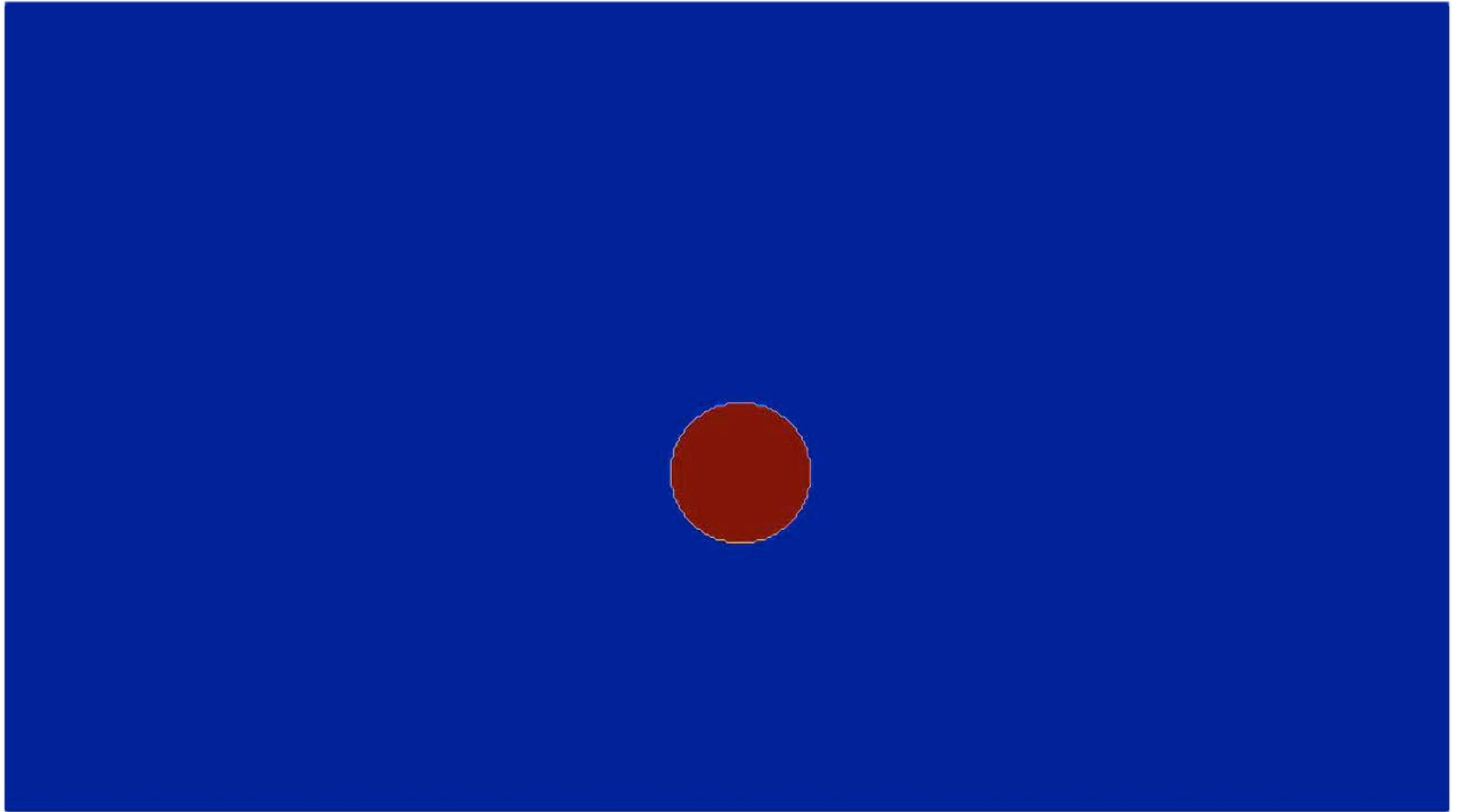
- Moving airburst



Basic Verification & Validation

Blasts over ground plane

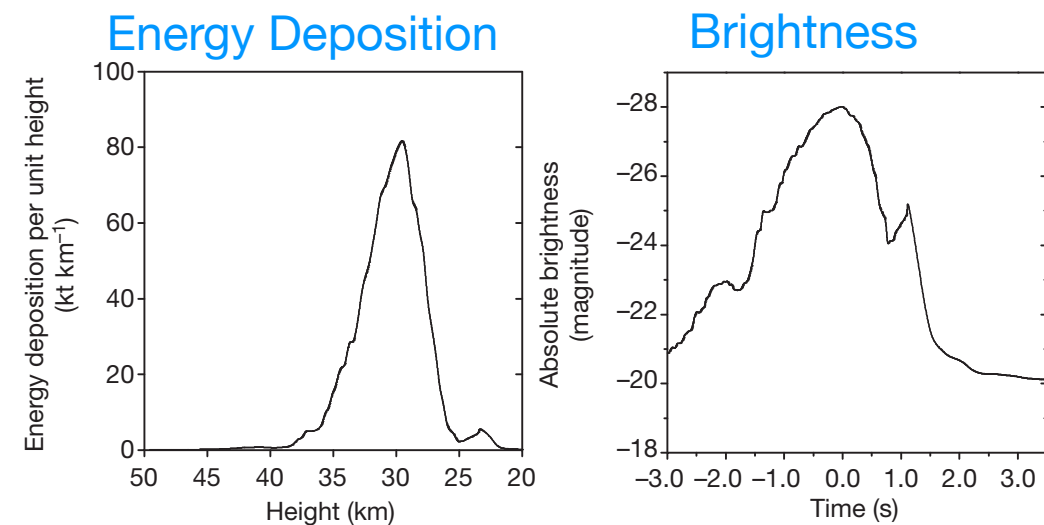
-



Validation: Chelyabinsk Meteor

February 15, 2013

- 12,500 metric tons, 19.8 m diameter
- Trajectory:
 - 18.6 km/sec, (\sim Mach 61.7)
 - 18° entry angle
- Data
 - Ground Damage (glass breakage data)
 - Shock arrival times
 - Light curve reconstruction
 - Energy deposition from infrasound measurements



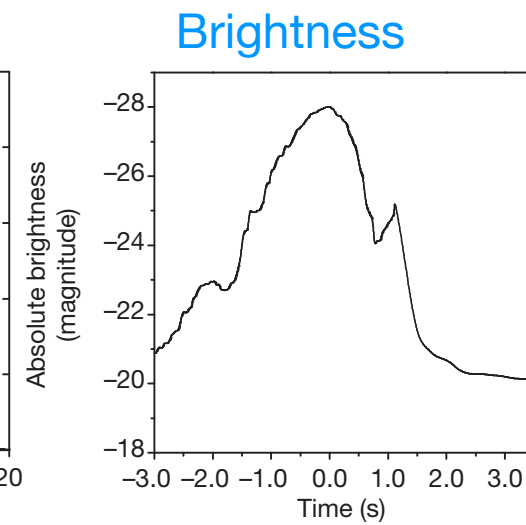
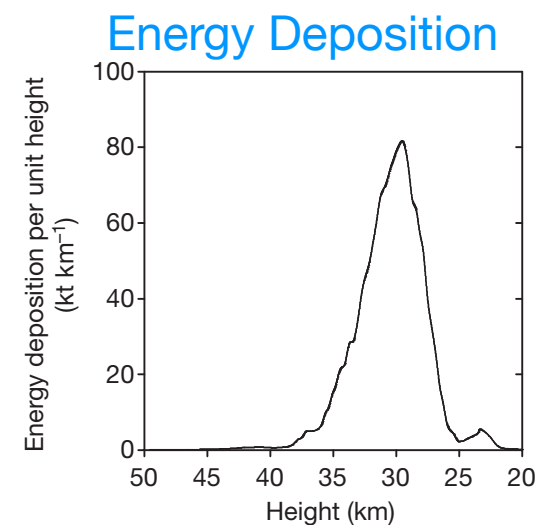
Brown et.al, Nature, 2013

Very well studied event, simulations of virtually all aspects of entry, breakup, analysis of composition, blast propagation, ground damage, etc.

Validation: Chelyabinsk Meteor

February 15, 2013

- 12,500 metric tons, 19.8 m diameter
- Trajectory:
 - 18.6 km/sec, (\sim Mach 61.7)
 - 18° entry angle
- Data
 - Ground Damage (glass breakage data)
 - Shock arrival times
 - Light curve reconstruction
 - Energy deposition from infrasound measurements
- Primary references used
 - Popova & Jenniskens *et al.*, Science Express, November 2013
 - Brown *et al.*, Nature, November 2013
 - Chelyabinsk Airburst Consortium, + various other media

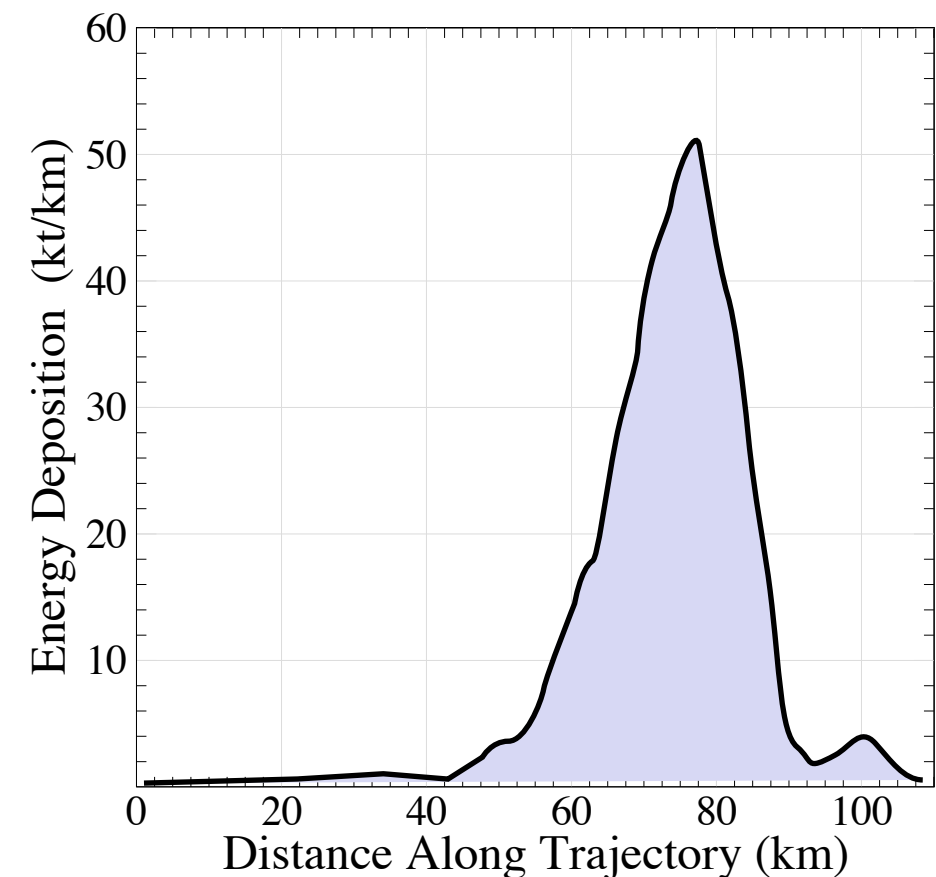
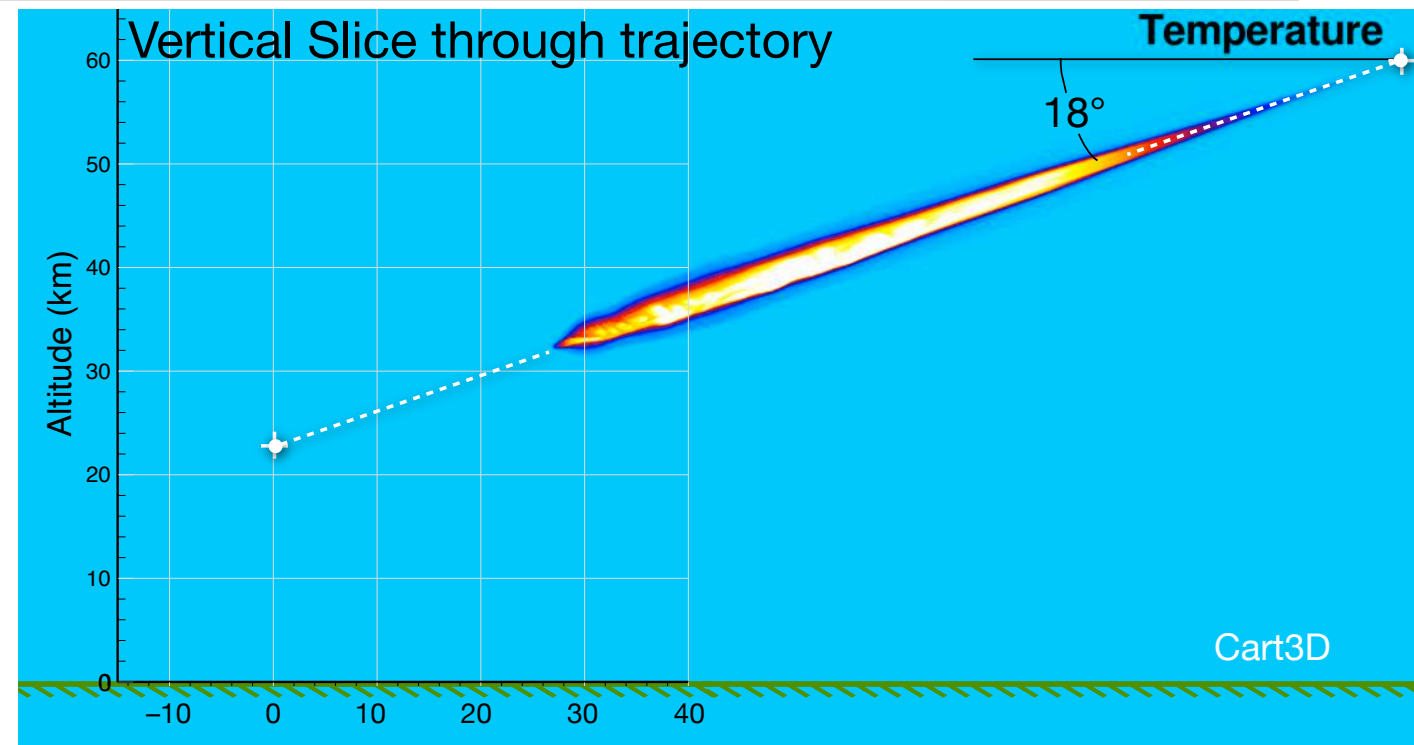


Brown et al, Nature, 2013

Validation: Chelyabinsk Meteor

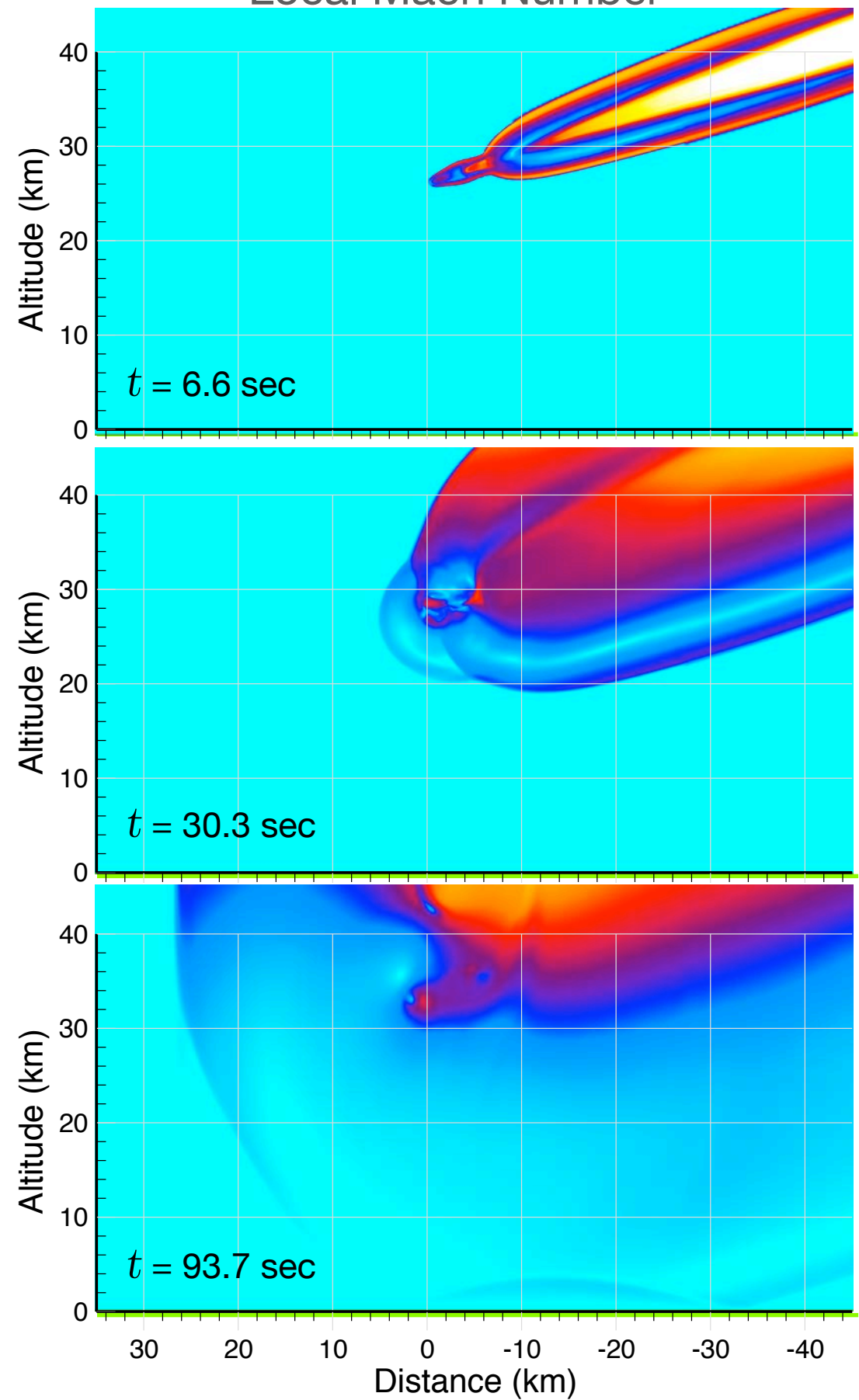
Simulation Details

- Energy deposition:
 - $E_{tot} = (520 \text{ kt} - 5\% \text{ radiation})$
 - Profile from Brown et al. Nature 2013
- Net mass deposited:
 - $m_{tot} = 12.5 \text{e6 kg}$
- Trajectory:
 - 18.6 km/sec, (~Mach 61.7) @ 18° angle
 - Peak brightness @ 29.5 km
 - ~110 km length, 60→24 km altitude
 - Assume constant velocity
- 3D simulation with ~90M cells
 - Resolution of ~20 m along trajectory & ~100 m resolution near ground
 - Simulation covers ~300 sec. of real time

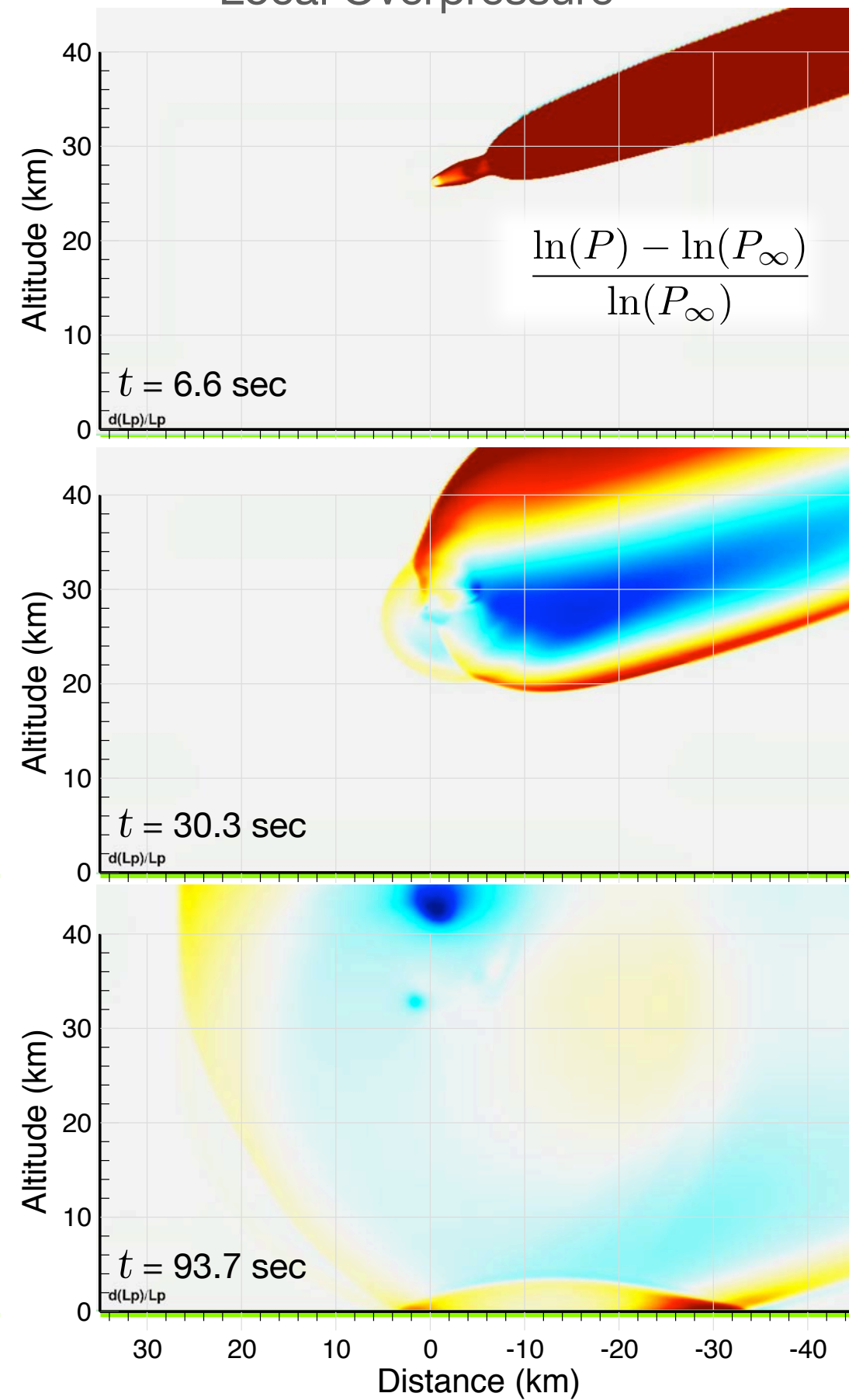


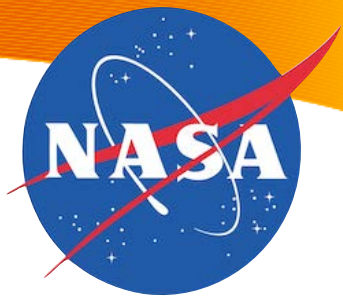


Local Mach Number

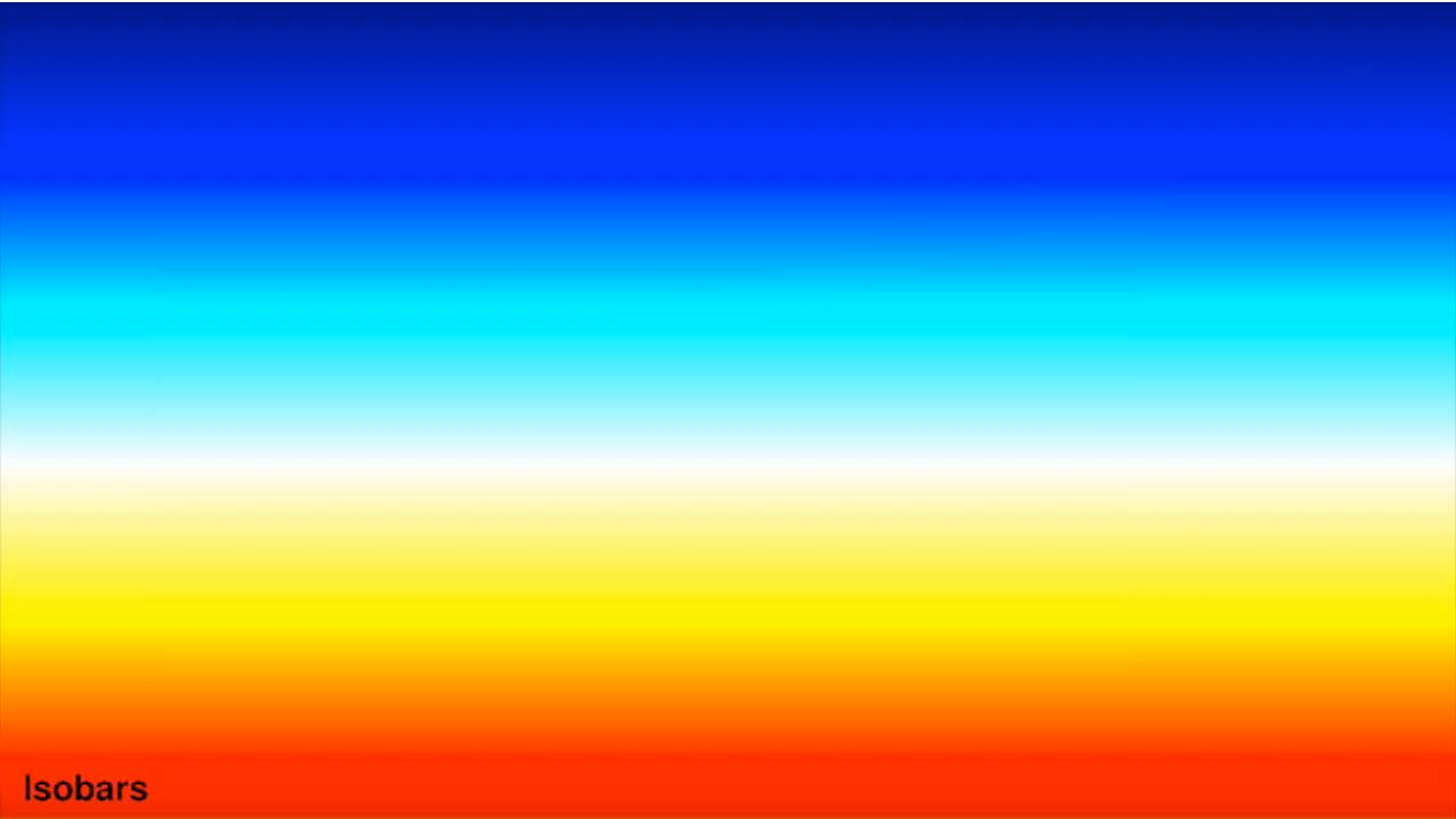


Local Overpressure





Validation: Chelyabinsk Meteor

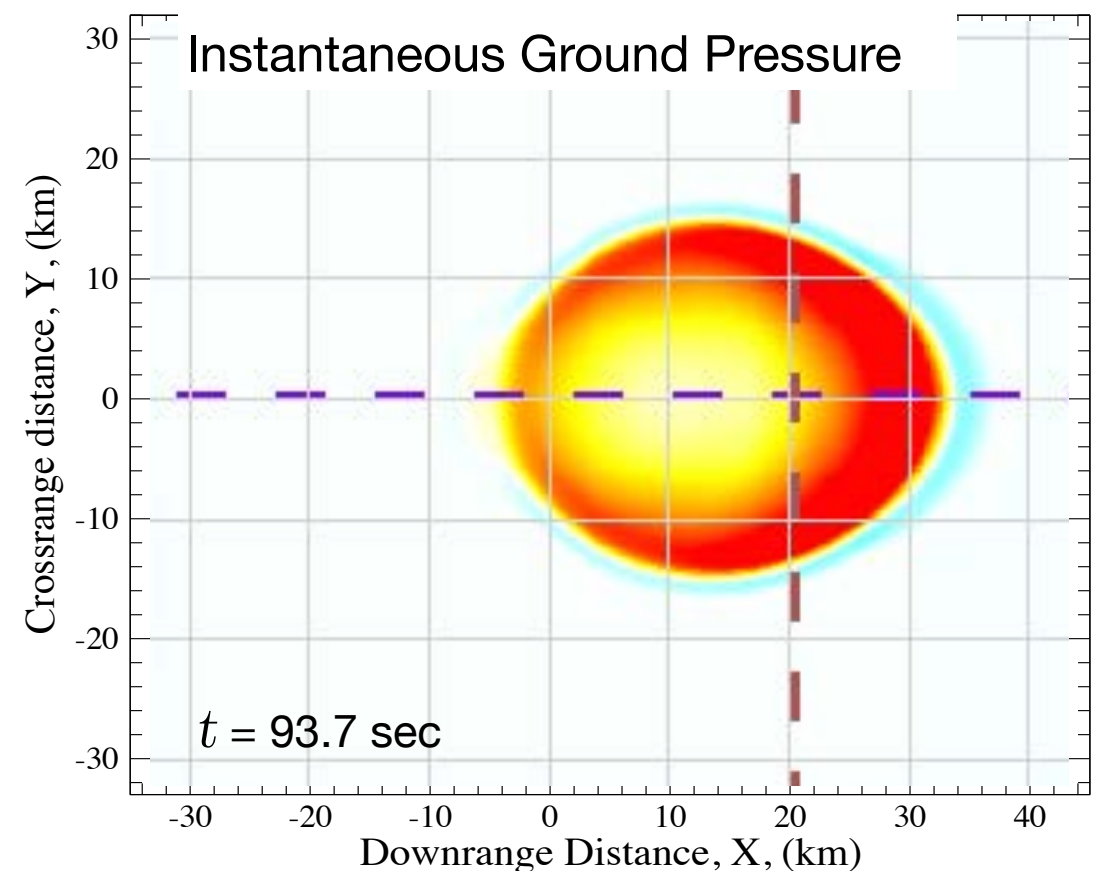
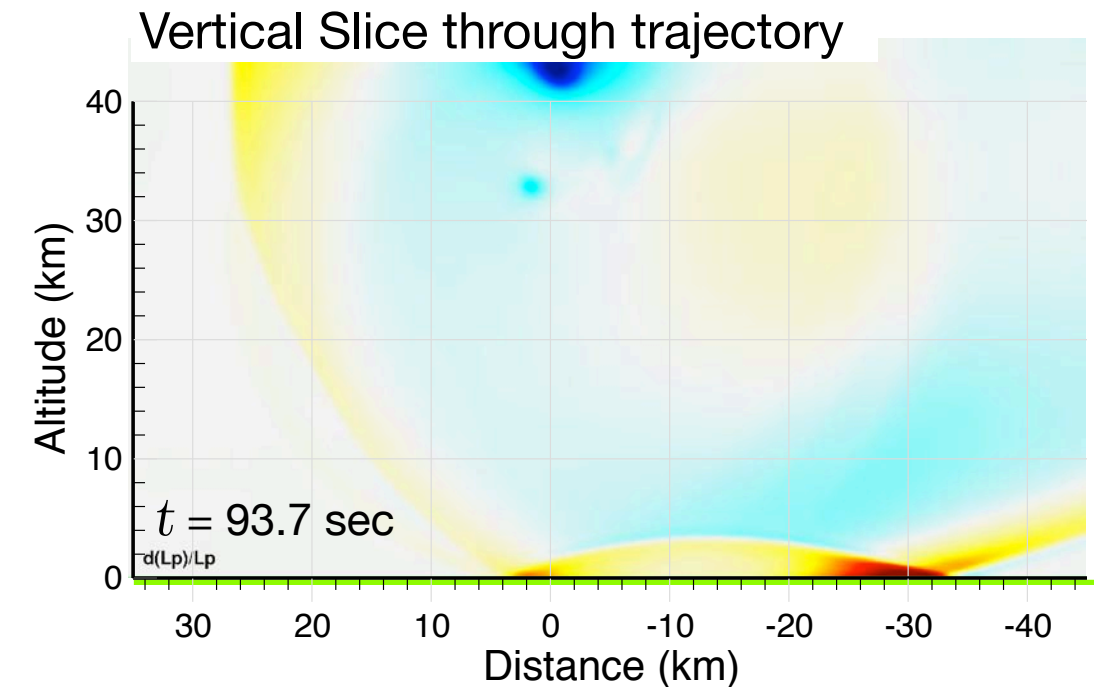


Isobars

Validation: Chelyabinsk Meteor

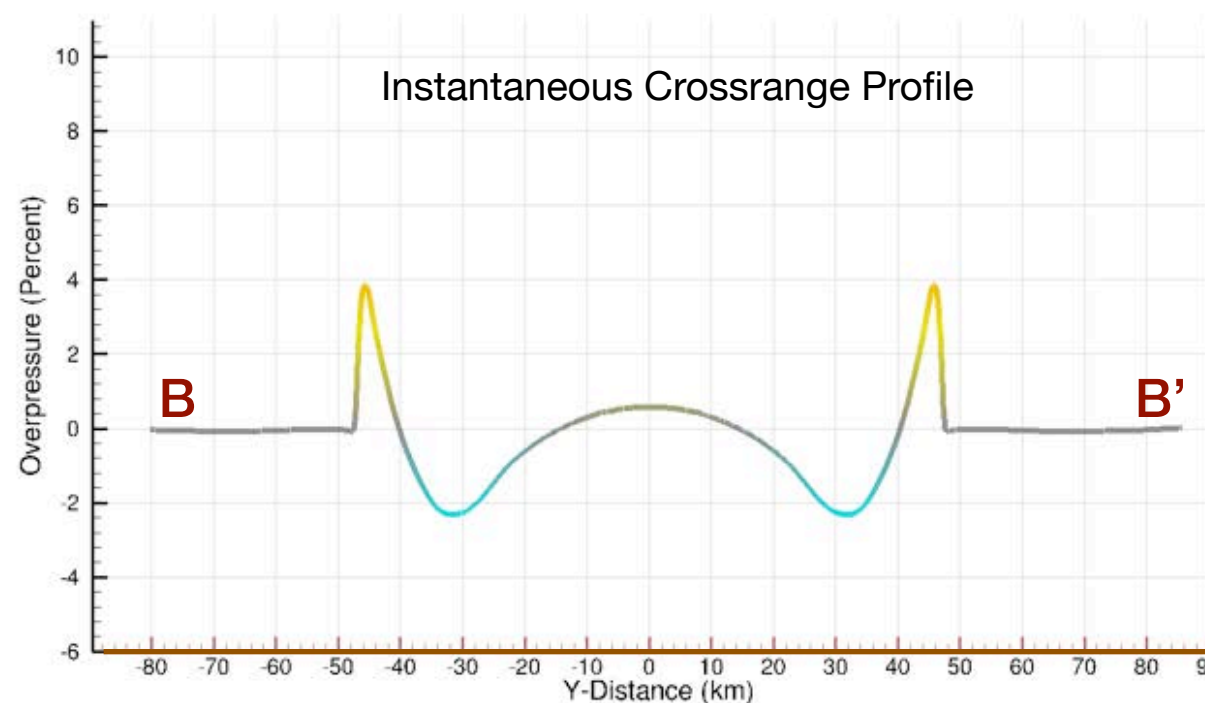
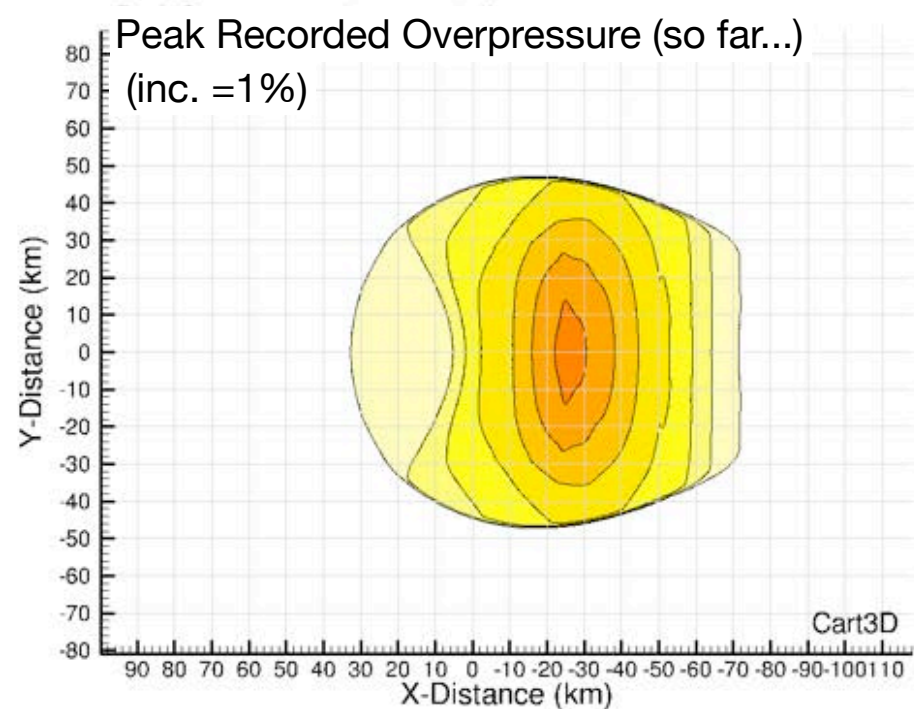
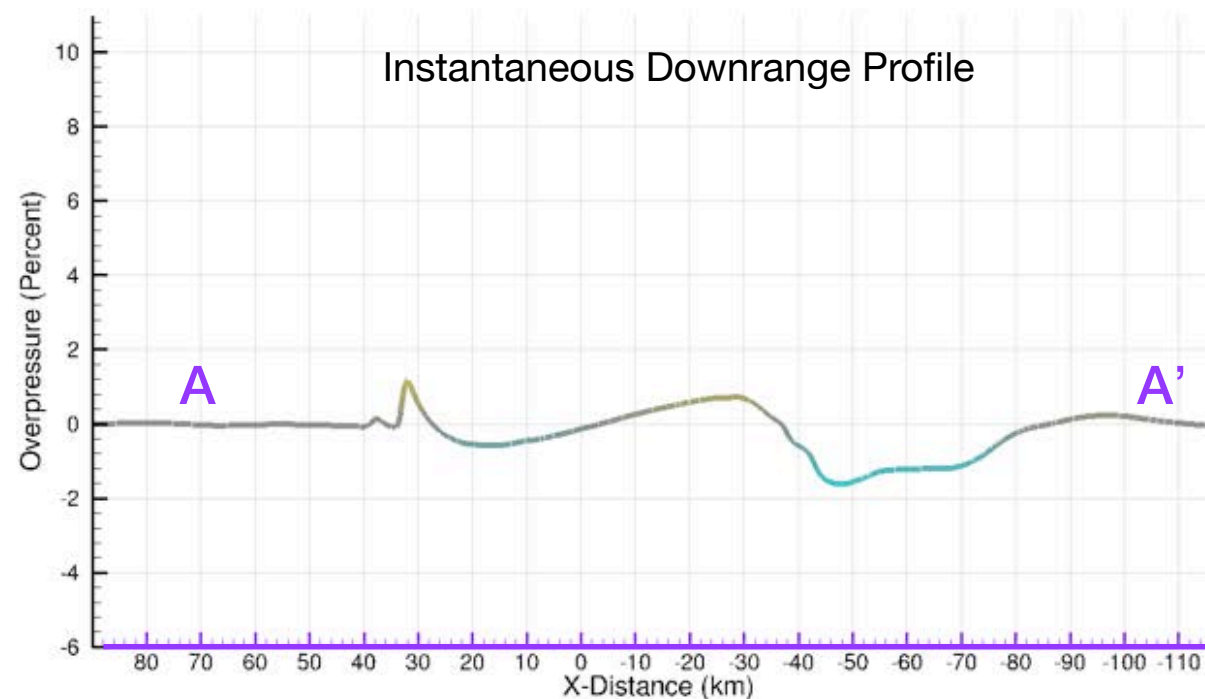
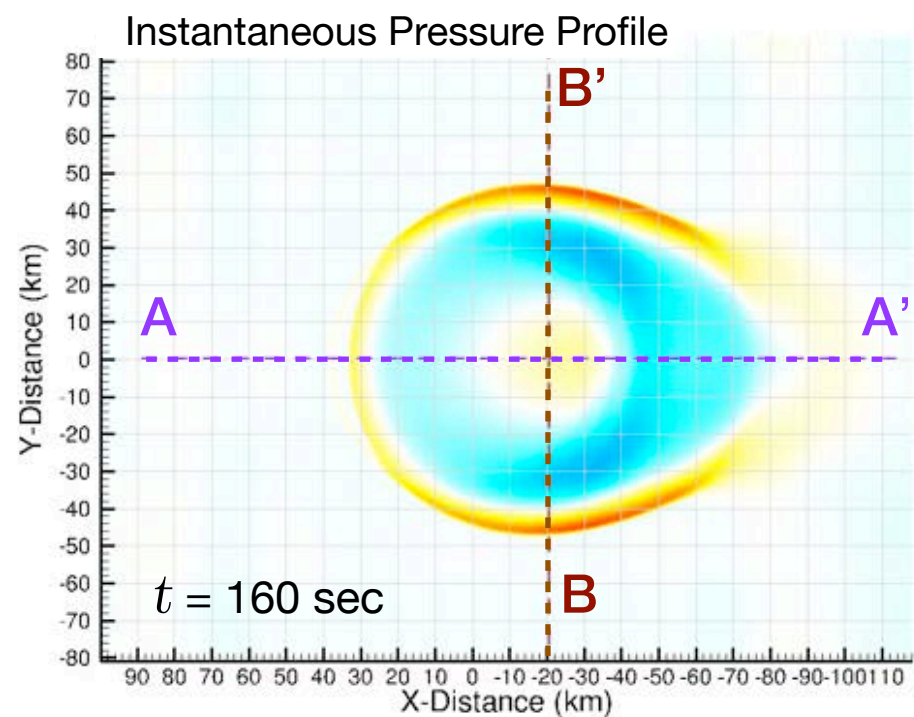
Ground footprint

- Goal is prediction of pressure & velocity on the ground
- Blast first contacts ground at $t = \sim 82.7$ sec elapsed time (~ 78 sec. after peak brightness)
- Excellent agreement with earliest data on blast arrival time data (76 – 90 sec) (Popova et al.)



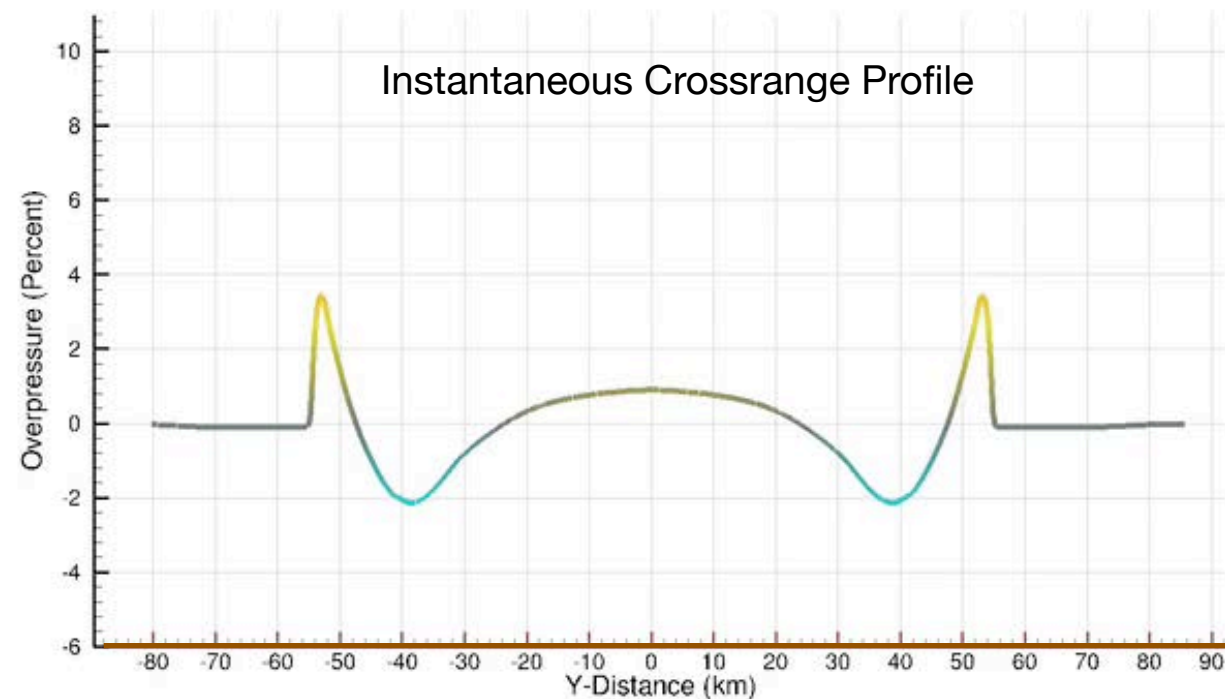
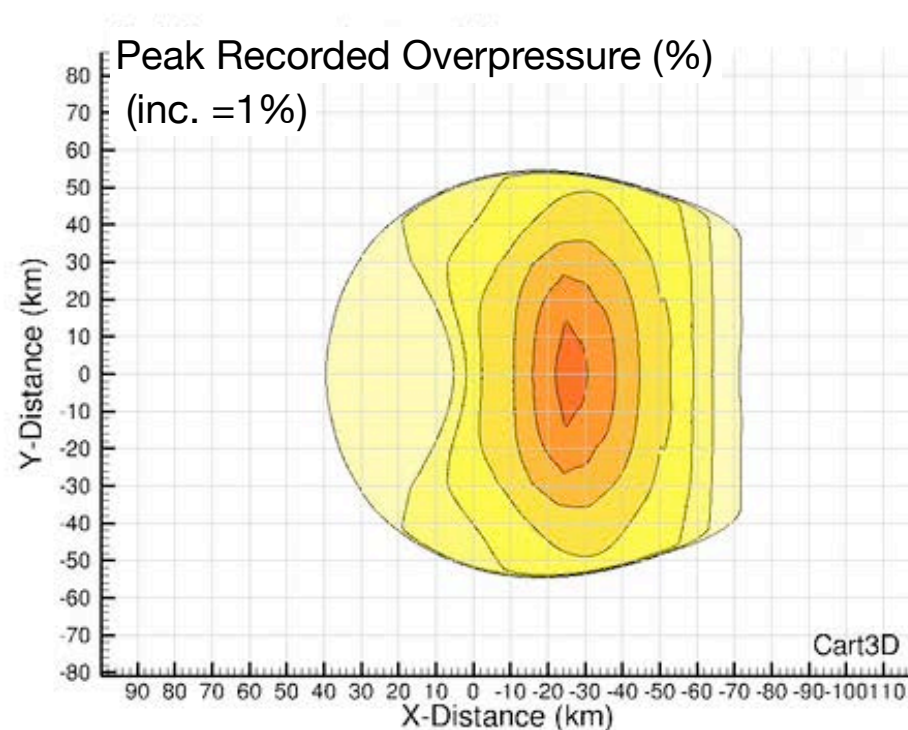
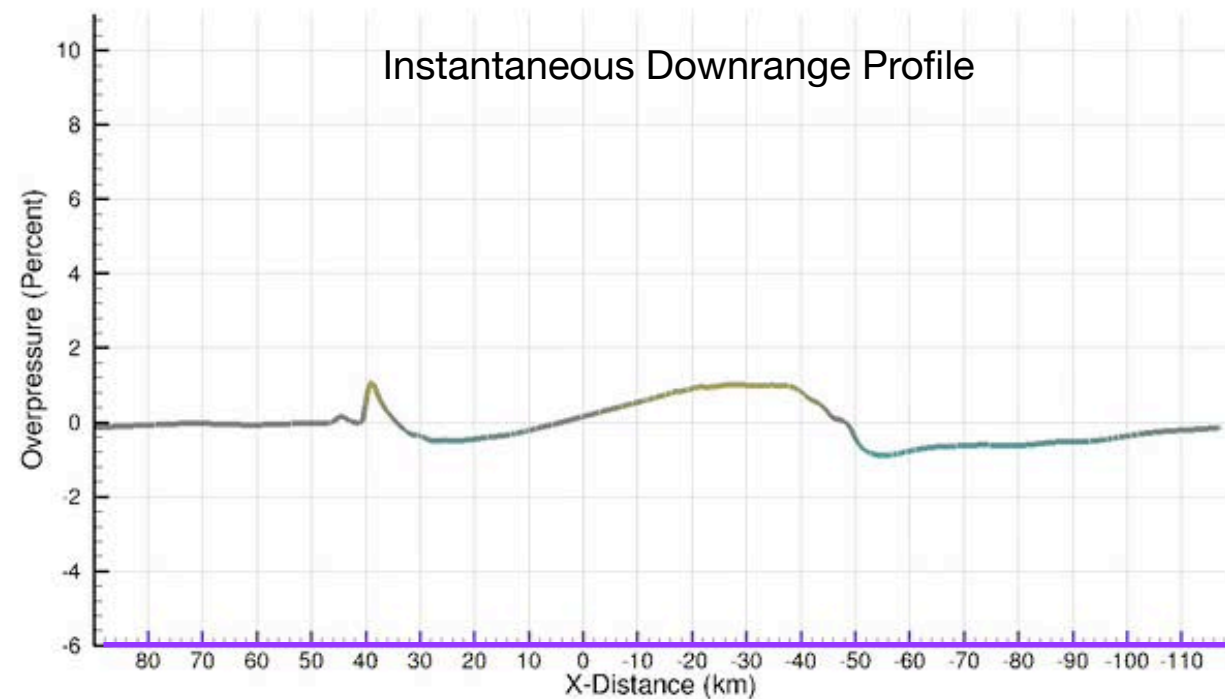
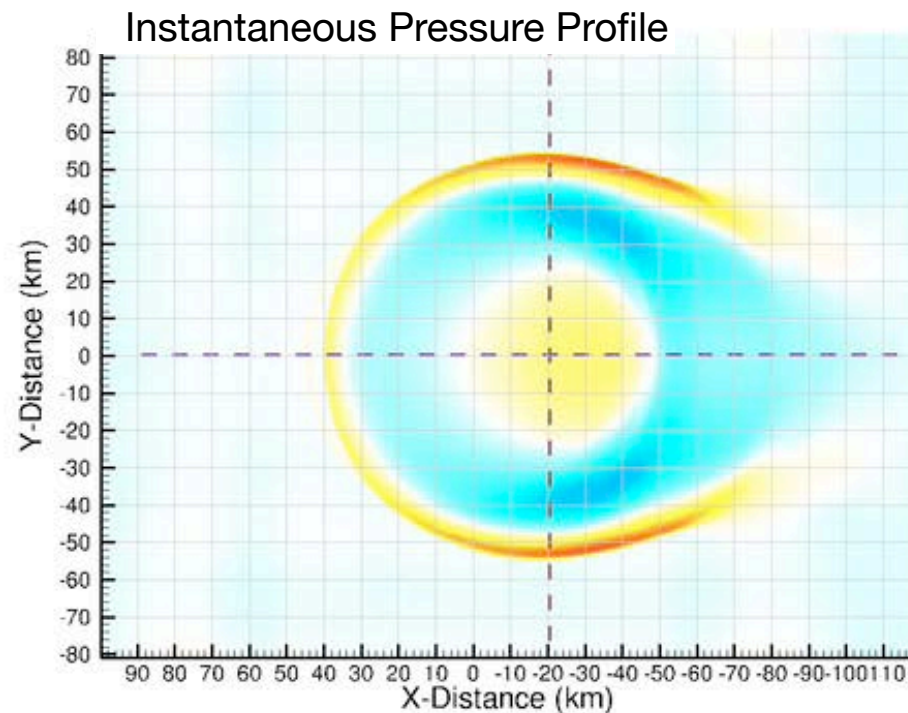
Validation: Chelyabinsk Meteor

Ground footprint evolution



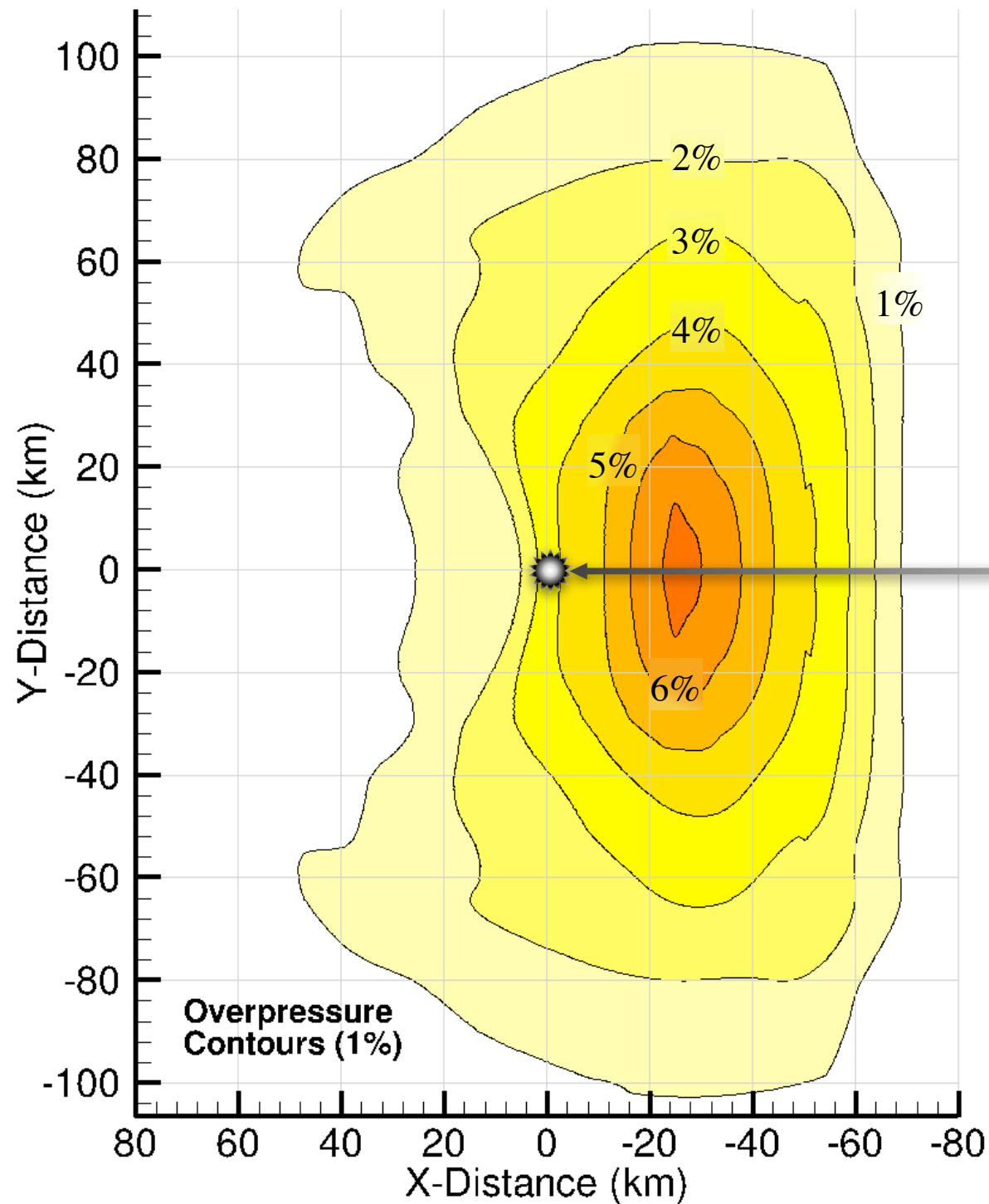
Validation: Chelyabinsk Meteor

Ground footprint evolution



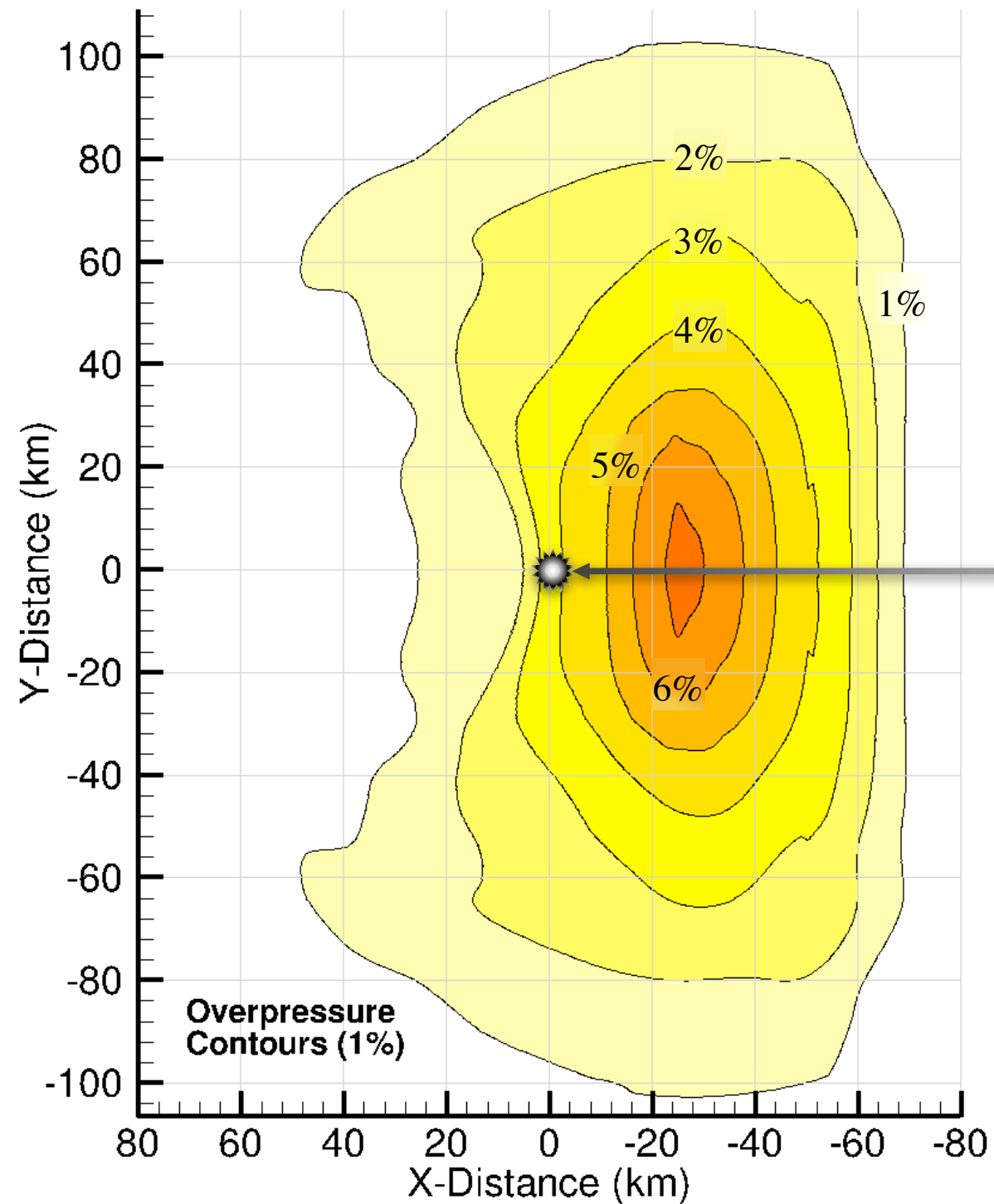
Validation: Chelyabinsk Meteor

Peak Ground Overpressures

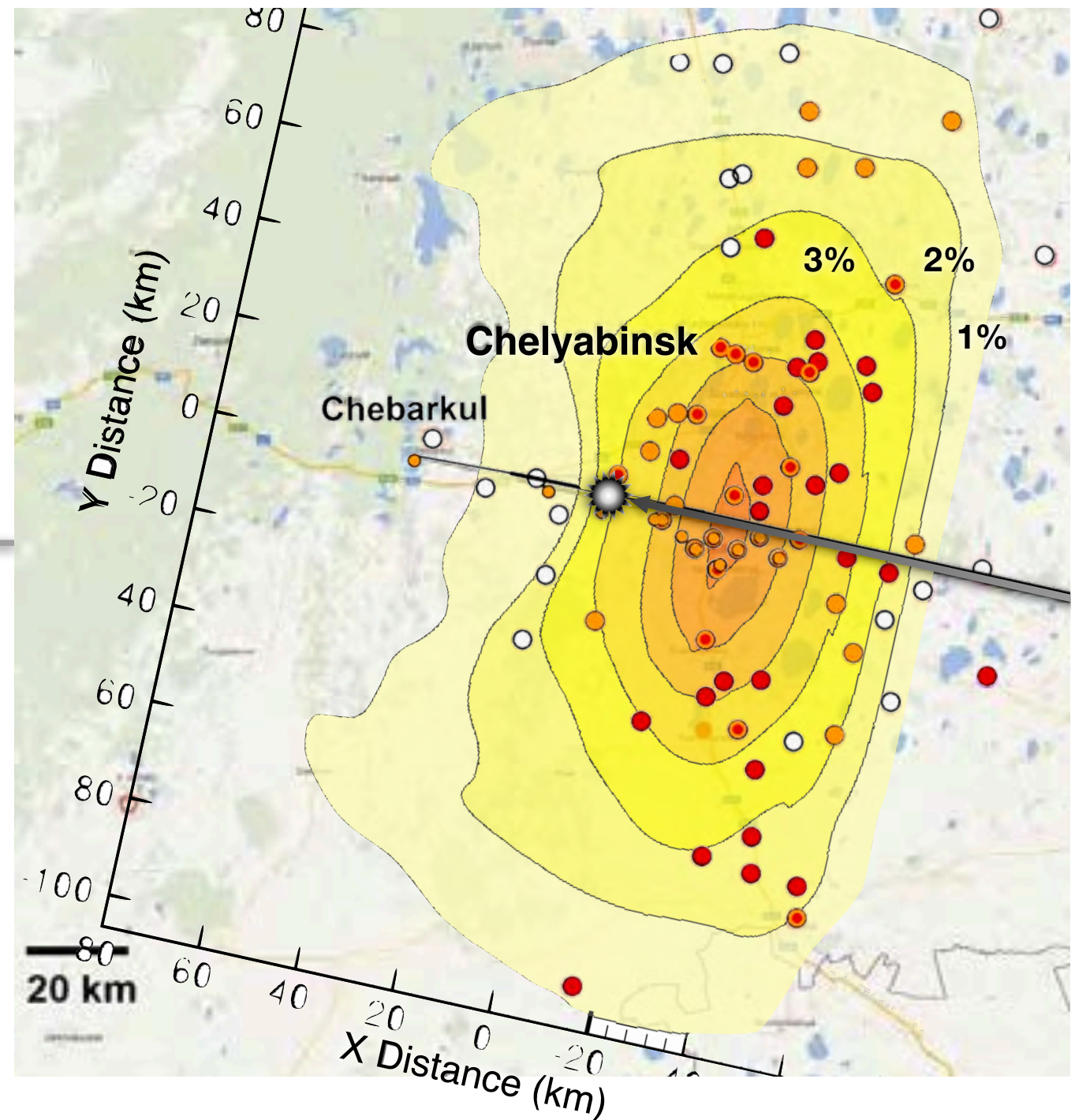


Validation: Chelyabinsk Meteor

Peak Ground Overpressures

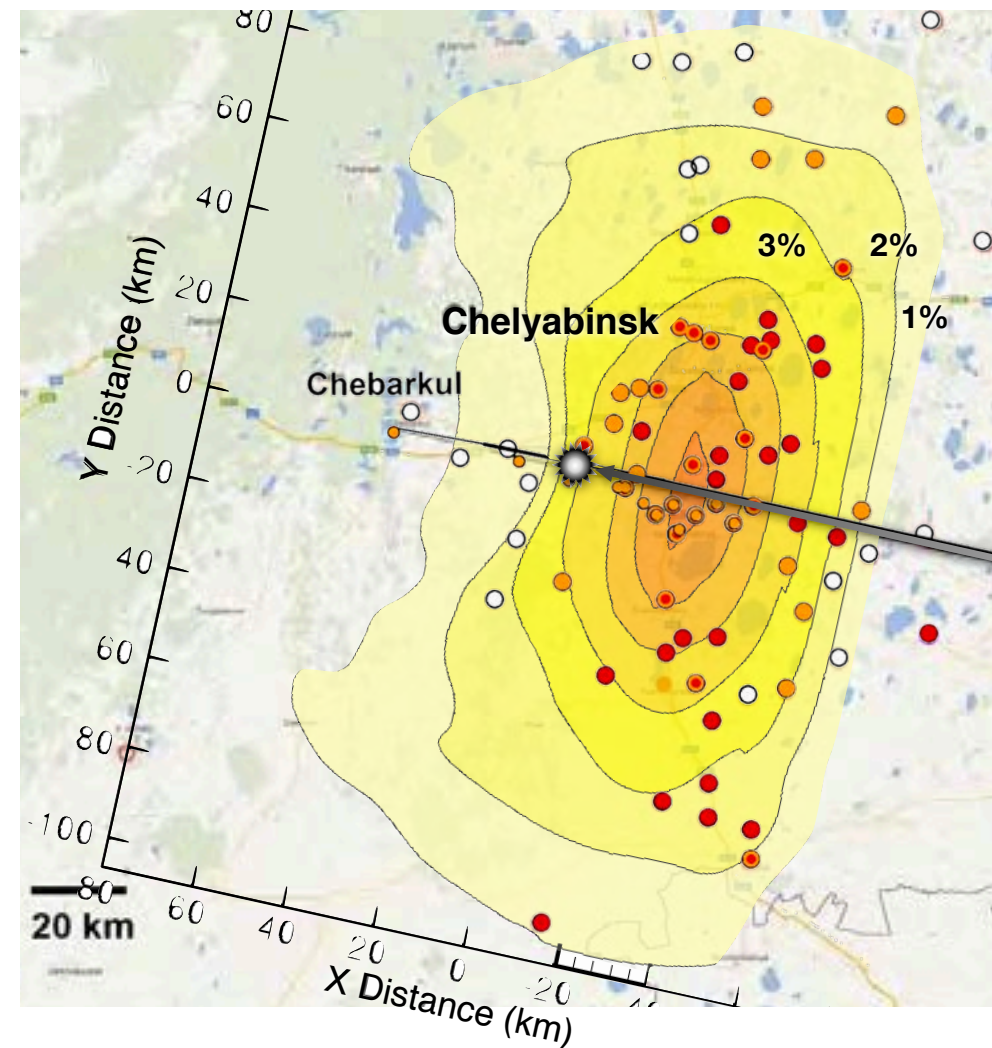
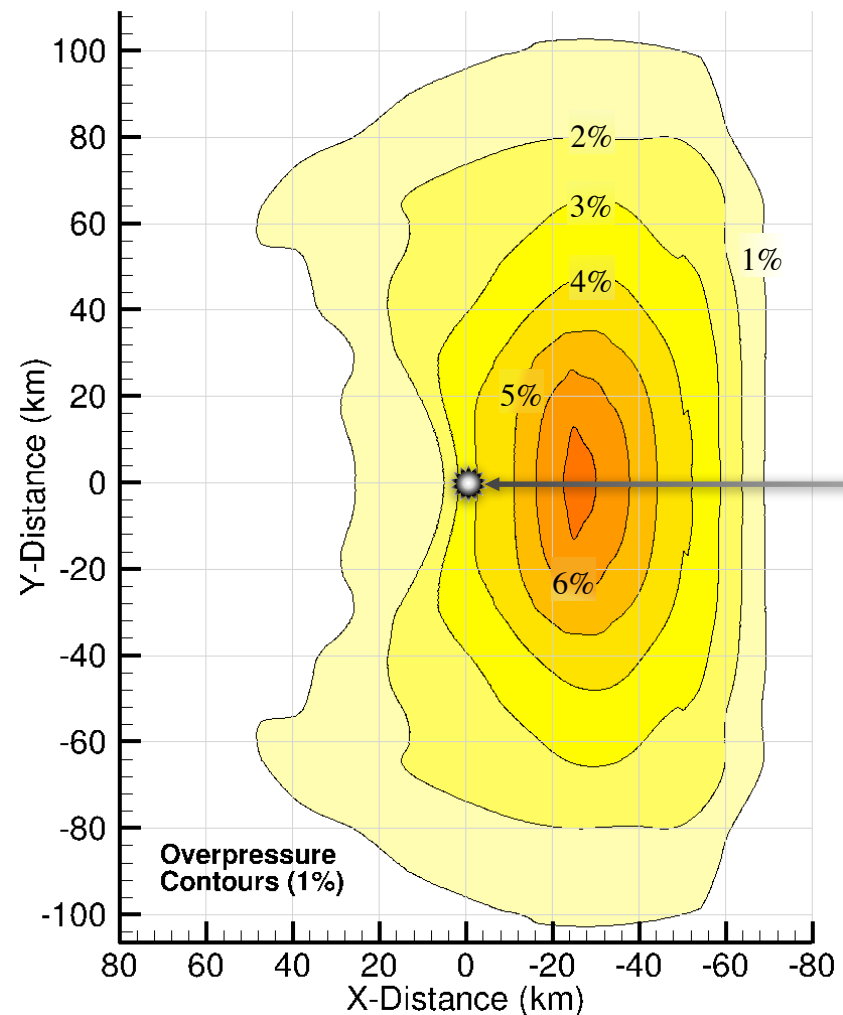


Glass Damage Data Comparison



Validation: Chelyabinsk Meteor

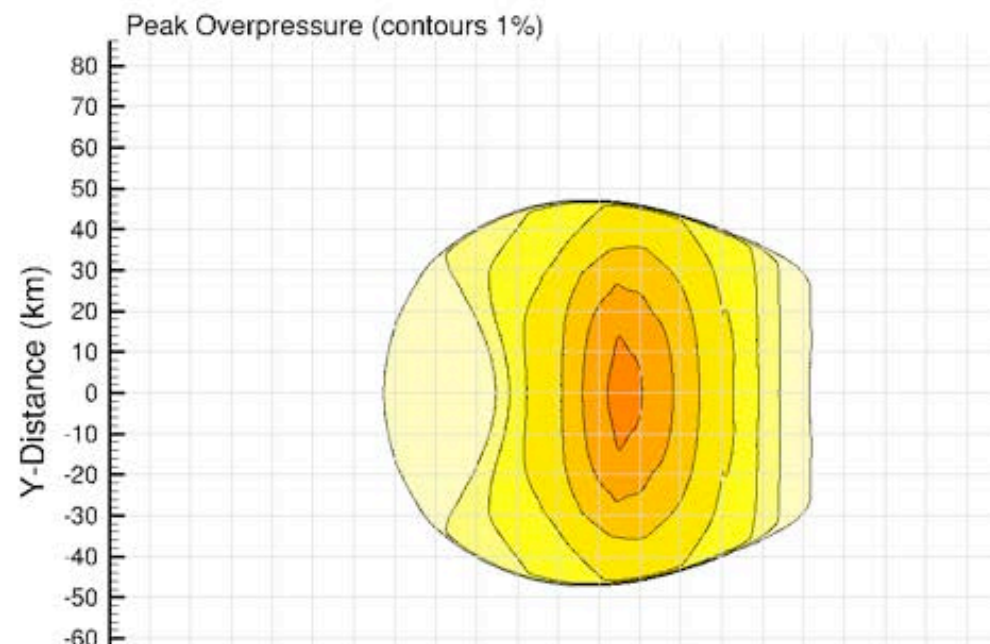
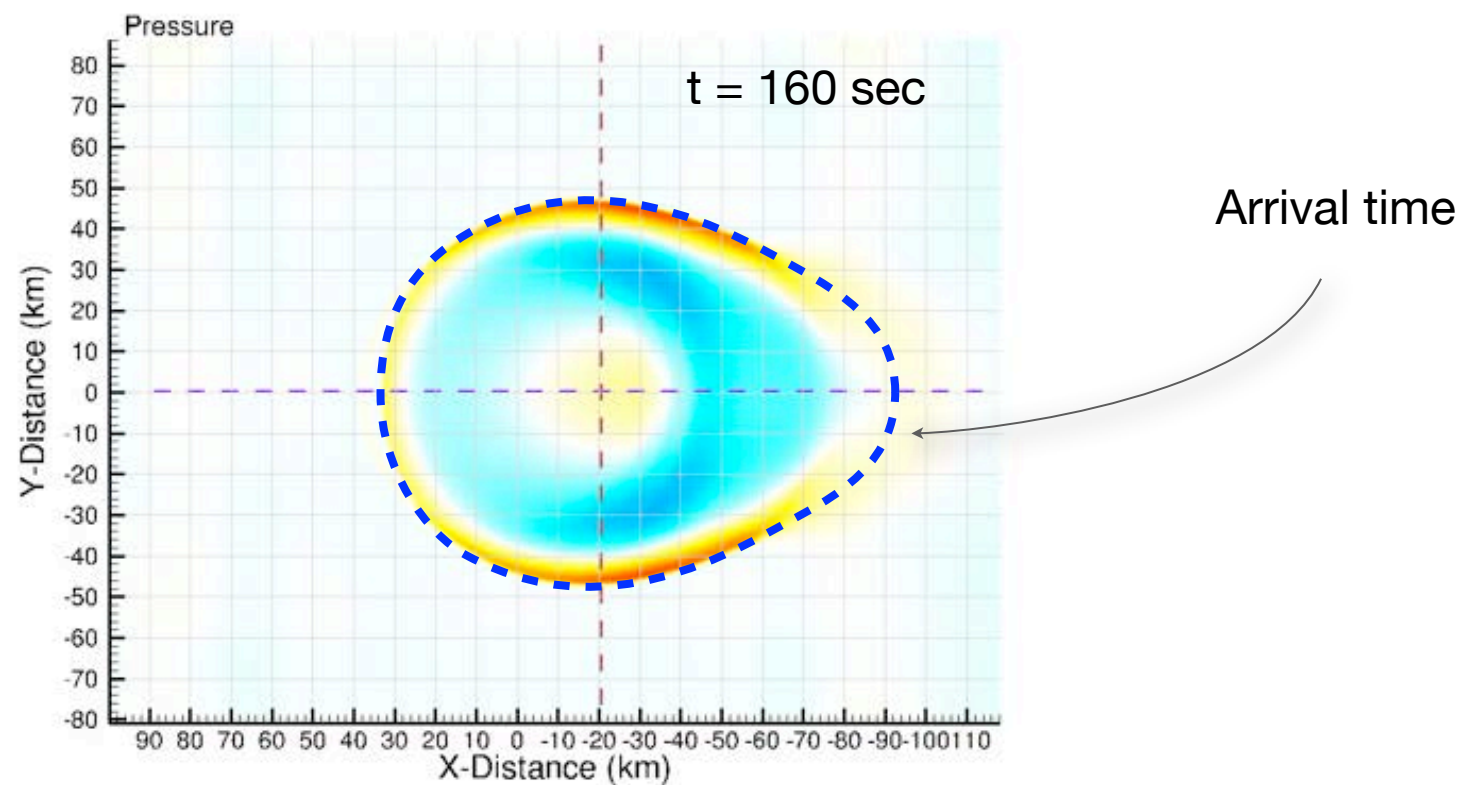
Peak Ground Overpressures



- Glass damage data collected by the Chelyabinsk Airburst Consortium
- Statistical correlation (Mannan & Lees) show 700 Pa (0.69%) shatters ~5% of typical windows, 6% overpressure breaks roughly 90%.
- Footprint similar to those in Popova et al. (ScienceExpress)
- Breakage data estimate overpressure at chelyabinsk ~2-4% (P. Brown)

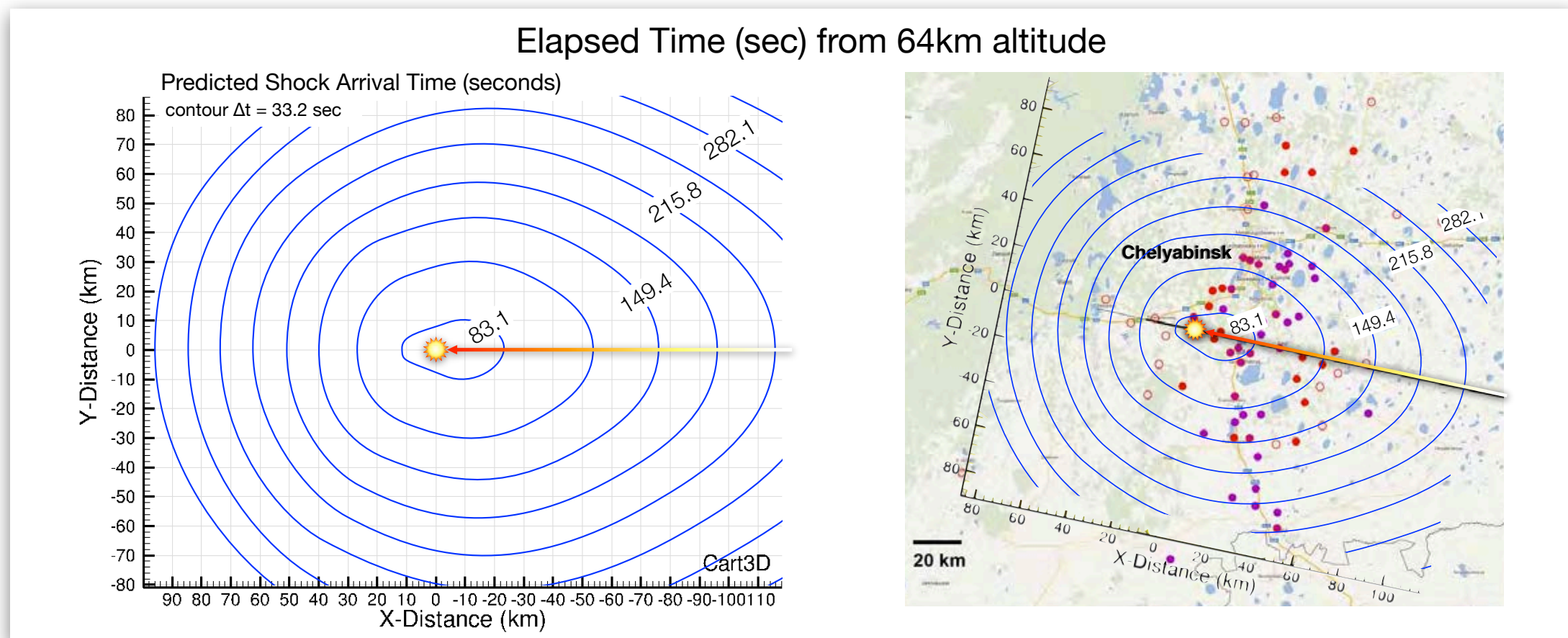
Validation: Chelyabinsk Meteor

Shock Arrival Time



Validation: Chelyabinsk Meteor

Shock Arrival Time



- Peak brightness at ~4 sec. elapsed time
- First arrival at ~78 sec after peak brightness,
- Predict ~90 sec (from peak brightness) at Korkino and Yemanzhelinsk
- Arrival in vicinity of Chelyabinsk at 140-145 seconds
- Neglected local wind, temperature and other effects of the real atmosphere
- Overall very good agreement with data & best predictions in literature



Overview

Report current status of effort and connection with PRA and tsunami

- Modeling & Solver
- Verification & Validation
 - Basic
 - Chelyabinsk Case Study
- Investigations of ground-footprint sensitivity
 - Line-source vs time-dependent entry
 - Entry Angle
- Upcoming Efforts



Overview

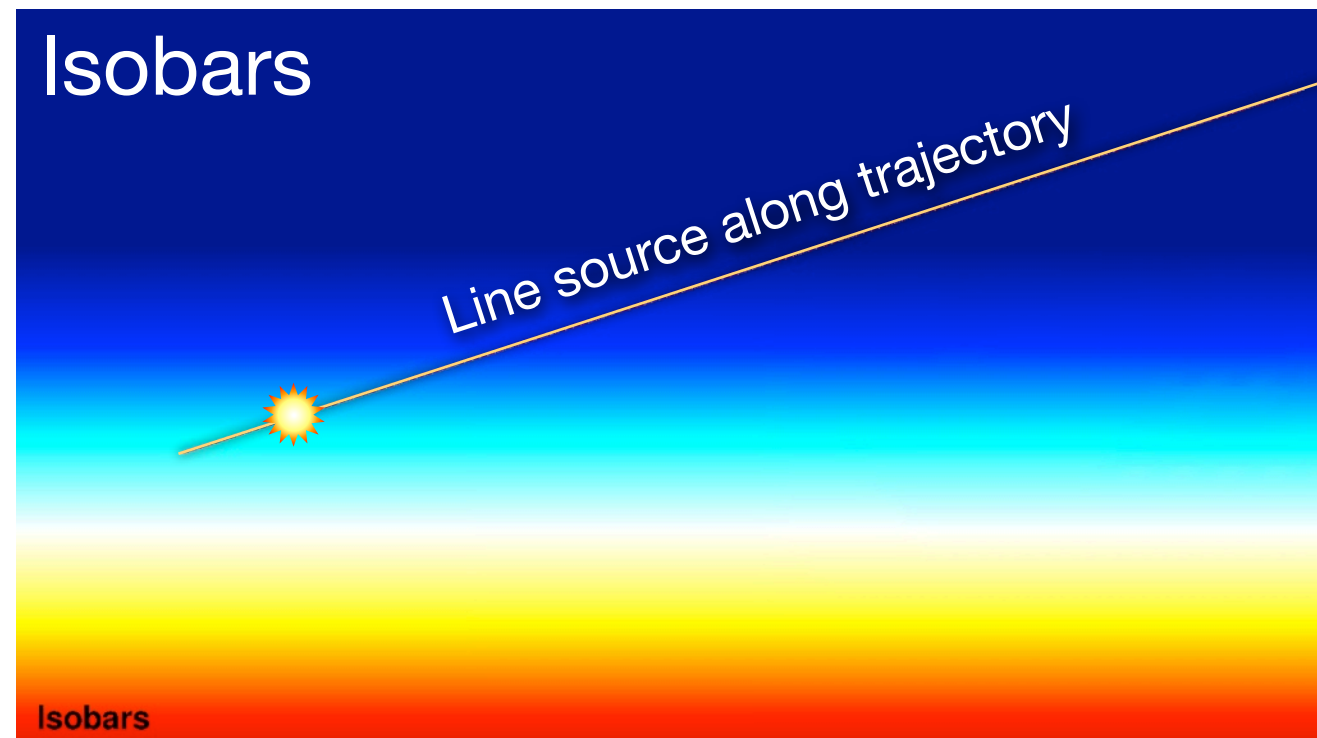
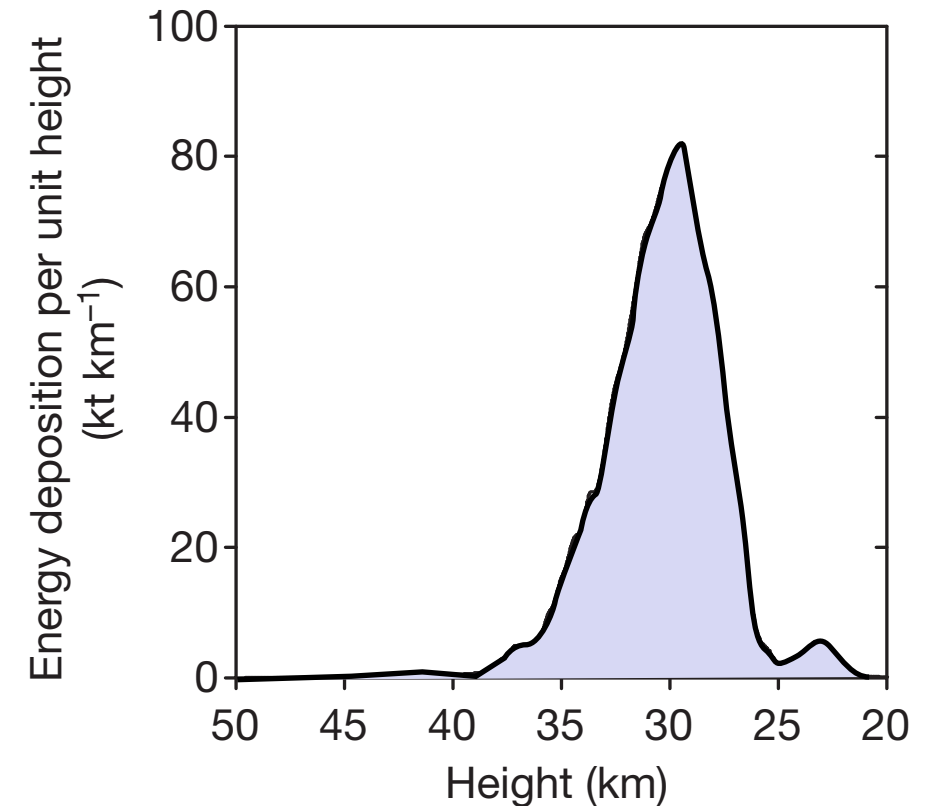
Report current status of effort and connection with PRA and tsunami

- Modeling & Solver
- Verification & Validation
 - Basic
 - Chelyabinsk Case Study
- Investigations of ground-footprint sensitivity
 - Sensitivity to entry modeling
 - Time-dependent compared to simple line source
 - Entry angle / Spherical charge investigation
- U

Sensitivity - Entry Modeling

Time-Dependent modeling vs simple line source

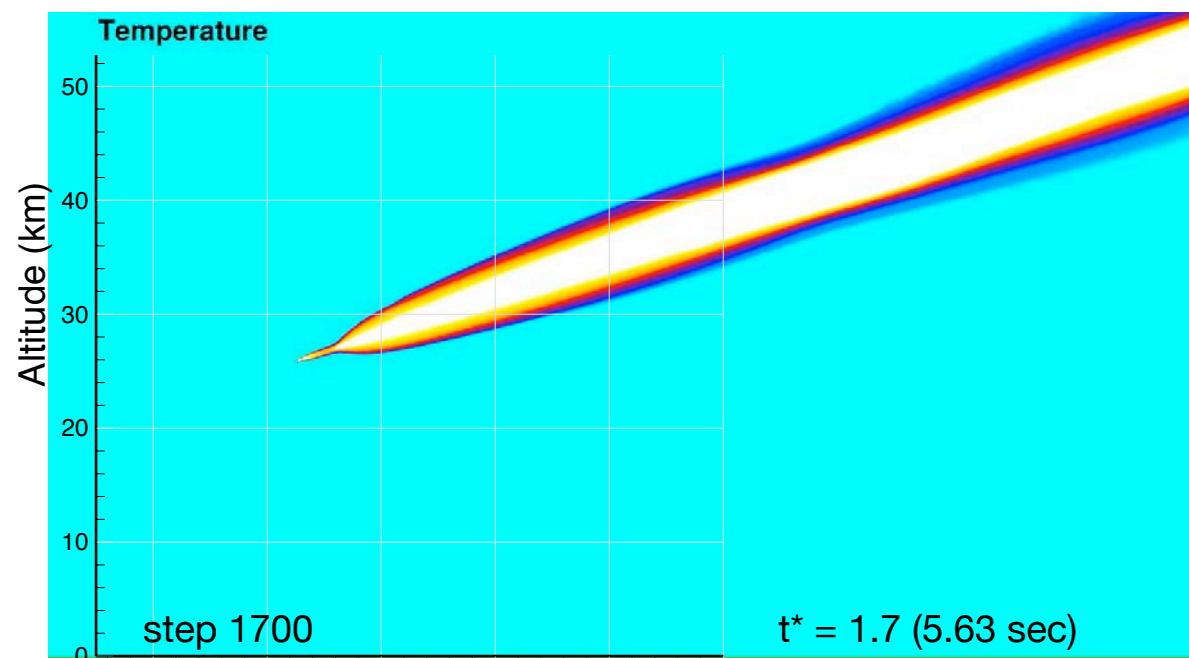
- Entry only lasts for seconds, blast propagates for minutes
 - Detailed entry modeling requires very fine time-scales ($\Delta t \approx 1.e-4$)
 - Cost: 90M cell simulation: (1000 cores x 8-12 hrs) - Under 1% of NAS Pleiades
 - Line Source for mass, momentum and energy can reduce cost by 50%
- When is line source modeling appropriate?



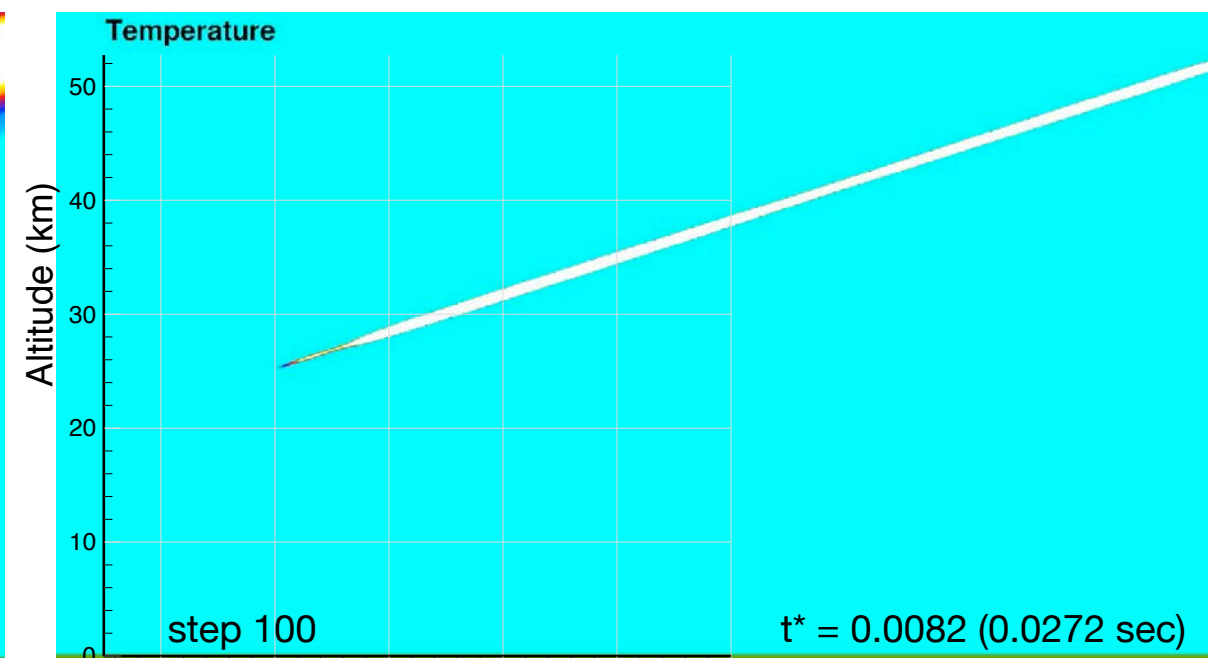
Sensitivity - Entry Modeling

Seconds after entry

Time-Dependent



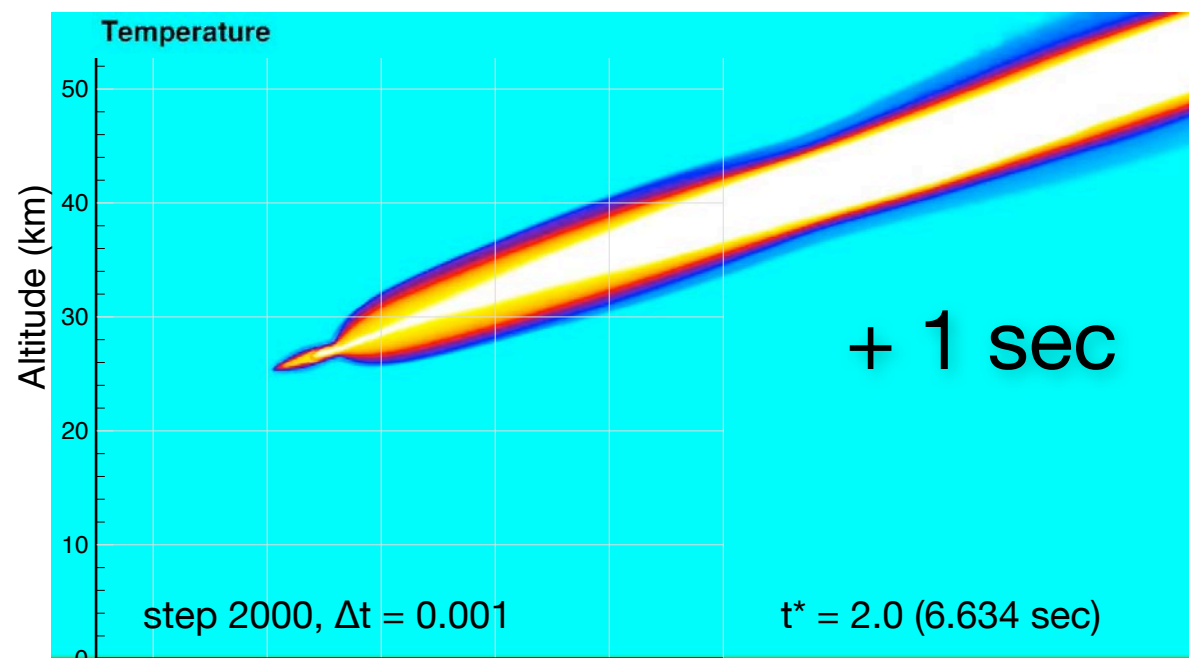
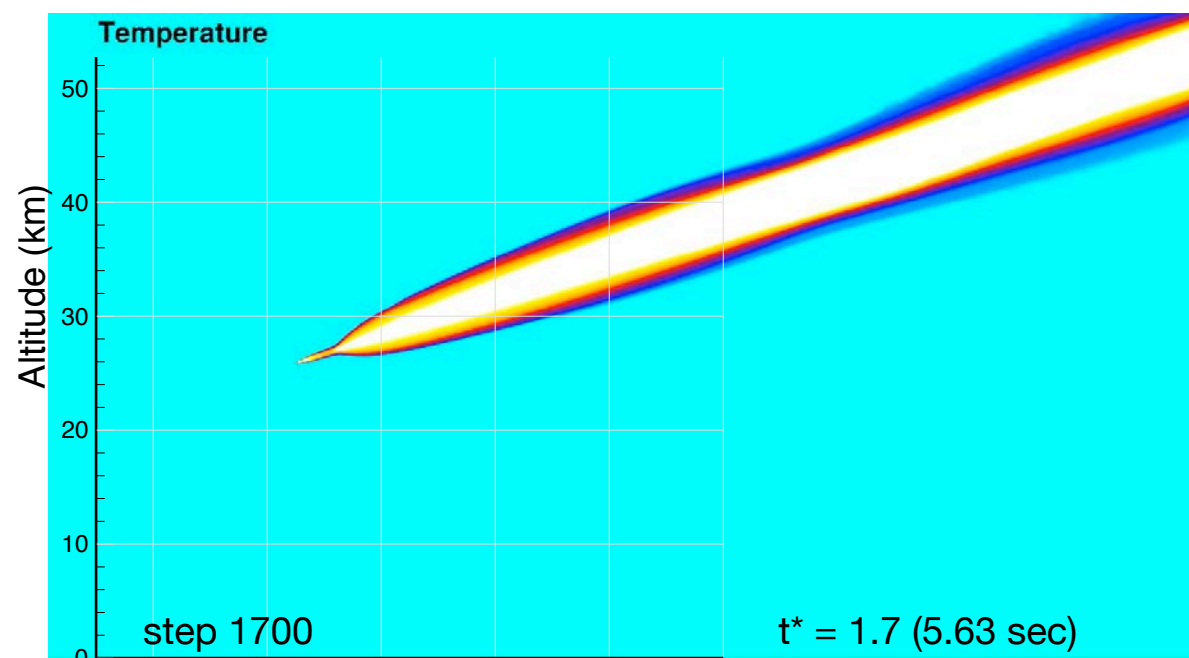
Line Source



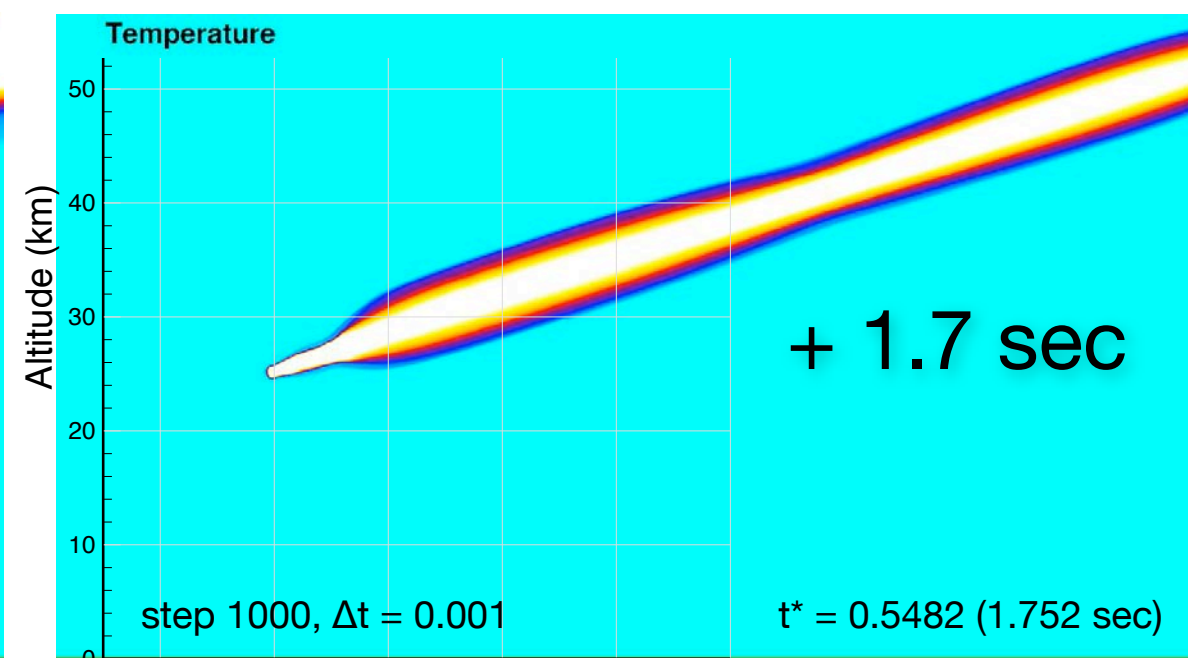
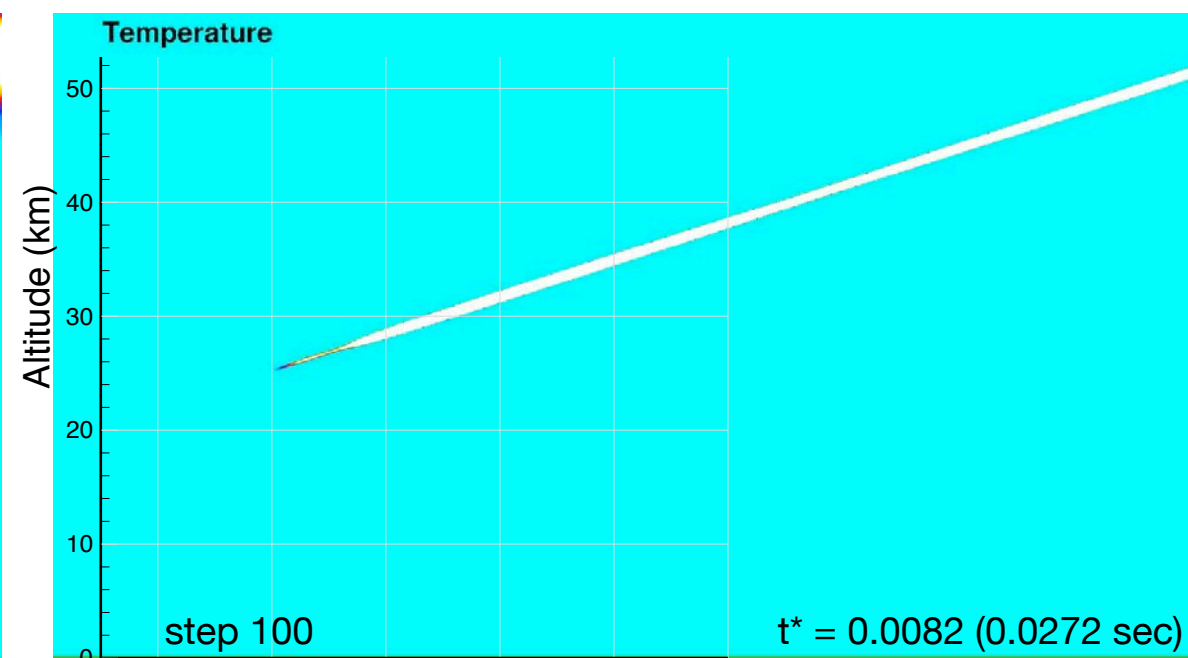
Sensitivity - Entry Modeling

Seconds after entry

Time-Dependent



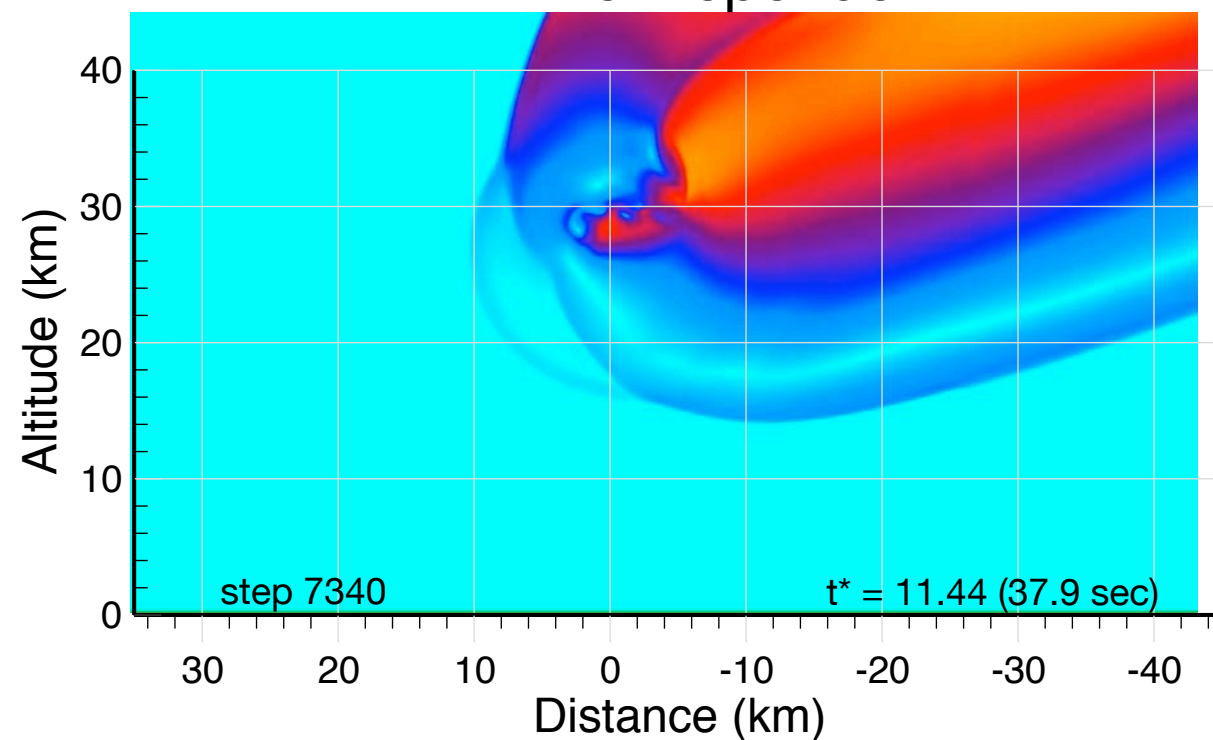
Line Source



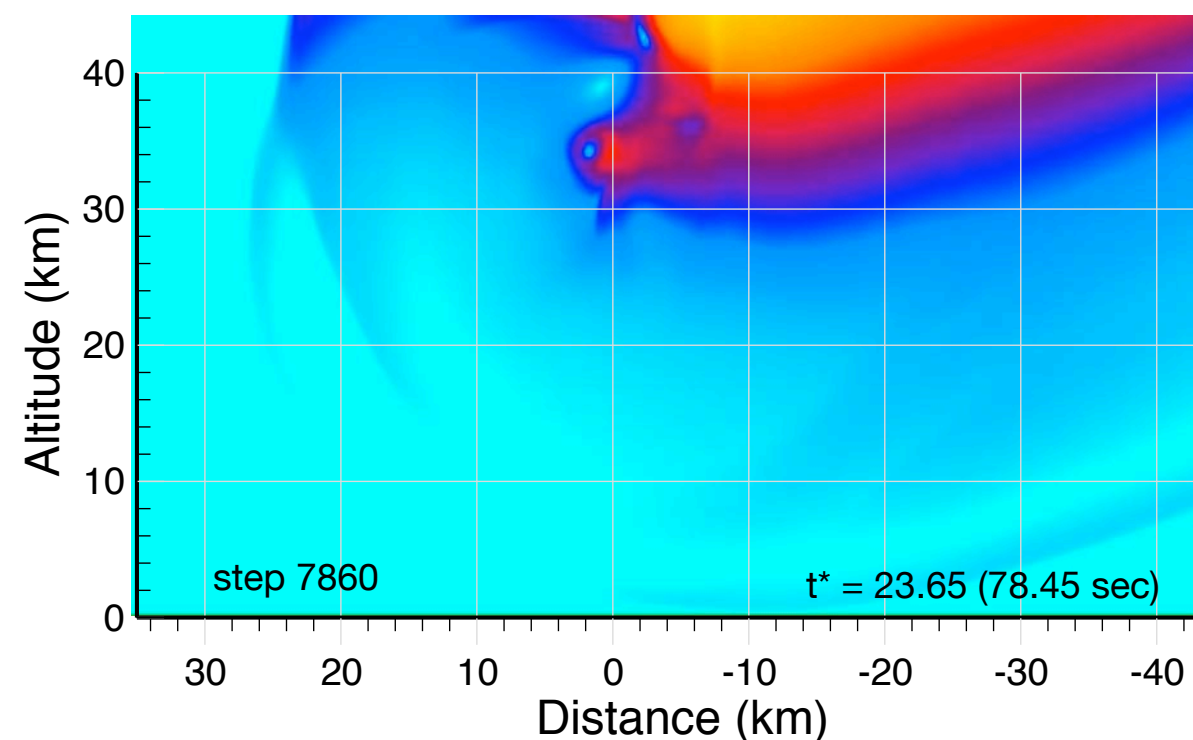
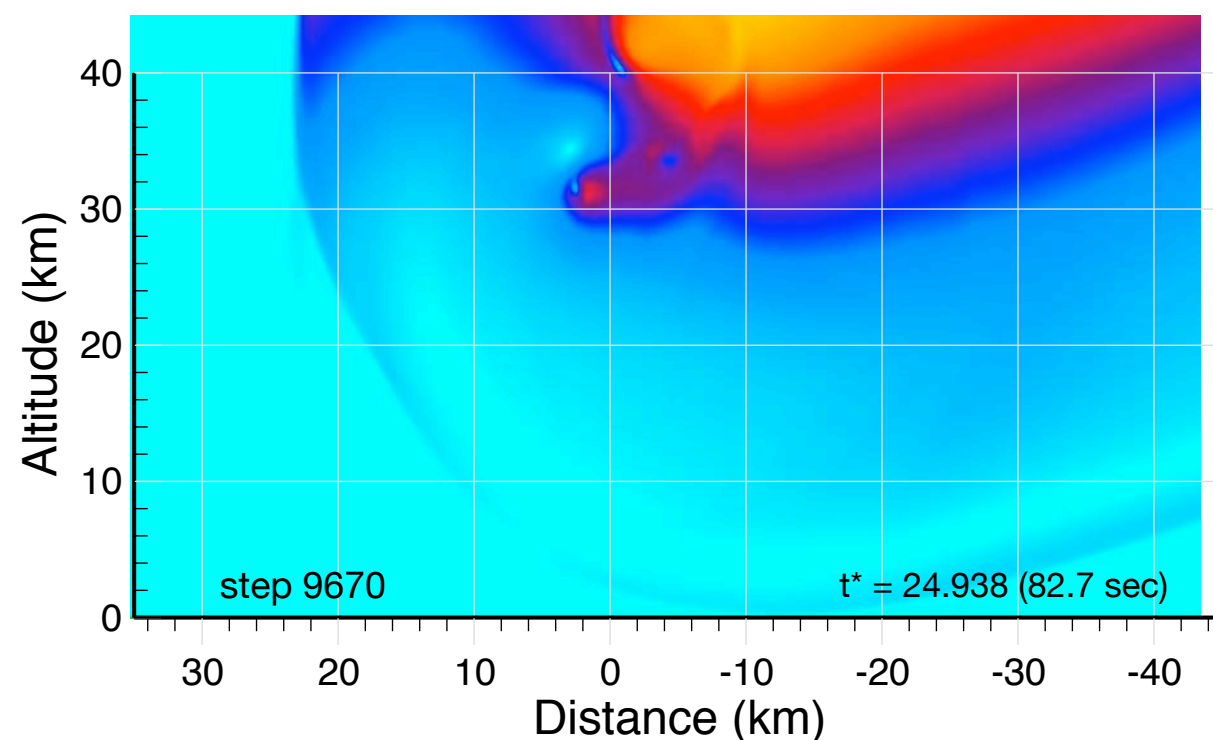
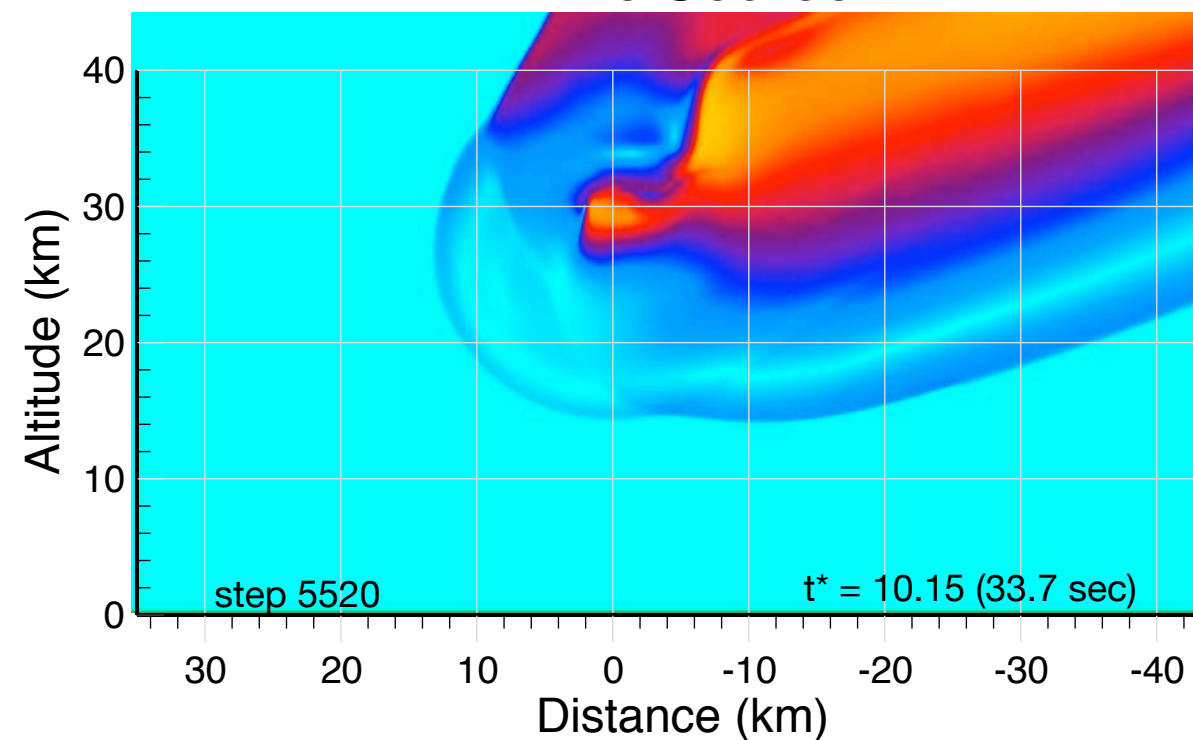
Sensitivity - Entry Modeling

Minutes after entry

Time-Dependent

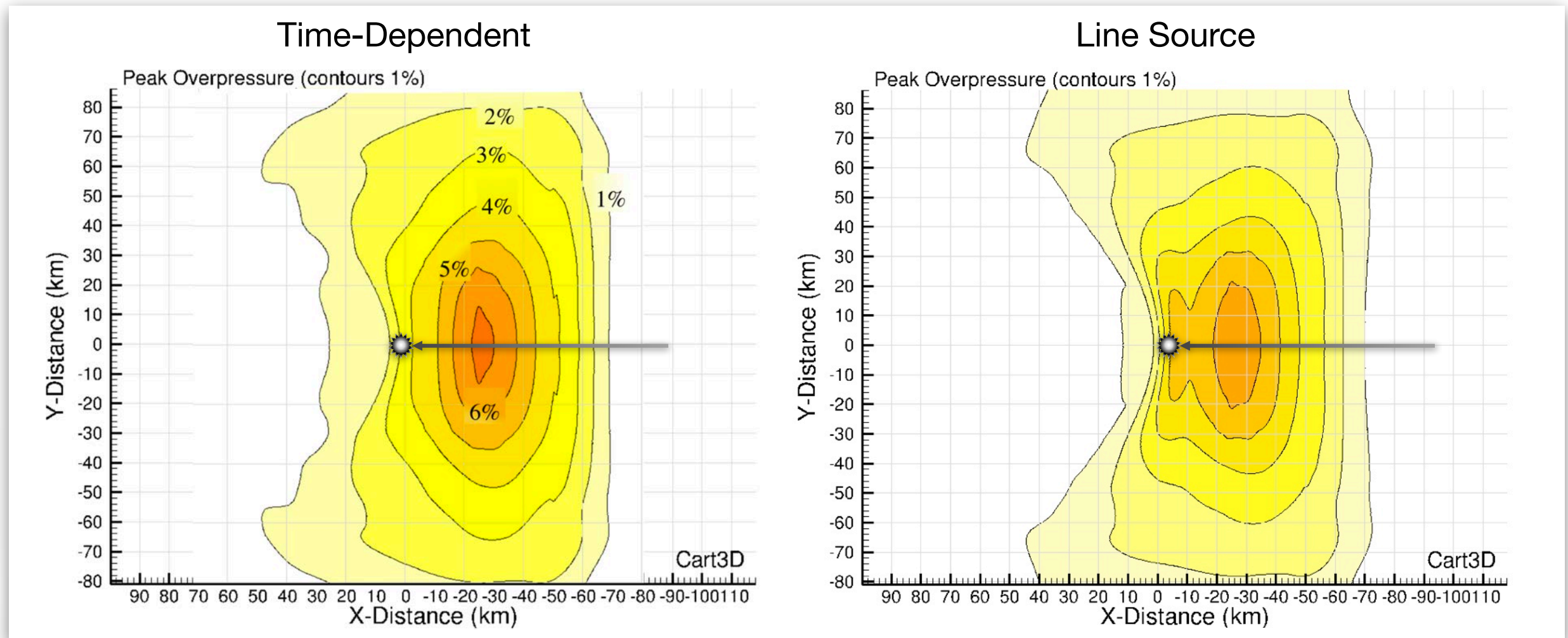


Line Source



Sensitivity - Entry Modeling

Ground Footprint

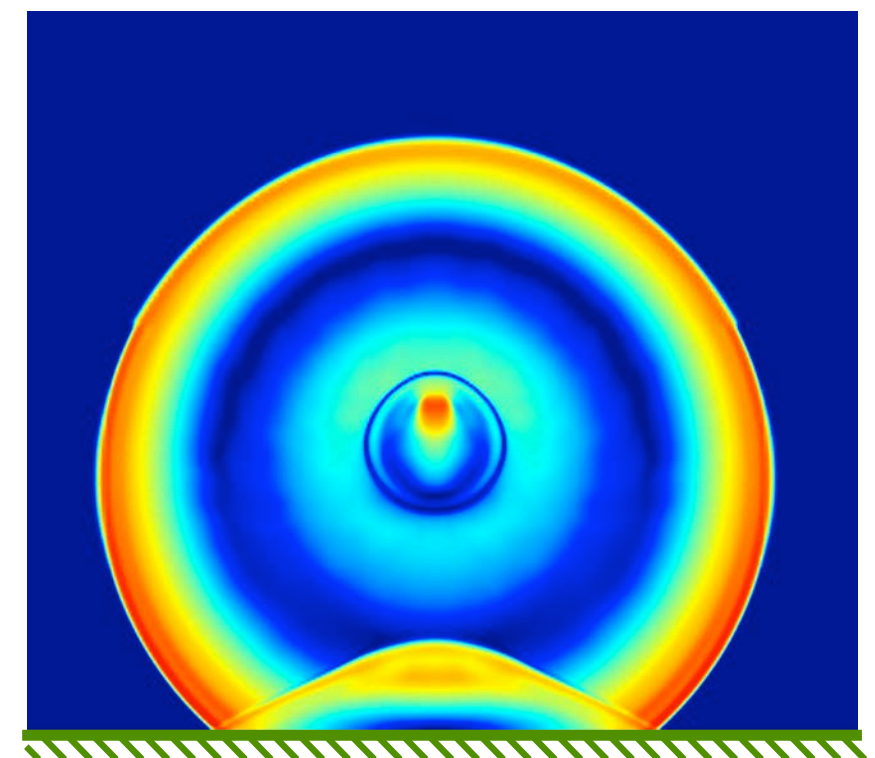
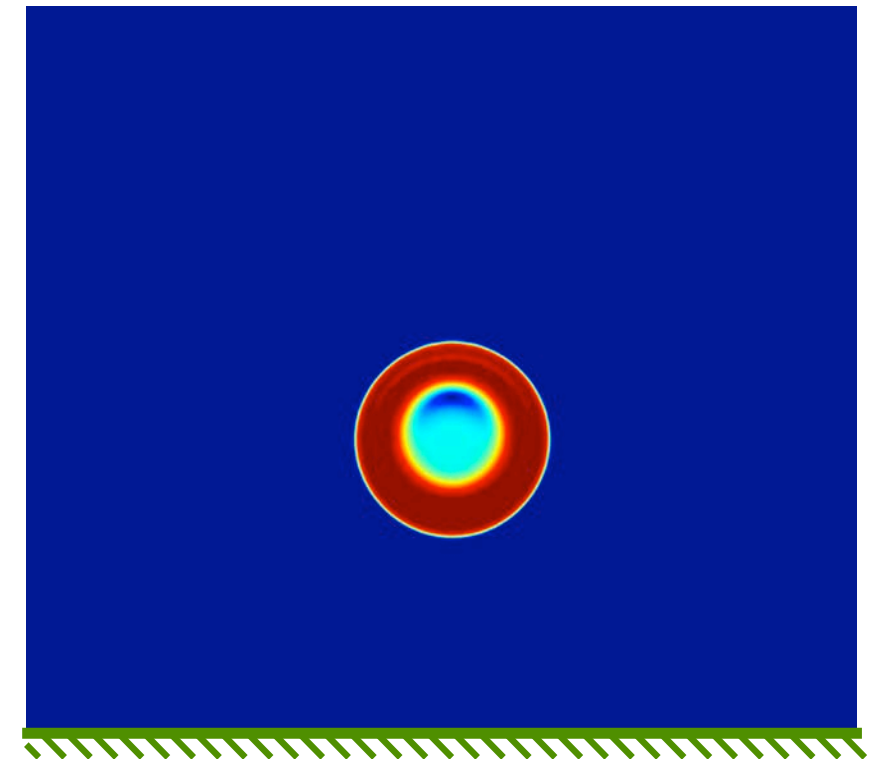


- Some differences in highest overpressures ($\sim 1\%$) at earliest arrival time
- Closer agreements at later time
- Good agreement for location of peak ground pressure
- Good agreement of arrival time from peak brightness
- Geometry dictates that low-entry trajectories will show most discrepancy

Sensitivity - 90° Entry vs Spherical Charge

How good is a static spherical charge model?

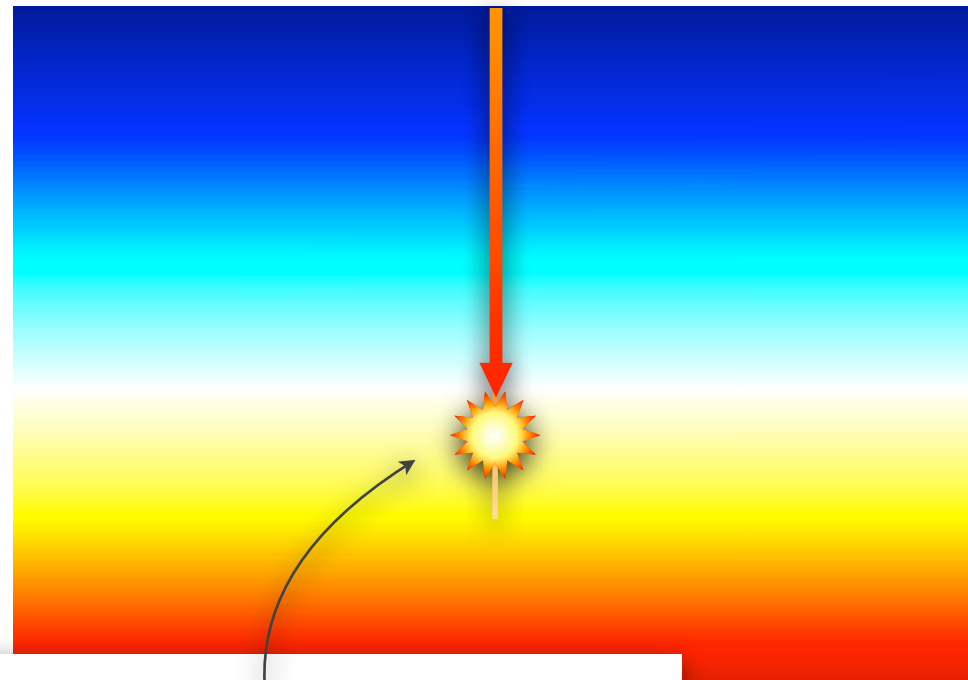
- Very cheap spherical charge models exist.
- Various handbook methods for damage estimation use spherical charge data
- Can these be used in risk assessment?
 - Where are these appropriate?
 - Perform quantitative assessment
- Investigate ground footprint
 - Accuracy of overpressure
 - Extent/strength of footprint
 - Details of impulse of blast on ground



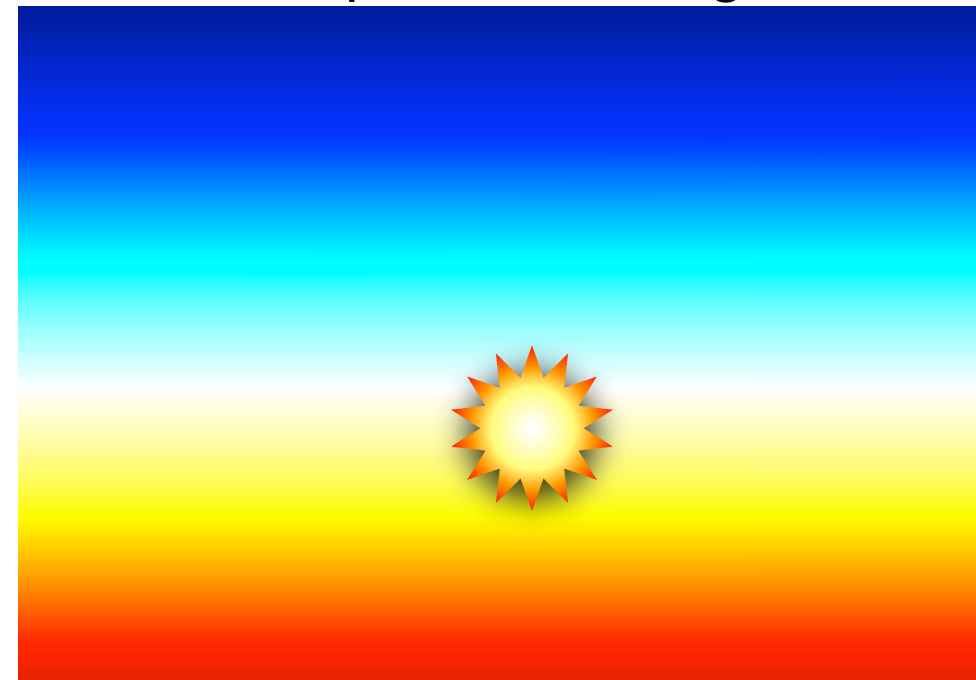
Sensitivity - 90° Entry vs Spherical Charge

How good is a static spherical charge model?

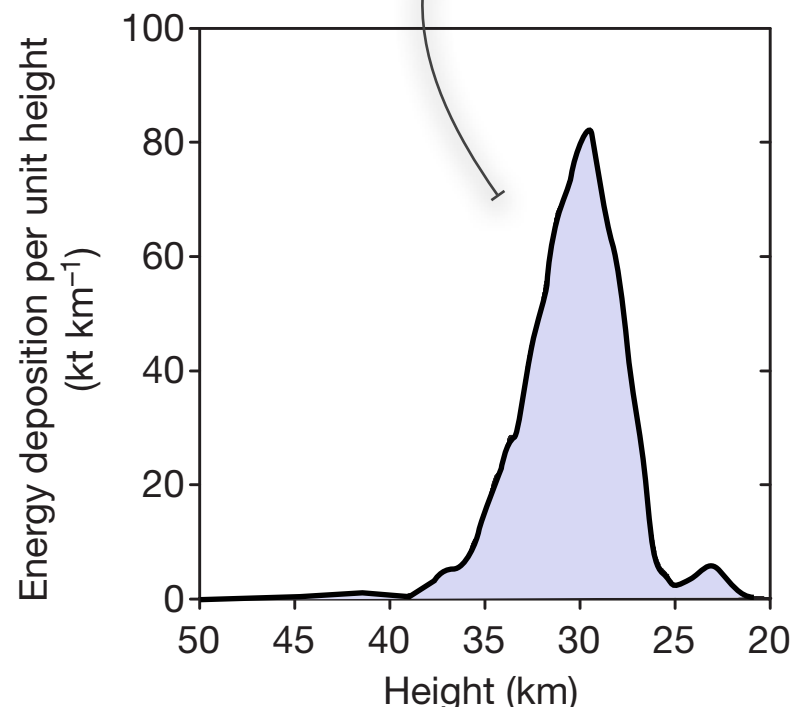
Line-Source at 90°



Spherical Charge



- $E_{tot} = 520 \text{ kt}$, $m_{tot} = 12.5 \text{e6 kg}$
- Spherical charge @ 29.5km altitude, $r_i = 1 \text{ km}$
- Line Source, 90° trajectory with same energy deposition as before
- Can also compare line source with 18° case for insight into entry angle sensitivity

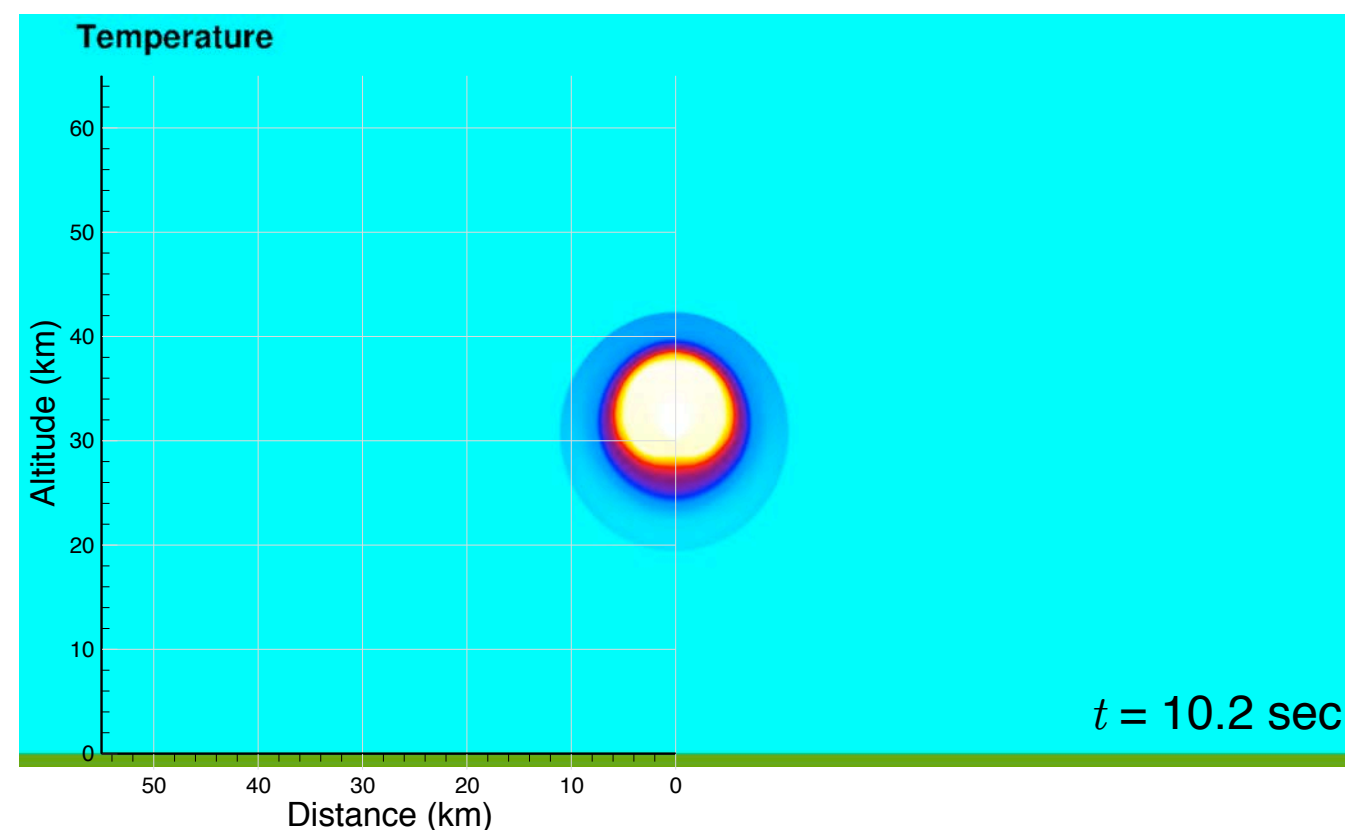
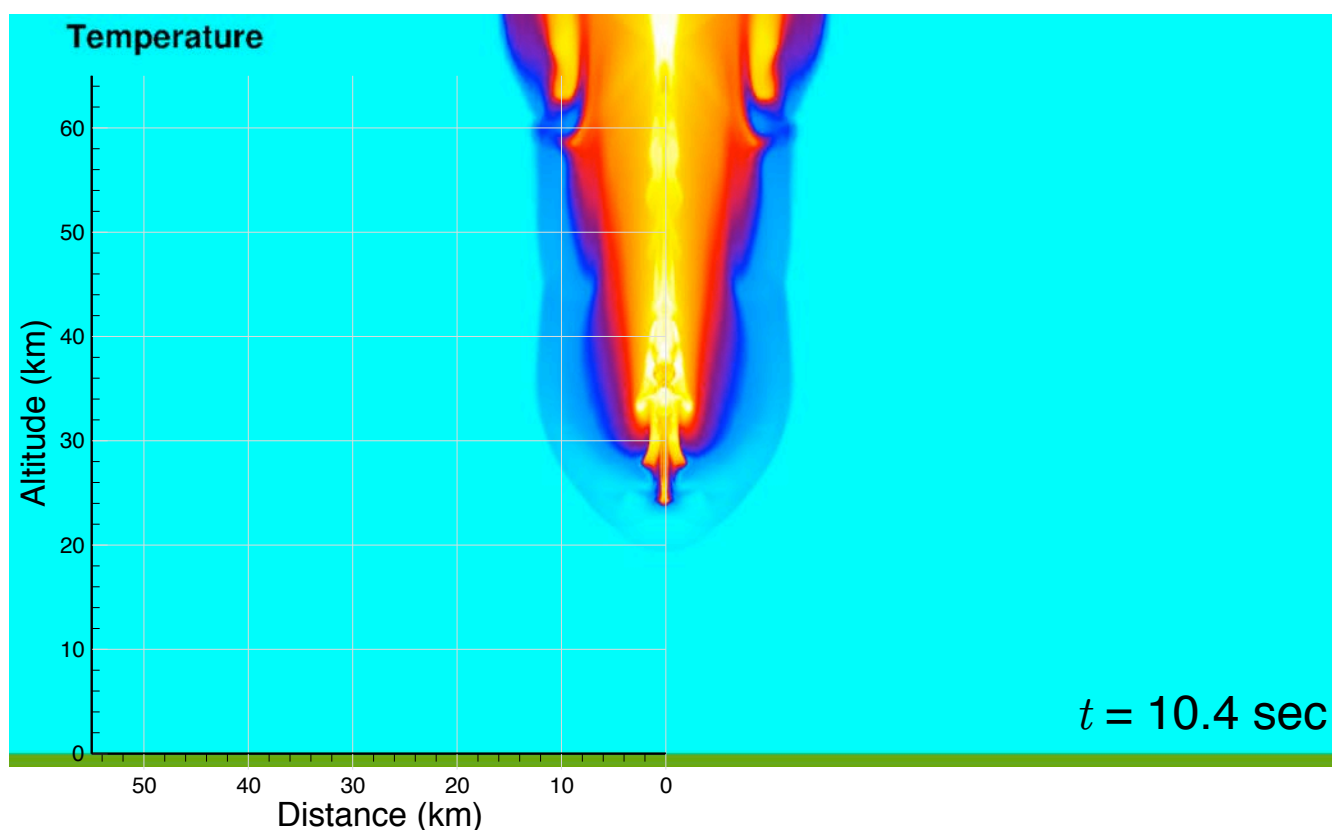


Sensitivity - 90° entry vs Spherical Charge

Time evolution

Line Source

Spherical Charge



$t = 10 \text{ sec}$

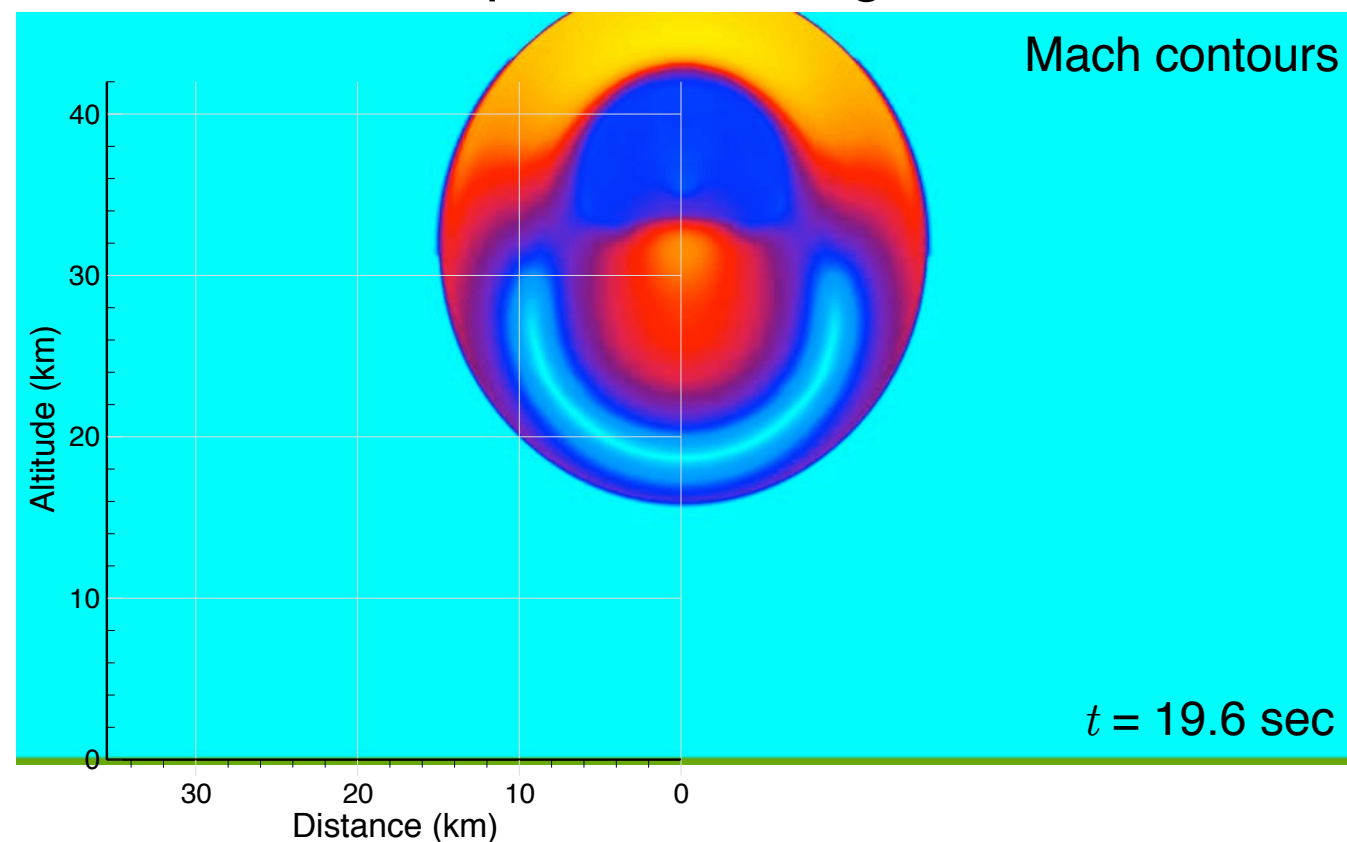
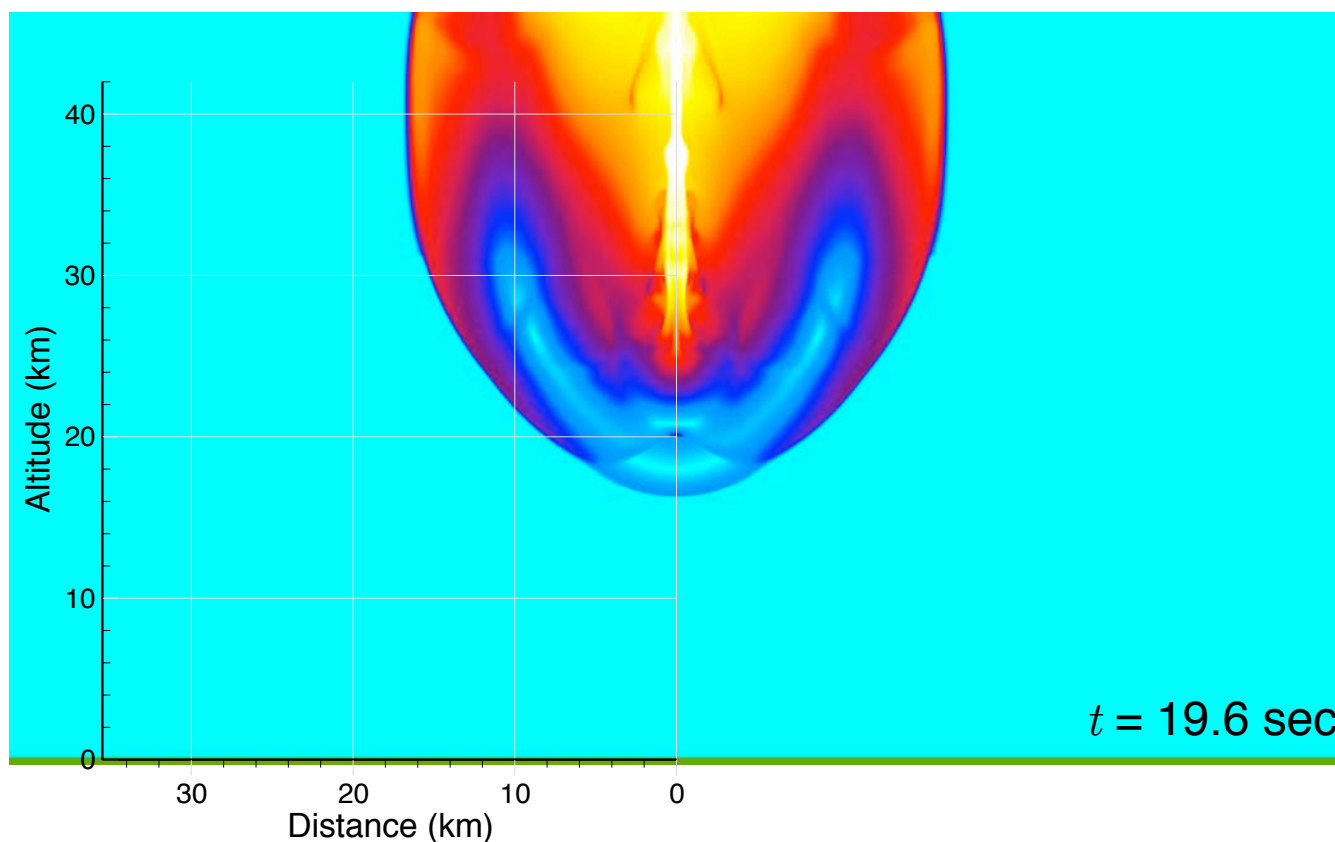
Sensitivity - 90° entry vs Spherical Charge

Time evolution

Line Source

Spherical Charge

Mach contours



$t = 19.6 \text{ sec}$

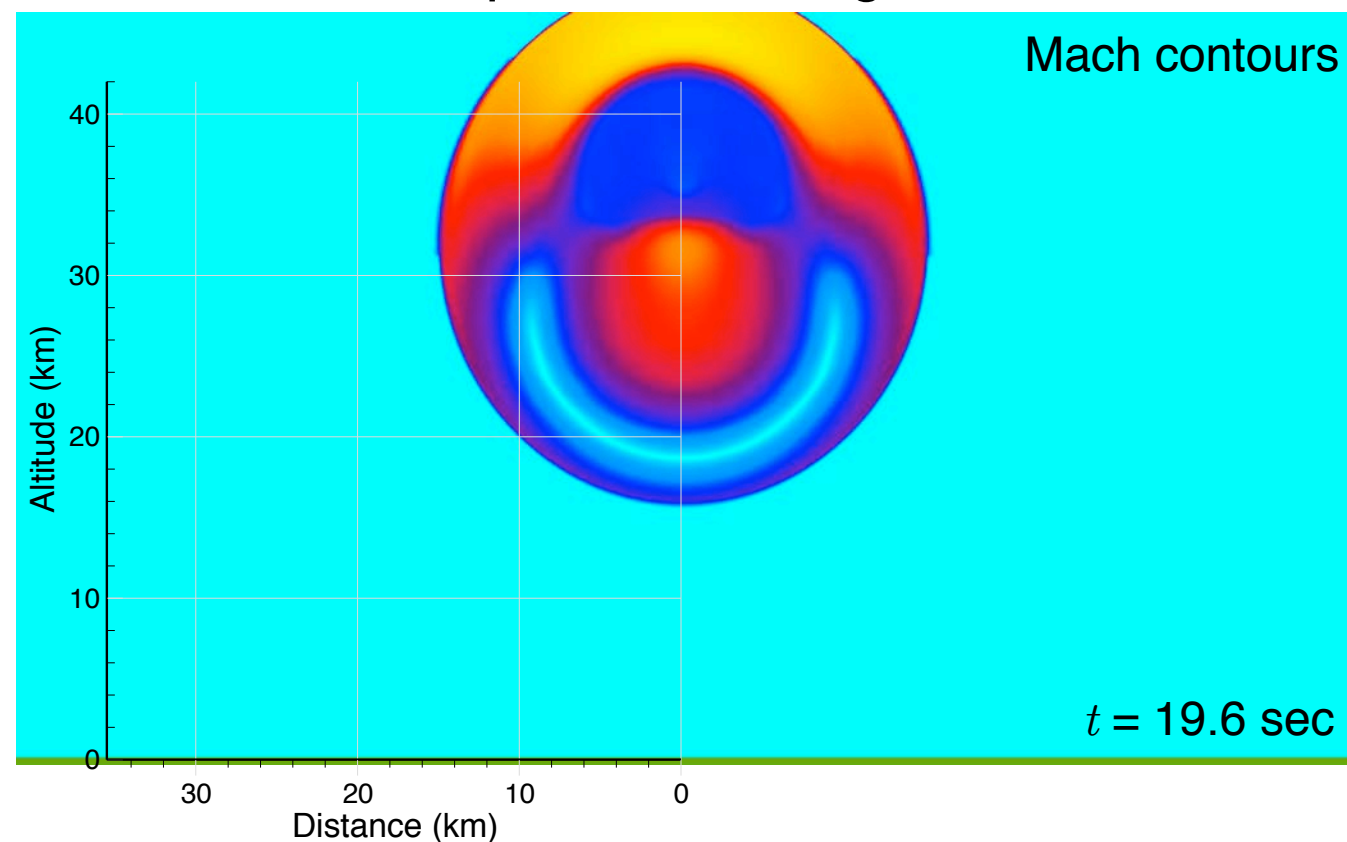
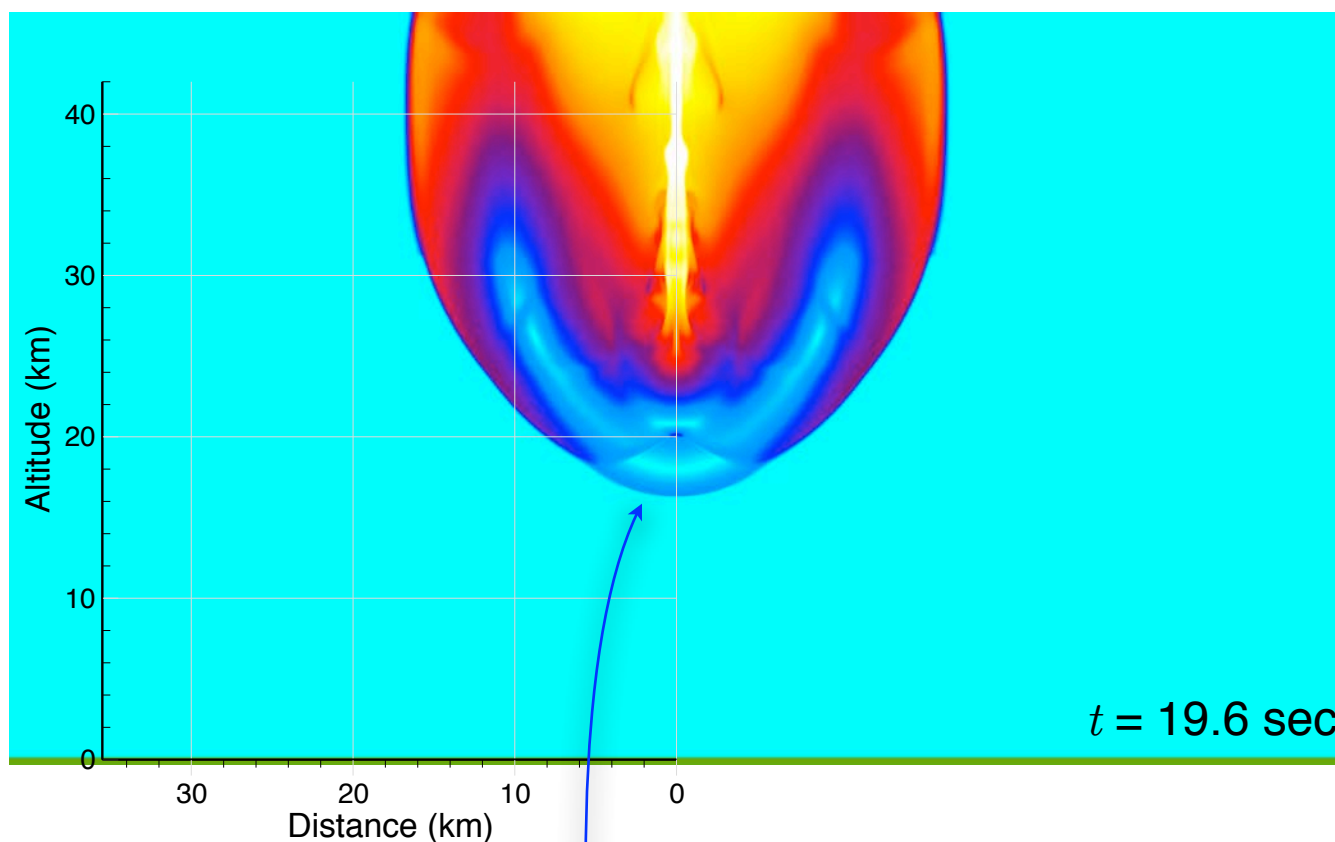
Sensitivity - 90° entry vs Spherical Charge

Time evolution

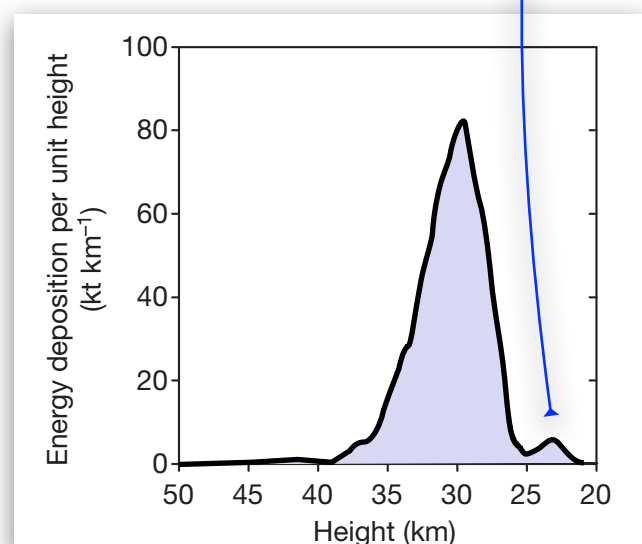
Line Source

Spherical Charge

Mach contours



$t = 19.6 \text{ sec}$

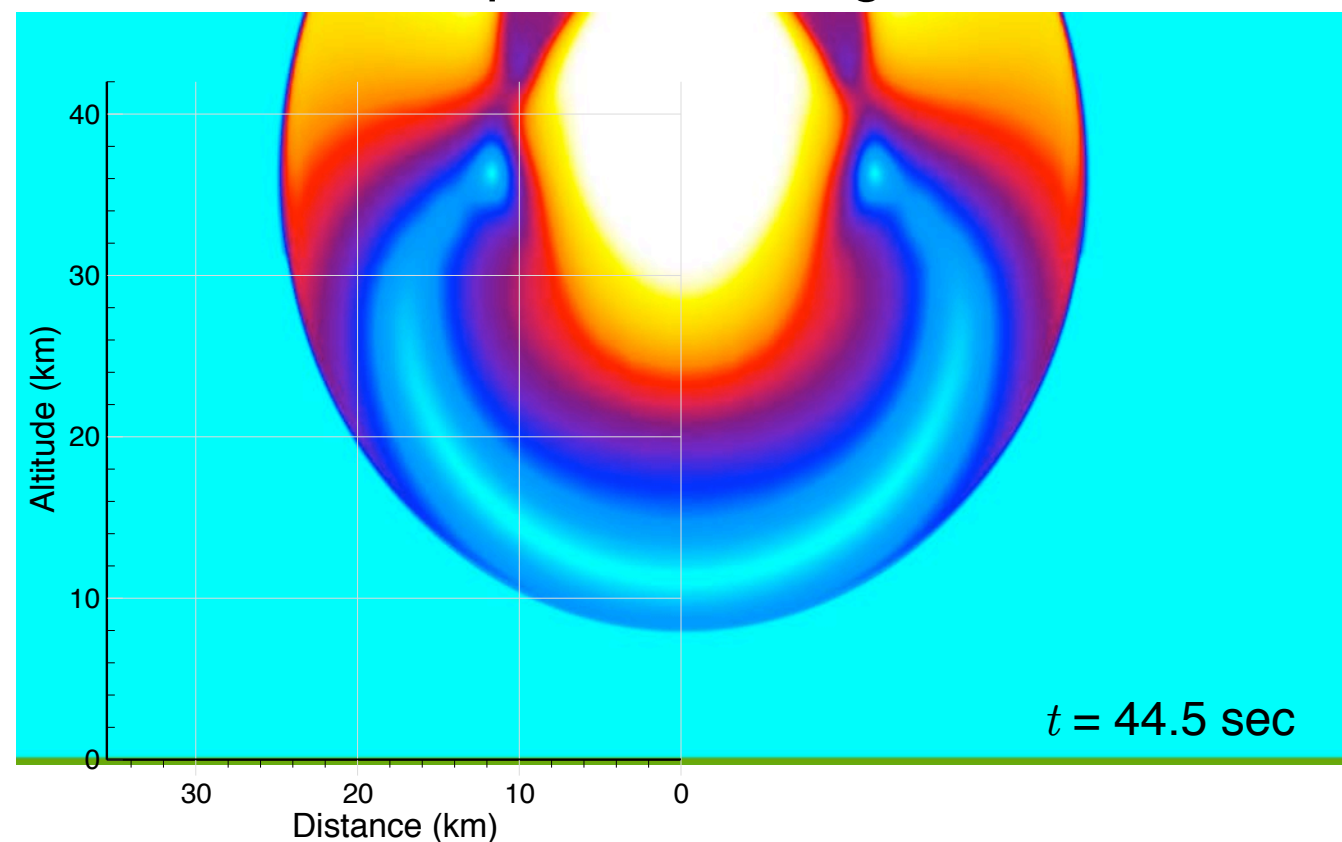
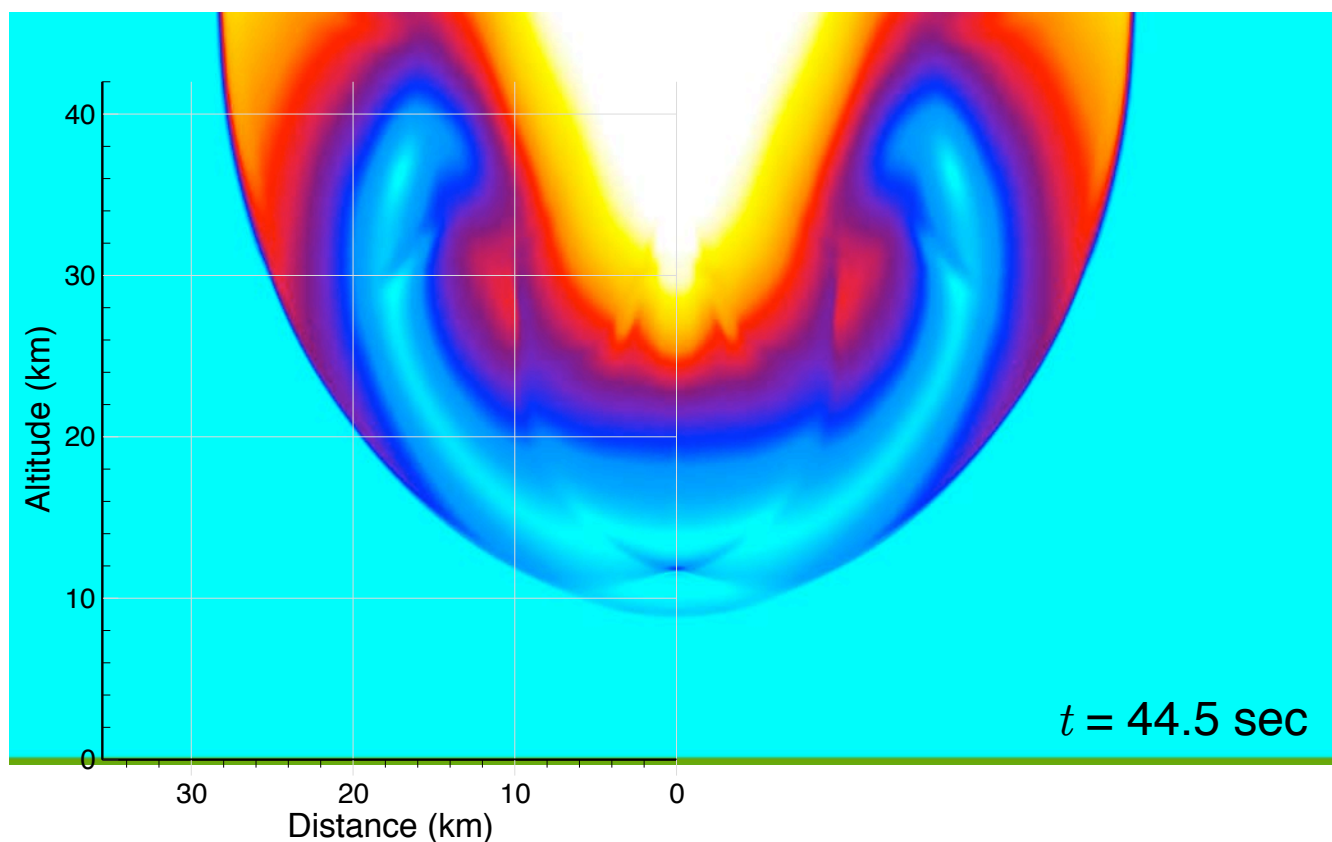


Sensitivity - 90° entry vs Spherical Charge

Time evolution

Line Source

Spherical Charge



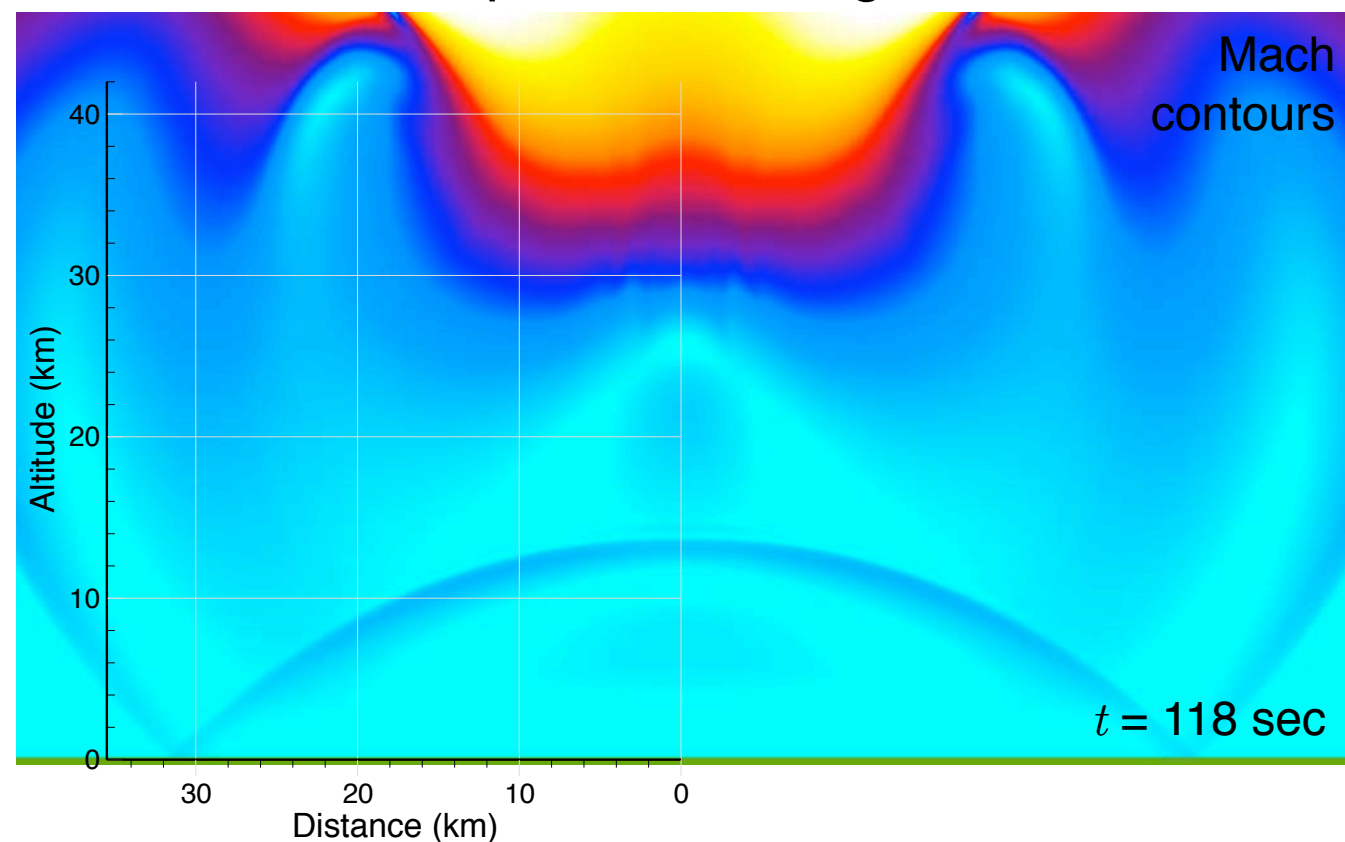
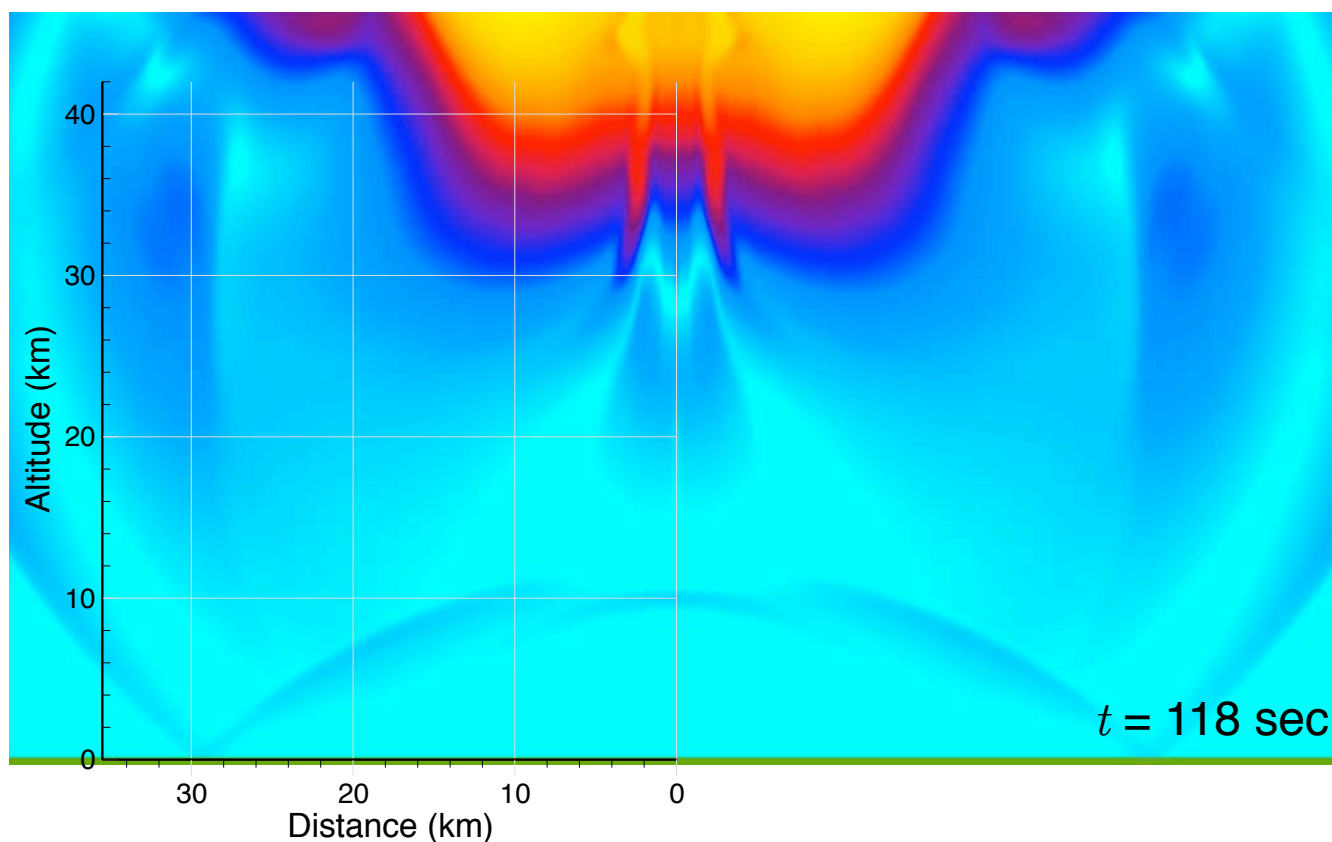
$t = 44.5 \text{ sec}$

Sensitivity - 90° entry vs Spherical Charge

Time evolution

Line Source

Spherical Charge

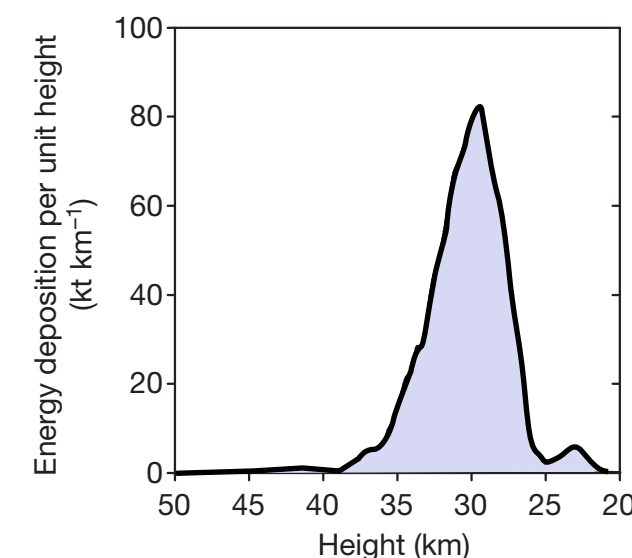


$t = 118 \text{ sec}$

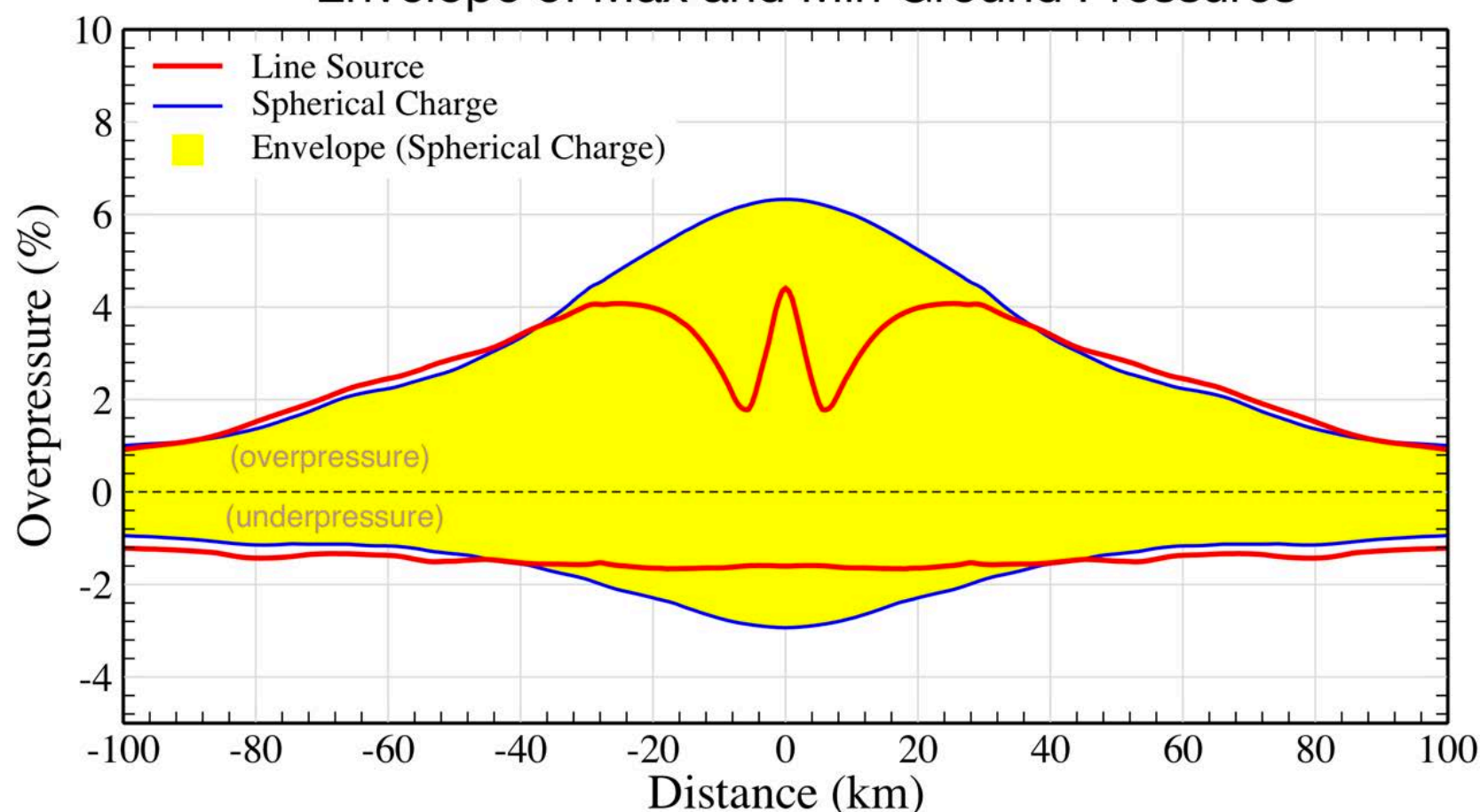
Sensitivity - 90° entry vs Spherical Charge

Ground footprint comparison

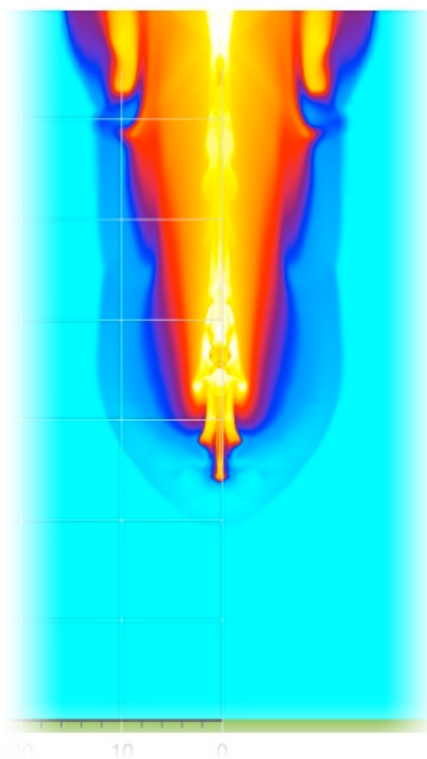
- Very similar envelopes - modulo details of energy deposition profile chosen.
- Both show lower peak overpressure than 18° trajectory



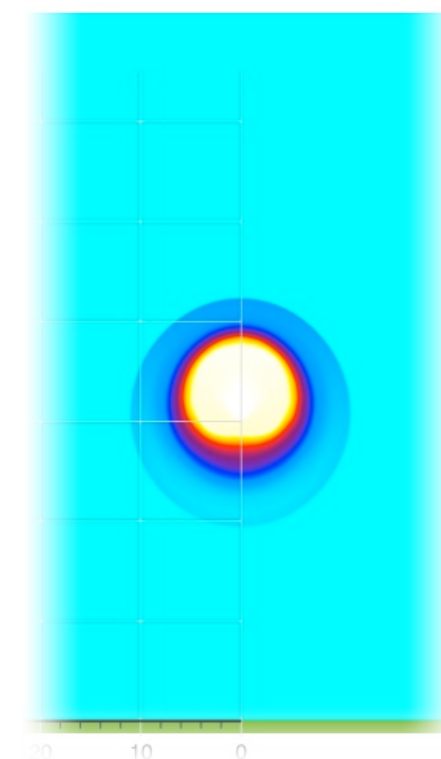
Envelope of Max and Min Ground Pressures



Line Source



Spherical Charge



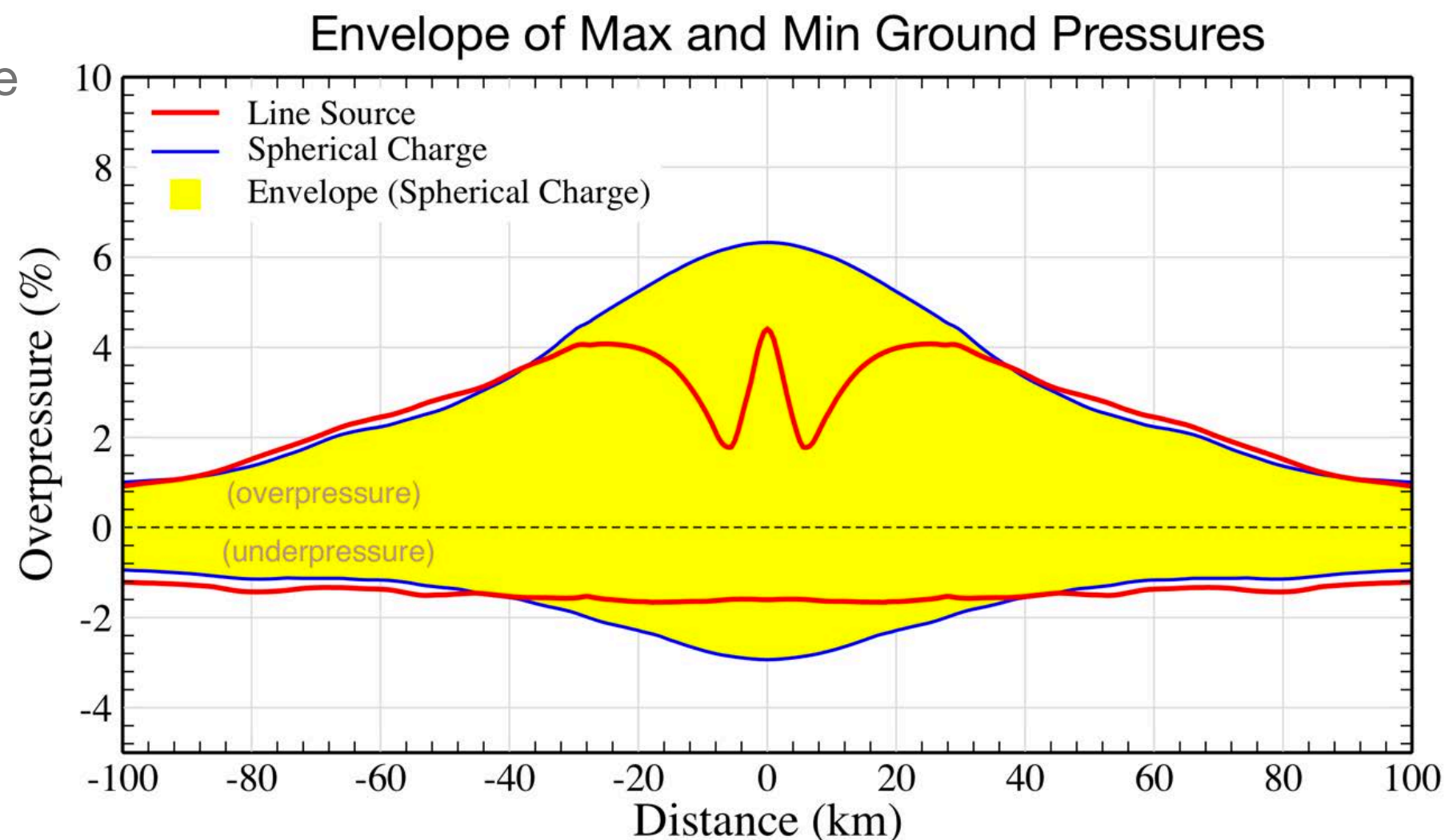
Sensitivity - 90° entry vs Spherical Charge

Ground footprint comparison

- Detailed pressure impulse shows similar instantaneous profiles as blast evolves



- Blast arrival times agree to within 2-3 seconds



Sensitivity - 90° entry vs Spherical Charge

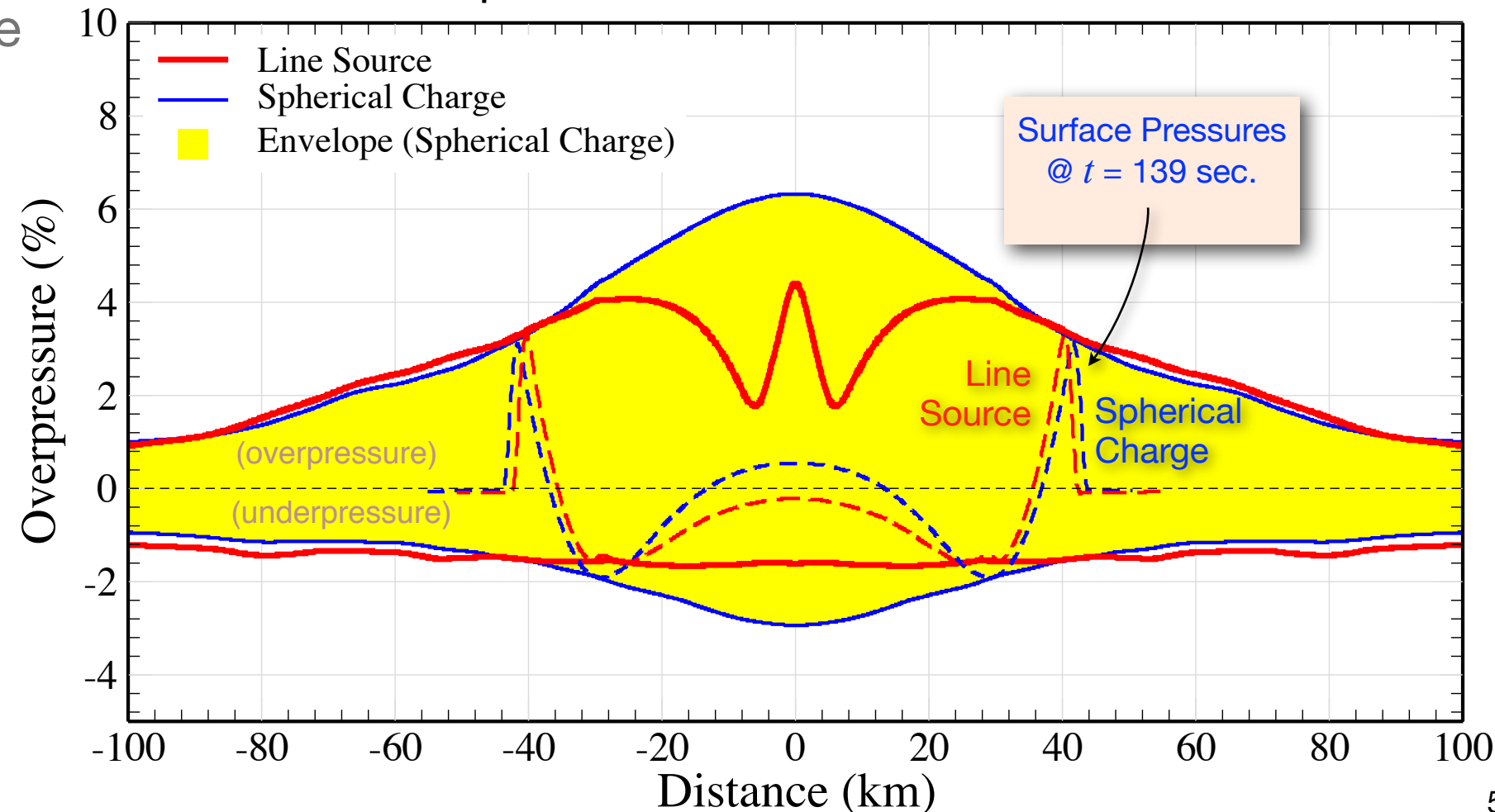
Ground footprint comparison

- Detailed pressure impulse shows similar instantaneous profiles as blast evolves



Envelope of Max and Min Ground Pressures

- Blast arrival times agree to within 2-3 seconds



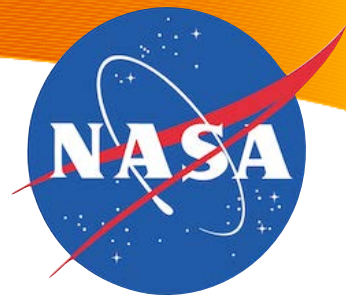


Summary

Atmospheric propagation and ground effects modeling

- Outlined modeling for far-field propagation of airburst events using a Cartesian finite-volume method
- Showed basic verification and validation
 - Good prediction for model problems
 - Good prediction of footprint and arrival time data for Chelyabinsk meteor
- Showed envelopes and time-evolution of ground footprints for damage prediction and atmospheric-driven tsunami simulations
- Preliminary sensitivity investigations
 - Line source vs full time-dependent entry
 - Effects of Entry angle & comparison with specific spherical blast

Full paper for modeling and V&V planned at AIAA SciTech 2016 in San Diego (Jan 2016)



Next Steps...

Atmospheric propagation and ground effects modeling

- Parametric drivers
 - Vary entry angle, size and strength of asteroid
 - Parametric modification of energy deposition curve
 - Precompute parametric studies -- feed results to PRA
- Cratering & splashing
- Terrain and structures
 - Refine particular when scenario arises (e.g. PDC 15)
- Update models being output to Physics-Based Risk Analysis
- Update models being input from entry and breakup modeling



Thank You!

- NASA Advanced Supercomputing Division – Task 3 & 4 teams

Marian Nemec
Jonathan Chiew
Chris Mattenberger
Lorien Wheeler

Donovan Mathias
George Anderson
Darrel Robertson

- Entry Systems Division – Task 2 team

Dinesh Prabhu

Ethiraj Venkatapathy

- New York University

Marsha Berger

- NASA PD IPT

James Arnold
Jessie Dotson
Derek Sears

Craig Burkhard
David Morrison

- IPT Seminar Speakers

Peter Jenniskens
Olga Popova
Paul Chodas

Peter Brown
Jay Melosh

- NASA NEO Office

Lindley Johnson